

**COAL COMBUSTION RESIDUAL RULE
GROUNDWATER MONITORING SYSTEM CERTIFICATION**

**MARTIN LAKE STEAM ELECTRIC STATION
PERMANENT DISPOSAL POND 5
RUSK COUNTY, TEXAS**

OCTOBER 16, 2017

Prepared For:

Luminant Generation Company, LLC
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Texas Engineering Firm No. 4760

PROFESSIONAL CERTIFICATION

This document and all attachments were prepared by Pastor, Behling & Wheeler, LLC under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gather and evaluate the information submitted. Based on my inquiry of those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I hereby certify that the groundwater monitoring system installed at the referenced facility has been designed and constructed to meet the requirements of Section 257.91 of the CCR Rule.



Patrick J. Behling, P.E.
Principal Engineer
PASTOR, BEHLING & WHEELER, LLC

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1.0 INTRODUCTION

Luminant Power (Luminant) operates the Martin Lake Steam Electric Station (MLSES) located approximately 5 miles southeast of Tatum, Rusk County, Texas (Figure 1). The MLSES consists of three coal/lignite-fired power generation units. Coal Combustion Residuals (CCRs) including fly ash, bottom ash and gypsum are generated as part of the MLSES unit operations. Currently, CCRs generated at the MLSES are transported off-site for beneficial use by third-parties or are managed by Luminant in surface impoundments located on the MLSES property or the A1 Area Landfill located approximately 2.5 miles east of the MLSES. Three CCR Units have been identified within the MLSES operations, the Ash Pond Area (the West Ash Pond (WAP) East Ash Pond (EAP), and the New Scrubber Pond), Permanent Disposal Pond 5 (PDP 5), and A1 Area Landfill. This report discusses PDP 5 (the Site). PDP 5 meets the definition of a CCR surface impoundment and is subject to groundwater monitoring system requirements of the CCR Rule.

The CCR Rule (40 CFR 257 Subpart D - *Standards for the Receipt of Coal Combustion Residuals in Landfills and Surface Impoundments*) has been promulgated by the EPA to regulate the management and disposal of CCRs as solid waste under Resource Conservation and Recovery Act (RCRA) Subtitle D. The final CCR Rule was published in the Federal Register on April 17, 2015. The effective date of the CCR Rule was October 19, 2015.

The CCR Rule establishes national minimum criteria for existing and new CCR landfills, existing and new CCR surface impoundments, and lateral expansions to landfills/impoundments. Pastor, Behling & Wheeler, LLC (PBW) was retained by Luminant to evaluate and certify that the groundwater monitoring system at the Site in accordance with Section 257.91 of the CCR Rule.

1.1 Description of PDP 5

PDP 5 was constructed in 2010 and is located approximately 3,000 feet west of the MLSES power units (Figure 2). It is used for emergency storm water storage and for storage of material from the ash ponds and New Scrubber Pond during cleaning cycles (BM, 2015).

Based on drawings provided by Luminant and included in the BM report, PDP 5 is lined with compacted soil measuring 3 feet thick on its sides and 2 feet thick on its bottom (BM, 2015). PDP 5 is built on top of three closed and capped landfills (PDP 1, PDP 2, and PDP 3). PDP 4, which is located adjacent to PDP 5

to the south, is also a closed and capped landfill. PDP 1 through PDP 4 are not considered regulated units under the CCR Rule.

1.2 CCR Unit Groundwater Monitoring System Requirements

Section 257.91 of the CCR Rule indicates that existing CCR landfills and surface impoundments be provided with a groundwater monitoring system that consists of sufficient wells, installed at appropriate location and depths, to yield groundwater samples from the uppermost aquifer that meet the following criteria:

- Accurately represent the quality of background groundwater that has not been affected by leakage from a CCR unit; and
- Accurately represent the quality of groundwater passing the waste boundary of the CCR unit. The downgradient monitoring system must be installed at the waste boundary to ensure detection of groundwater contamination in the uppermost aquifer. All potential contaminant pathways must be monitored.

The specific configuration of the groundwater monitoring system must be determined based on site-specific technical information that must include aquifer thickness, groundwater flow rate, groundwater flow direction (including seasonal and temporal fluctuation in groundwater flow), saturated and unsaturated geologic units and fill materials that overly the uppermost aquifer, materials comprising the uppermost aquifer, and materials comprising the confining unit defining the lower boundary of the upmost aquifer, including, but not limited to, thickness, stratigraphy, lithology, hydraulic conductivities, porosities, and effective porosities.

At a minimum, the monitoring system must consist of at least one upgradient and three downgradient monitoring wells, and any additional monitoring wells necessary to accurately represent the quality of the background groundwater that has not been affected by leakage from the CCR unit and the quality of groundwater passing the waste boundary of the CCR unit. Multi-unit groundwater monitoring systems are allowed but must be equally as capable of detecting monitored constituents at the waste boundary of a CCR unit as individual groundwater monitoring wells.

Monitoring wells must be cased in a manner that maintains the integrity of the monitoring well borehole. This casing must be screened or perforated and packed with gravel or sand, where necessary, to enable collection of groundwater samples. The annular space above the sampling depth must be sealed to prevent contamination of samples and the groundwater. There must be documentation in the operating

record of the design, installation, development, and decommissioning of any monitoring wells, piezometers and other measurement, sampling, and analytical devices. The qualified engineer must have access to and must review this documentation as part of the groundwater monitoring system certification.

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2.0 GROUNDWATER MONITORING SYSTEM EVALUATION

2.1 PDP 5 Groundwater Monitoring System

The CCR groundwater monitoring well system at PDP 5 consists of nine monitoring wells (MW-17A, MW-18A, MW-19, MW-20A, PDP-22, PDP-23, PDP-24, PDP-25, PDP-26) that are each screened in the uppermost aquifer at the Site. The locations of the CCR monitoring wells are shown on Figure 2. Well construction information and survey data for the CCR wells are summarized in Table 1, CCR monitoring well logs are presented in Appendix A, and photographs of the CCR wells are presented in Appendix B.

2.2 Local Geology and Hydrogeology

PDP 5 is located in the outcrop area of the Eocene-aged Wilcox Group (Barnes, 1965). PBW reviewed current and historical soil boring logs, monitoring well completion documentation, and historical reports to describe the geologic and hydrogeologic conditions at PDP 5. Geologic cross sections were constructed using these data. Cross section locations are presented on Figure 3 and the cross sections are presented on Figures 4, 5, and 6.

The geologic units encountered during the completion of monitoring wells/soil borings in the PDP 5 Area include: (1) an upper sand unit observed on hilltops and other topographically high areas, (2) an intermediate continuous clay unit that contains discontinuous, interbedded sand layers, and (3) a lower unit of silt and sand that contains discontinuous packages of relatively thick, interbedded clay. Based on information provided by Luminant, PDP 5 is completed entirely within the upper hilltop sand unit. The uppermost aquifer at the Site occurs in the lower unit of silt and sand that contains discontinuous packages of relatively thick, interbedded clay.

2.3 Groundwater Potentiometric Surface Elevations

Eight background groundwater monitoring events were performed using the PDP 5 CCR monitoring well system from October 2015 to December 2016. Static water levels measured during the background monitoring period indicated water elevations ranging from 352.38 feet above mean sea level (amsl) to 381.40 feet amsl, and depths to water ranging from 5.14 feet bgs to 37.46 feet bgs (Table 2). Groundwater potentiometric surface maps based on data collected during the background monitoring period are presented in Appendix C.

Groundwater is mounded at PDP 5, with an inferred groundwater flow direction radially outward from the unit. Based on the inferred direction of groundwater flow, there are no upgradient areas in the immediate vicinity of PDP 5. All of the CCR monitoring wells, which are positioned radially around PDP 5, are downgradient wells.

2.4 Uppermost Aquifer Hydraulic Conductivity Testing

PBW performed slug tests at monitoring wells PDP-22, PDP-25, and PDP-26 on October 7, 2015 to evaluate groundwater linear flow velocities at the uppermost aquifer at the Site. Slug test data and time-head change plots used to calculate hydraulic conductivities and transmissivities of the uppermost aquifer are provided in Appendix D. A summary of these hydraulic properties is presented in Table 3. The average hydraulic conductivities for the wells ranged from 2.48×10^{-5} cm/sec (well PDP-22) to 1.37×10^{-4} cm/sec (well PDP-25), with a geometric mean for the test wells of 4.40×10^{-5} cm/sec.

2.5 Conclusions

The CCR groundwater monitoring well system at PDP 5 complies with Section 257.91 of the CCR Rule. This conclusion is supported by the following as described in detail in previous sections of this report:

- Nine monitoring wells are included in the CCR groundwater monitoring system. Based on the inferred direction of groundwater flow there are no upgradient areas in the immediate vicinity of PDP 5, and all of the CCR monitoring wells, which are positioned radially around PDP 5, are downgradient wells.
- Each monitoring well is screened in the uppermost aquifer at the Site. Samples collected from the downgradient wells will ensure detection of groundwater contamination in the uppermost aquifer from the CCR unit.
- The monitoring wells are constructed with appropriate well casing to maintain the integrity of the monitoring well borehole and with slotted well screens to enable collection of groundwater samples. In addition, the annular space above the well screen is appropriately sealed to prevent contamination of groundwater samples from surface sources.
- Appropriate documentation exists concerning the design, installation, and development of the monitoring wells.

3.0 REFERENCES

Barnes, Virgil E., 1965. Geologic Atlas of Texas, Tyler Sheet. Texas Bureau of Economic Geology.

Burns & McDonnell Engineering Company, Inc (BM), 2015. CCR Study for Martin Lake Steam Electric Station – Final Draft. June 2015.

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Tables

TABLE 1
WELL CONSTRUCTION SUMMARY
PERMANENT DISPOSAL POND 5
MARTIN LAKE STEAM ELECTRIC STATION

| Well ID | Date Installed | Northing | Easting | Ground Elevation (ft amsl) | TOC Elevation (ft amsl) | Top of Screen (ft bgs) | Bottom of Screen (ft bgs) | Screen Length (ft) | Total Design Depth (ft bgs) | Casing Diameter (in) |
|----------------|-----------------------|-----------------|----------------|-----------------------------------|--------------------------------|-------------------------------|----------------------------------|---------------------------|------------------------------------|-----------------------------|
| MW-17A | 10/01/08 | 228279 | 2902653 | 384.57 | 387.75 | 27 | 47 | 20 | 47 | 2 |
| MW-18A | 10/2/08 | 228860 | 2902563 | 410.89 | 414.44 | 47 | 67 | 20 | 67 | 2 |
| MW-19 | 9/30/08 | 229492 | 2902142 | 367.98 | 371.33 | 10 | 25 | 15 | 25 | 2 |
| MW-20A | 9/30/08 | 228847 | 2901077 | 395.74 | 398.98 | 10 | 40 | 30 | 41 | 2 |
| PDP-22 | 9/9/15 | 229672 | 2901564 | 383.90 | 386.75 | 35 | 60 | 25 | 60 | 2 |
| PDP-23 | 9/10/15 | 229231 | 2902465 | 391.06 | 394.43 | 35 | 45 | 10 | 45 | 2 |
| PDP-24 | 9/11/15 | 228132 | 2902782 | 387.06 | 389.73 | 30 | 40 | 10 | 40 | 2 |
| PDP-25 | 9/11/15 | 227735 | 2901945 | 385.13 | 387.97 | 50 | 60 | 10 | 60 | 2 |
| PDP-26 | 9/9/15 | 227663 | 2900878 | 394.29 | 397.68 | 39 | 49 | 10 | 49 | 2 |

Notes:

1. Abbreviations: ft - feet; amsl - above mean sea level; bgs - below ground surface.

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**TABLE 2
GROUNDWATER ELEVATION SUMMARY
PERMANENT DISPOSAL POND 5
MARTIN LAKE STEAM ELECTRIC STATION**

| Well ID | TOC Elevation (ft amsl) | Date | Depth to Water (ft bgs) | Water Elevation (ft amsl) |
|----------------|--------------------------------|-------------|--------------------------------|----------------------------------|
| MW-17A | 387.75 | 10/19/15 | 18.69 | 369.06 |
| | | 12/14/15 | 17.14 | 370.61 |
| | | 02/24/16 | 16.80 | 370.95 |
| | | 04/05/16 | 16.46 | 371.29 |
| | | 06/06/16 | 15.62 | 372.13 |
| | | 08/09/16 | 16.14 | 371.61 |
| | | 10/17/16 | 16.39 | 371.36 |
| | | 12/11/16 | 18.17 | 369.58 |
| MW-18A | 414.44 | 10/20/15 | 37.41 | 377.03 |
| | | 12/14/15 | 35.92 | 378.52 |
| | | 02/24/16 | 34.84 | 379.60 |
| | | 04/05/16 | 33.88 | 380.56 |
| | | 06/06/16 | 33.96 | 380.48 |
| | | 08/09/16 | 33.04 | 381.40 |
| | | 10/17/16 | 35.31 | 379.13 |
| | | 12/11/16 | 37.46 | 376.98 |
| MW-19 | 371.33 | 10/20/15 | 12.60 | 358.73 |
| | | 12/14/15 | 5.14 | 366.19 |
| | | 02/24/16 | 5.56 | 365.77 |
| | | 04/05/16 | 5.99 | 365.34 |
| | | 06/06/16 | 5.31 | 366.02 |
| | | 08/09/16 | 9.59 | 361.74 |
| | | 10/17/16 | 6.81 | 364.52 |
| | | 12/11/16 | 9.06 | 362.27 |
| MW-20A | 398.98 | 10/20/15 | 25.17 | 373.81 |
| | | 12/14/15 | 23.64 | 375.34 |
| | | 02/24/16 | 23.44 | 375.54 |
| | | 04/05/16 | 23.23 | 375.75 |
| | | 06/06/16 | 22.39 | 376.59 |
| | | 08/09/16 | 23.92 | 375.06 |
| | | 10/17/16 | 24.47 | 374.51 |
| | | 12/11/16 | 25.96 | 373.02 |
| PDP-22 | 386.75 | 10/20/15 | 34.17 | 352.58 |
| | | 12/14/15 | 33.48 | 353.27 |
| | | 02/24/16 | 33.09 | 353.66 |
| | | 04/05/16 | 32.66 | 354.09 |
| | | 06/06/16 | 33.49 | 353.26 |
| | | 08/09/16 | 32.21 | 354.54 |
| | | 10/17/16 | 32.59 | 354.16 |
| | | 12/11/16 | 34.37 | 352.38 |
| PDP-23 | 394.43 | 10/20/15 | 23.61 | 370.82 |
| | | 12/14/15 | 22.34 | 372.09 |
| | | 02/24/16 | 19.94 | 374.49 |
| | | 04/05/16 | 19.29 | 375.14 |
| | | 06/06/16 | 18.11 | 376.32 |
| | | 08/09/16 | 21.41 | 373.02 |
| | | 10/17/16 | 22.51 | 371.92 |
| | | 12/11/16 | 23.04 | 371.39 |

TABLE 2
GROUNDWATER ELEVATION SUMMARY
PERMANENT DISPOSAL POND 5
MARTIN LAKE STEAM ELECTRIC STATION

| Well ID | TOC Elevation (ft amsl) | Date | Depth to Water (ft bgs) | Water Elevation (ft amsl) |
|---------|-------------------------|----------|-------------------------|---------------------------|
| PDP-24 | 389.73 | 10/20/15 | 25.62 | 364.11 |
| | | 12/14/15 | 24.94 | 364.79 |
| | | 02/24/16 | 24.76 | 364.97 |
| | | 04/05/16 | 24.51 | 365.22 |
| | | 06/06/16 | 23.87 | 365.86 |
| | | 08/09/16 | 22.61 | 367.12 |
| | | 10/17/16 | 22.08 | 367.65 |
| | | 12/11/16 | 24.19 | 365.54 |
| PDP-25 | 387.97 | 10/20/15 | 13.49 | 374.48 |
| | | 12/14/15 | 12.76 | 375.21 |
| | | 02/24/16 | 26.84 | 361.13 |
| | | 04/05/16 | 26.96 | 361.01 |
| | | 06/06/16 | 26.17 | 361.80 |
| | | 08/09/16 | 26.06 | 361.91 |
| | | 10/17/16 | 27.83 | 360.14 |
| | | 12/11/16 | 29.71 | 358.26 |
| PDP-26 | 397.68 | 10/20/15 | 31.24 | 366.44 |
| | | 12/14/15 | 30.67 | 367.01 |
| | | 02/24/16 | 30.11 | 367.57 |
| | | 04/05/16 | 29.89 | 367.79 |
| | | 06/06/16 | 29.06 | 368.62 |
| | | 08/09/16 | 29.54 | 368.14 |
| | | 10/17/16 | 30.57 | 367.11 |
| | | 12/11/16 | 32.81 | 364.87 |
| PDP-27 | 377.58 | 10/20/15 | 18.28 | 359.30 |
| | | 12/14/15 | 7.61 | 369.97 |
| | | 02/24/16 | 11.95 | 365.63 |
| | | 04/05/16 | 10.27 | 367.31 |
| | | 06/06/16 | 7.44 | 370.14 |
| | | 08/09/16 | 17.46 | 360.12 |
| | | 10/17/16 | 19.06 | 358.52 |
| | | 12/11/16 | 19.78 | 357.80 |
| PDP-28 | 368.62 | 10/20/15 | 13.68 | 354.94 |
| | | 12/14/15 | 13.68 | 354.94 |
| | | 02/24/16 | 10.75 | 357.87 |
| | | 04/05/16 | 9.61 | 359.01 |
| | | 06/06/16 | 11.74 | 356.88 |
| | | 08/09/16 | 10.91 | 357.71 |
| | | 10/17/16 | 12.19 | 356.43 |
| | | 12/11/16 | 13.09 | 355.53 |
| PDP-29 | 383.05 | 10/20/15 | 14.12 | 368.93 |
| | | 12/14/15 | 14.06 | 368.99 |
| | | 02/24/16 | 12.45 | 370.60 |
| | | 04/05/16 | 10.86 | 372.19 |
| | | 06/06/16 | 12.62 | 370.43 |
| | | 08/09/16 | 11.24 | 371.81 |
| | | 10/17/16 | 13.09 | 369.96 |
| | | 12/11/16 | 14.23 | 368.82 |

Notes:

1. Abbreviations: ft - feet; amsl - above mean sea level; bgs - below ground surface

**TABLE 3
SUMMARY OF AQUIFER TEST RESULTS
PERMANENT DISPOSAL POND 5
MARTIN LAKE STEAM ELECTRIC STATION**

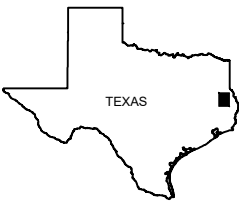
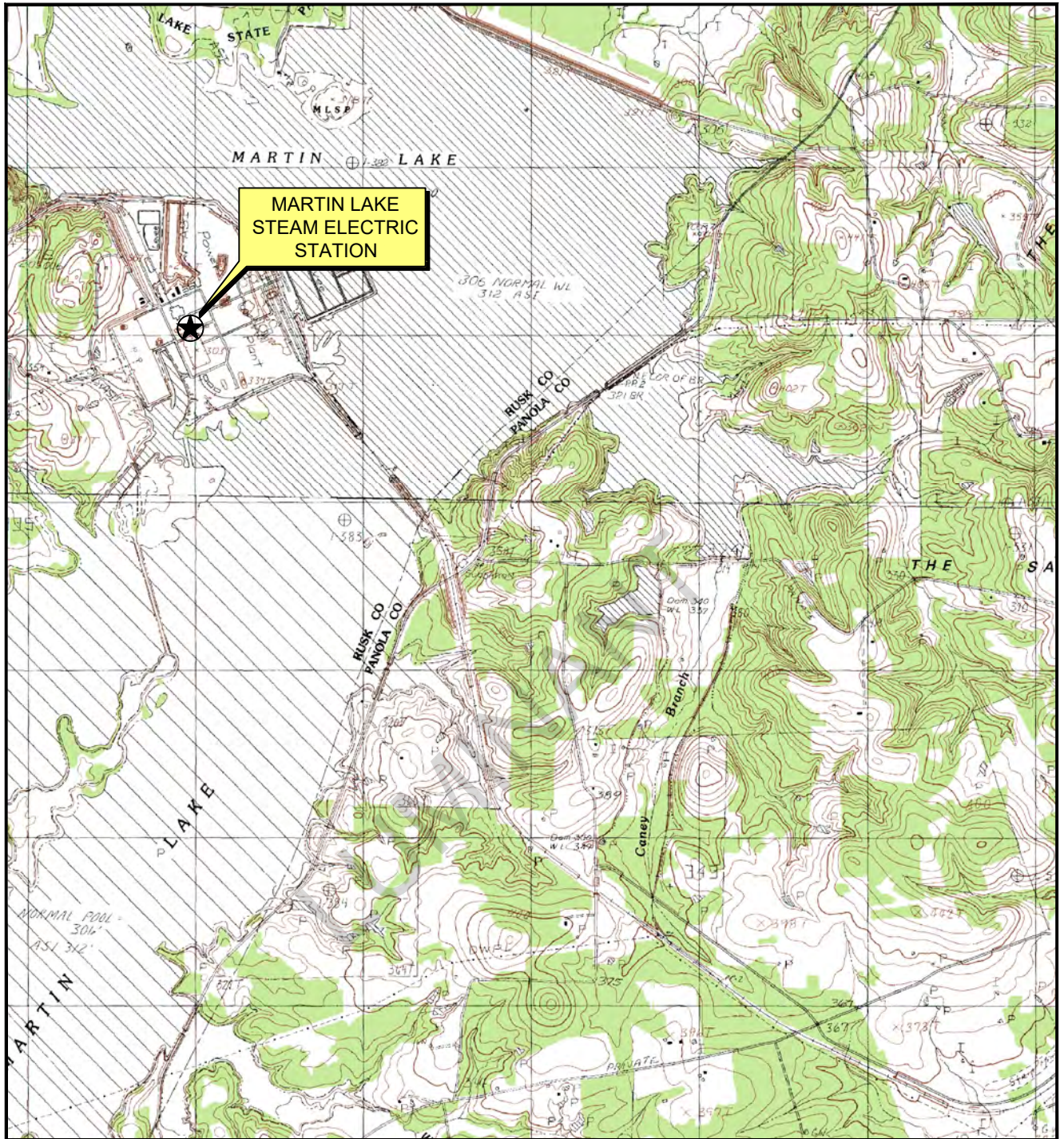
| Well ID | Test Type | Aquifer Type | Analysis Method | Saturated Thickness (feet) | Results | |
|---|-----------|--------------|-----------------|----------------------------|--------------------------|-----------------|
| | | | | | T (cm ² /sec) | K (cm/sec) |
| PDP 5 | | | | | | |
| PDP-22 | Slug-In | Unconfined | Bouwer-Rice | 22.84 | 3.04E-02 | 4.36E-05 |
| PDP-22 | Slug-Out | Unconfined | Bouwer-Rice | 22.84 | 4.16E-03 | 5.98E-06 |
| Mean | | | | | 1.73E-02 | 2.48E-05 |
| PDP-25 | Slug-In | Confined | Bouwer-Rice | 24 | 1.09E-01 | 1.49E-04 |
| PDP-25 | Slug-Out | Confined | Bouwer-Rice | 24 | 9.05E-02 | 1.24E-04 |
| Mean | | | | | 9.99E-02 | 1.37E-04 |
| PDP-26 | Slug-In | Confined | Bouwer-Rice | 8 | 8.31E-03 | 3.41E-05 |
| PDP-26 | Slug-Out | Confined | Bouwer-Rice | 8 | 3.95E-03 | 1.62E-05 |
| Mean | | | | | 6.13E-03 | 2.51E-05 |
| Geometric Mean for All PDP 5 Tests | | | | | 2.19E-02 | 4.40E-05 |

Notes:

- Abbreviations: T - transmissivity; K - hydraulic conductivity.

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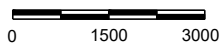
Figures



QUADRANGLE LOCATION



Scale in Feet



MARTIN LAKE STEAM ELECTRIC STATION
TATUM, TEXAS

Figure 1

PDP 5 AREA
SITE LOCATION MAP

PROJECT: 5123B

BY: AJD

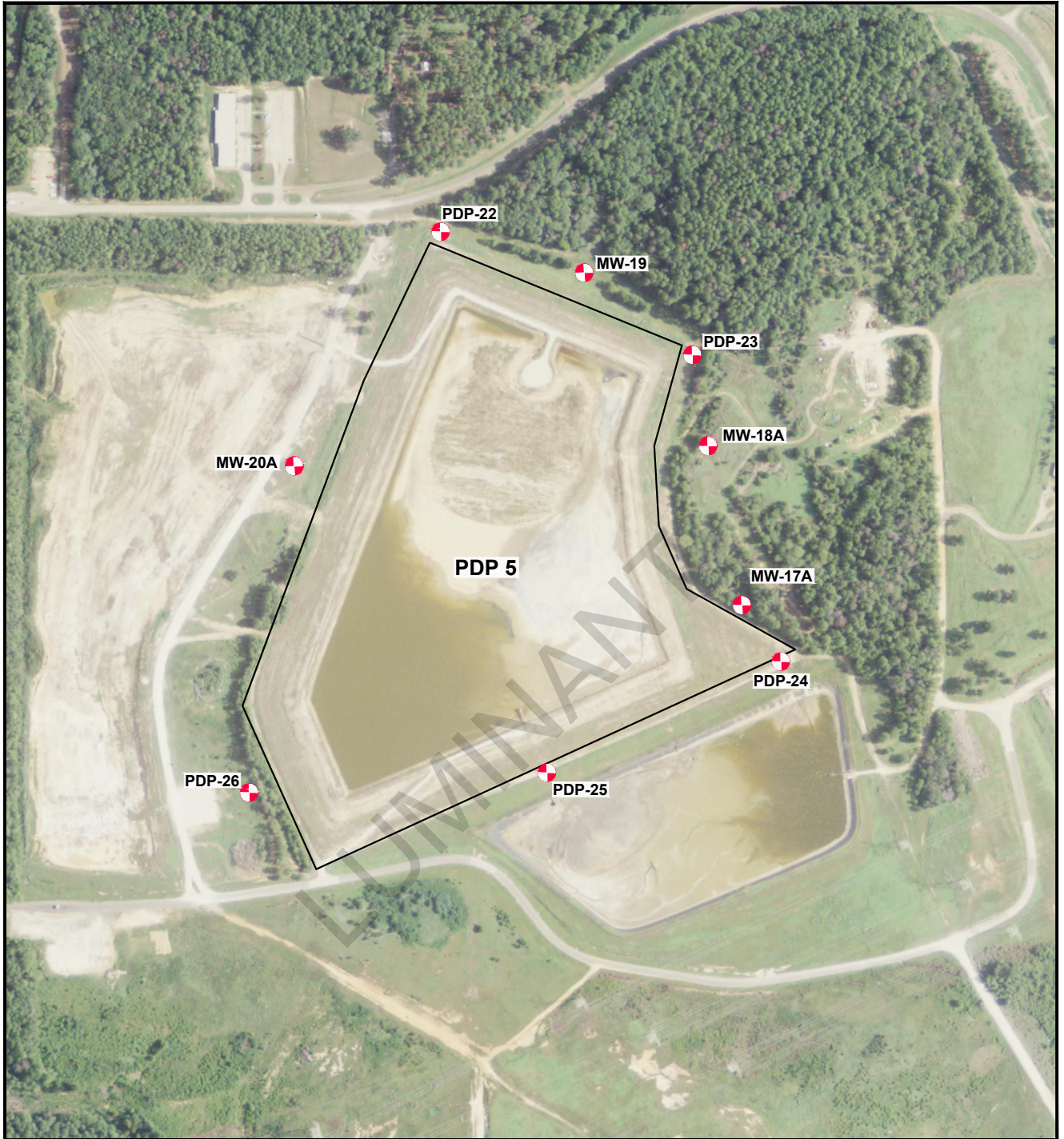
REVISIONS

DATE: JUNE, 2015

CHECKED: PJB

PASTOR, BEHLING & WHEELER, LLC
CONSULTING ENGINEERS AND SCIENTISTS

SOURCE:
Base map from www.tnris.gov, Tatum, TX 7.5 min. USGS quadrangle dated 1983.

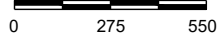


EXPLANATION

 CCR Monitoring Well



Scale in Feet



SOURCE:
Imagery from www.tnris.gov, Rusk County, aerial photographs, 2012.

MARTIN LAKE STEAM ELECTRIC STATION
TATUM, TEXAS

Figure 2

PDP 5 AREA
DETAILED SITE PLAN

PROJECT: 5164B

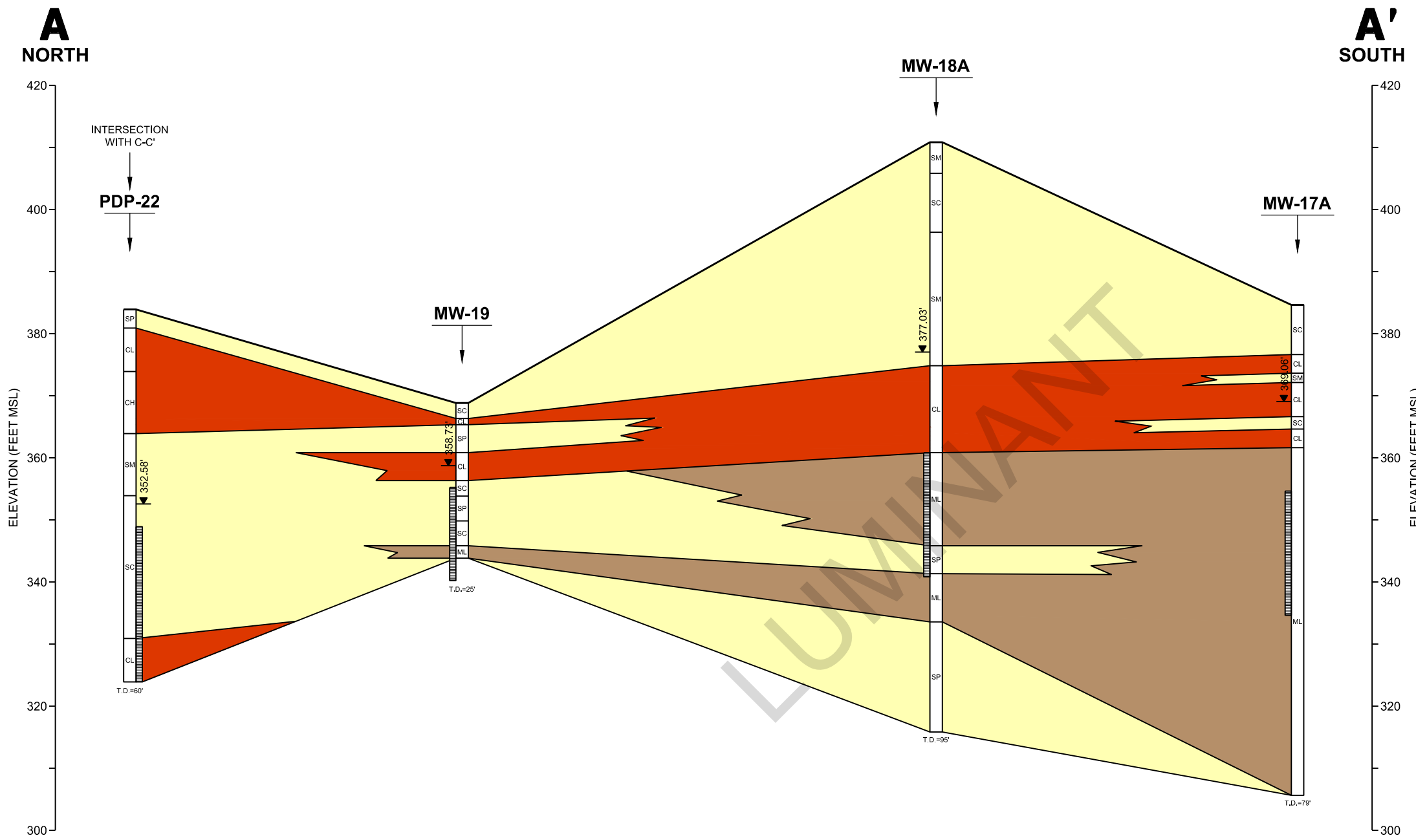
BY: AJD

REVISIONS

DATE: SEPT., 2017

CHECKED: PJB

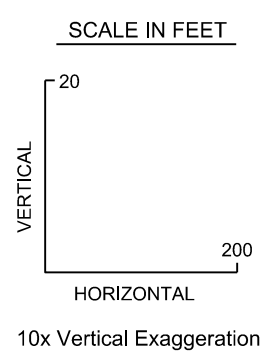
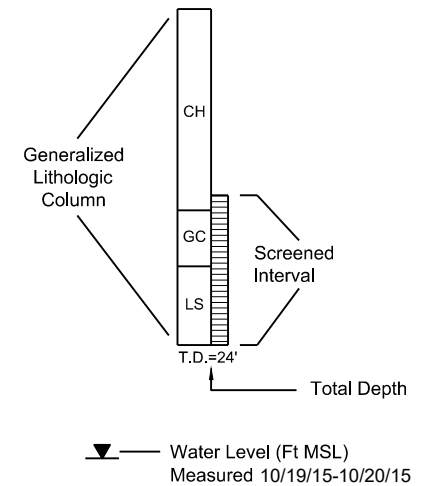
PASTOR, BEHLING & WHEELER, LLC
CONSULTING ENGINEERS AND SCIENTISTS



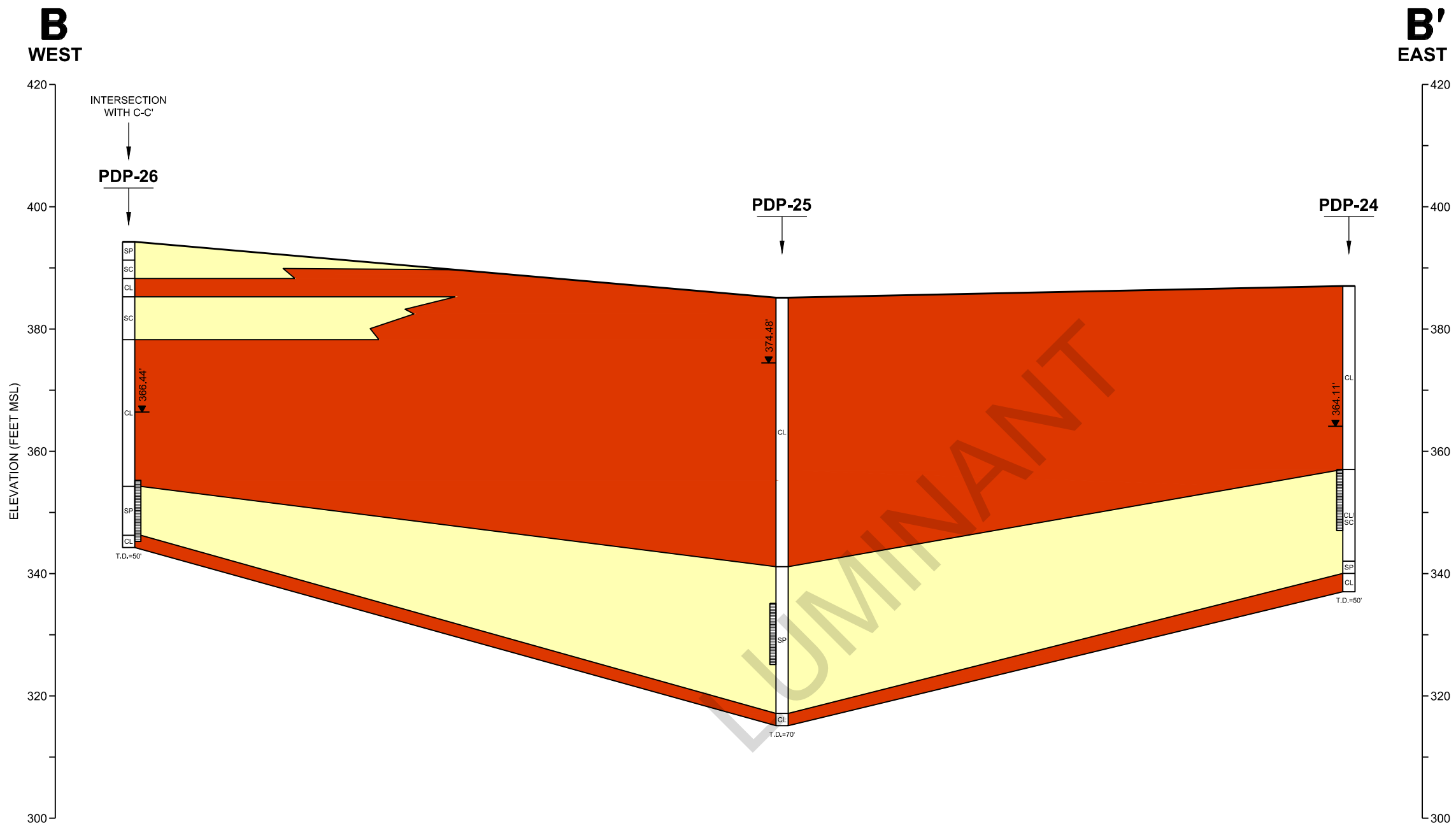
EXPLANATION

- SAND
- CLAY
- SILT

MONITORING WELL CONSTRUCTION



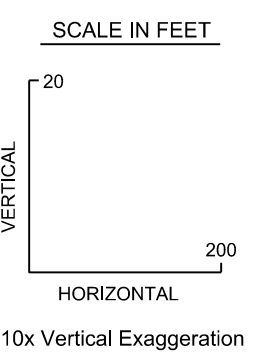
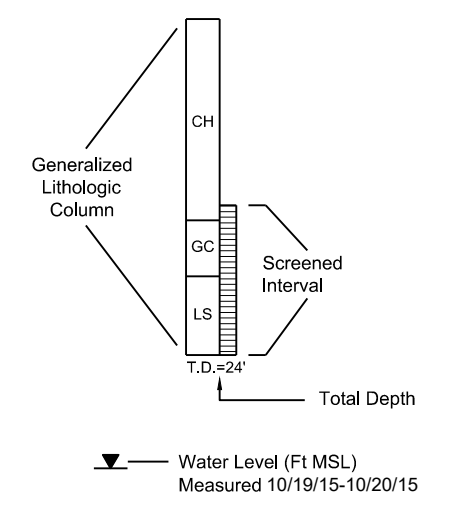
| | | |
|--|--------------|-----------|
| MARTIN LAKE STEAM ELECTRIC STATION TATUM, TEXAS | | |
| Figure 4 | | |
| PDP 5 AREA GEOLOGIC CROSS SECTION A-A' NORTH SIDE OF PDP5 | | |
| PROJECT: 5164B | AJD | REVISIONS |
| DATE: OCT., 2017 | CHECKED: PJB | |
| PASTOR, BEHLING & WHEELER, LLC CONSULTING ENGINEERS AND SCIENTISTS | | |



EXPLANATION

- SAND
- CLAY
- SILT

MONITORING WELL CONSTRUCTION



**MARTIN LAKE STEAM ELECTRIC STATION
TATUM, TEXAS**

Figure 5

**PDP 5 AREA
GEOLOGIC CROSS SECTION
B-B' SOUTH SIDE OF PDP 5**

| | | |
|------------------|--------------|-----------|
| PROJECT: 5164B | BY: AJD | REVISIONS |
| DATE: OCT., 2017 | CHECKED: PJB | |

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C
NORTH

ELEVATION (FEET MSL)
420
400
380
360
340
320

INTERSECTION
WITH A-A'
PDP-22

MW-20A

C'
SOUTH

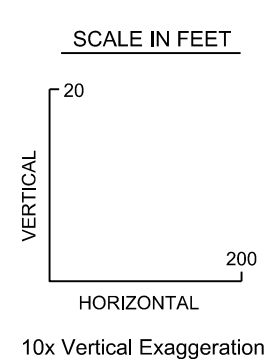
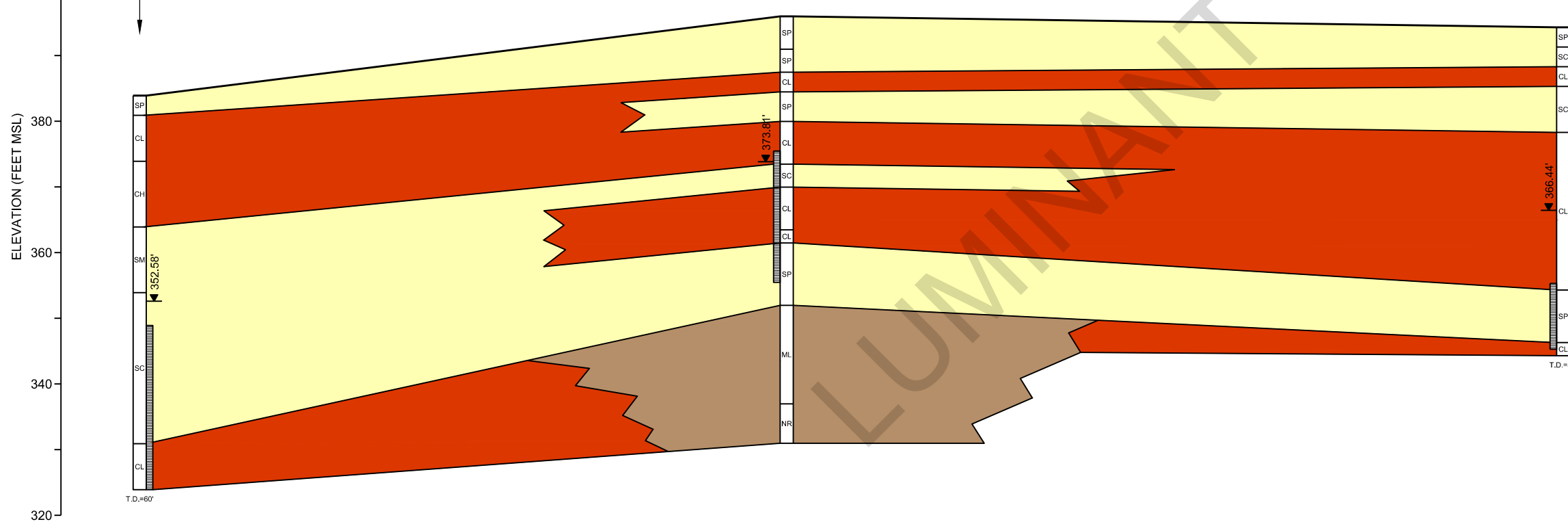
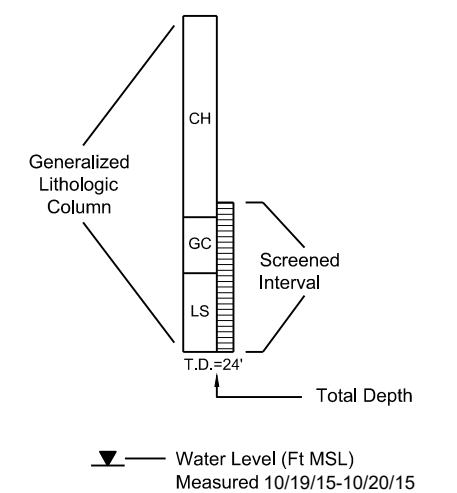
INTERSECTION
WITH B-B'
PDP-26

ELEVATION (FEET MSL)
420
400
380
360
340
320

EXPLANATION

- SAND
- CLAY
- SILT

MONITORING WELL CONSTRUCTION



MARTIN LAKE STEAM ELECTRIC STATION
TATUM, TEXAS

Figure 6

PDP 5 AREA
GEOLOGIC CROSS SECTION
C-C' WEST SIDE OF PDP 5

| | | |
|------------------|--------------|-----------|
| PROJECT: 5164B | BY: AJD | REVISIONS |
| DATE: OCT., 2017 | CHECKED: PJB | |

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Appendix A

CCR Monitoring Well Logs



BORING/WELL CONSTRUCTION LOG

| | |
|--------------------------------------|---|
| Project Number: 08-1388 | Boring/Well Number: MW-17A |
| Project Name: Martin Lake SES | Date Drilled: October 1, 2008 |
| Location: 8850 FM 2658 Tatum, TX | Casing Type/Diameter: PVC/2" ID |
| Drilling Method: HSA | Screen Type/Diameter: PVC/0.01" |
| Sampling Method: CT | Gravel Pack Type: 8/16 Grade Silica Sand |
| Ground Elevation: 384.63' msl | Grout Type: Bentonite Pellets |
| Top of Casing Elevation: 387.53' msl | Depth to Water/Date: 26.62' BTOC/10-09-2008 |
| Logged by: T. Ripley | Ground Water Elevation/Date: 360.91' msl/10-09-2008 |
| Remarks: | Drilling Co./Driller: SCI / M. Bridges |

| PID (ppm) | Blow Counts | Recovery (%) | Sampling Method | Sample | Depth (ft. BGL) | U.S.C.S | Graphic Log | Lithologic Description | Contact Depth | Well Diagram |
|-----------|-------------|--------------|-----------------|--------|-----------------|---------|-------------|---|---------------|--------------|
| NA | NA | NA | CT | NA | 10 | | | See MW-17B boring log for Lithologic Description | | |
| | | | | | 20 | | | | | |
| | | | | | 30 | | | | | |
| | | | | | 40 | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | 50 | | | | | |
| | | | | | | | | The boring was terminated and the well was set at 47' bgs. The well was completed with a protective stickup which requires approximately 3 feet of additional casing above grade. | 50.0 | |



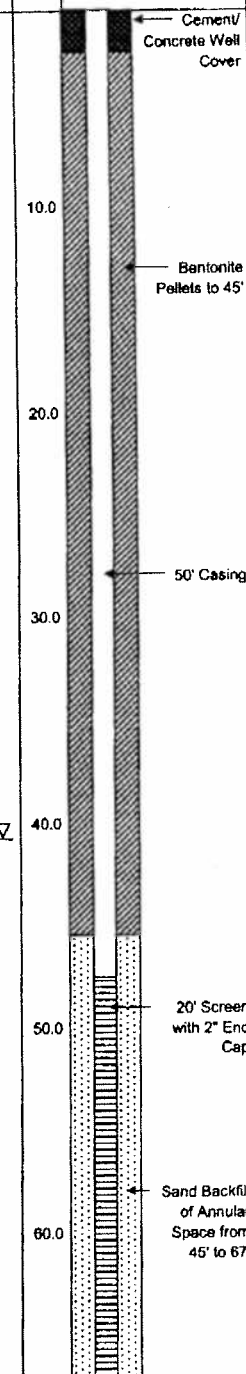
**GREEN STAR
ENVIRONMENTAL**

BORING/WELL CONSTRUCTION LOG

| | |
|--------------------------------------|---|
| Project Number: 08-1388 | Boring/Well Number: MW-18A |
| Project Name: Martin Lake SES | Date Drilled: October 2, 2008 |
| Location: 8850 FM 2658 Tatum, TX | Casing Type/Diameter: PVC/2" ID |
| Drilling Method: HSA | Screen Type/Diameter: PVC/0.01" |
| Sampling Method: CT | Gravel Pack Type: 8/16 Grade Silica Sand |
| Ground Elevation: 410.83' msl | Grout Type: Bentonite Pellets |
| Top of Casing Elevation: 414.43' msl | Depth to Water/Date: 43.17' BTCC/10-09-2008 |
| Logged by: T. Ripley | Ground Water Elevation/Date: 371.26' msl/10-09-2008 |
| Remarks: | Drilling Co./Driller: SCI / M. Bridges |

| PID (ppm) | Blow Counts | Recovery (%) | Sampling Method | Sample | Depth (ft. BGL) | U.S.C.S | Graphic Log | Lithologic Description | Contact Depth | Well Diagram |
|-----------|-------------|--------------|-----------------|--------|-----------------|---------|-------------|--|---------------|--------------|
| NA | NA | NA | CT | NA | | | | See MW-18B boring log for Lithologic Description | | |
| | | | | | 10 | | | | | |
| | | | | | 20 | | | | | |
| | | | | | 30 | | | | | |
| | | | | | 40 | | | | ▽ | |
| | | | | | 50 | | | | | |
| | | | | | 60 | | | | | |
| | | | | | 70 | | | | | |

LUMINANT



The boring was terminated and the well was set at 67' bgs. The well was completed with a protective stickup which requires approximately 3 feet of additional casing above grade.



BORING/WELL CONSTRUCTION LOG

| | |
|--------------------------------------|---|
| Project Number: 08-1388 | Boring/Well Number: MW-19 |
| Project Name: Martin Lake SES | Date Drilled: September 30, 2008 |
| Location: 8850 FM 2658 Tatum, TX | Casing Type/Diameter: PVC/2" ID |
| Drilling Method: HSA | Screen Type/Diameter: PVC/0.01" |
| Sampling Method: CT | Gravel Pack Type: 20/40 Grade Silica Sand |
| Ground Elevation: 367.84' msl | Grout Type: Bentonite Pellets |
| Top of Casing Elevation: 371.23' msl | Depth to Water/Date: 13.89' BTOC/10-09-2008 |
| Logged by: T. Ripley | Ground Water Elevation/Date: 357.34' msl/10-09-2008 |
| | Drilling Co./Driller: SCI / M. Bridges |

Remarks:

| PID (ppm) | Blow Counts | Recovery (%) | Sampling Method | Sample | Depth (ft BGL) | U.S.C.S | Graphic Log | Lithologic Description | Contact Depth | Well Diagram |
|--|-------------|--------------|-----------------|--------|----------------|---------|-------------|--|---------------|---|
| NA | NA | 90 | CT | NA | | SC | | Moist, medium dense, reddish-brown, CLAYEY SAND (fine-grained SAND) | | |
| | | | | | 5 | CL | | Moist, soft, reddish-brown, SANDY CLAY | 5.0 | |
| | | | | | | SP | | Moist, loose, reddish-brown, fine-grained SAND -gray | | 13' Casing |
| | | 60 | | | 10 | CL | | Moist to wet, soft, brown, SANDY CLAY (fine-grained SAND) -stiff -light gray | 10.0 | |
| | | | | | | CL | | Moist, very stiff, light gray, SILTY CLAY | | |
| | | 100 | | | 15 | SC | | Moist, dense, gray and reddish-brown, CLAYEY SAND (fine-grained SAND) | 15.0 | 15' Screen with 2" End Cap |
| | | | | | | SP | | Wet, loose, light gray and reddish-brown, fine-grained SAND -medium dense | | |
| | | 70 | | | 20 | SC | | Wet, medium dense, light gray and reddish-brown, CLAYEY SAND (fine-grained SAND) -stringer of dense -stringer of dense | 20.0 | Sand Backfill of Annular Space from 9' to 25' |
| | | 100 | | | 25 | ML | | Moist, very stiff, gray CLAYEY SILT with some iron staining | 25.0 | |
| <p>The boring was terminated and the well was set at 25' bgs. The well was completed with a protective stickup which requires approximately 3 feet of additional casing above grade.</p> | | | | | | | | | | |



GREEN STAR ENVIRONMENTAL

BORING/WELL CONSTRUCTION LOG

| | |
|--------------------------------------|---|
| Project Number: 08-1388 | Boring/Well Number: MW-20A |
| Project Name: Martin Lake SES | Date Drilled: September 30, 2008 |
| Location: 8850 FM 2658 Tatum, TX | Casing Type/Diameter: PVC/2" ID |
| Drilling Method: HSA | Screen Type/Diameter: PVC/0.01" |
| Sampling Method: CT | Gravel Pack Type: 20/40 Grade Silica Sand |
| Ground Elevation: 395.95' msl | Grout Type: Bentonite Pellets |
| Top of Casing Elevation: 398.34' msl | Depth to Water/Date: 29.19' BTOC/10-09-2008 |
| Logged by: T. Ripley | Ground Water Elevation/Date: 369.65' msl/10-09-2008 |
| Remarks: | Drilling Co./Driller: SCI / M. Bridges |

| PID (ppm) | Blow Counts | Recovery (%) | Sampling Method | Sample | Depth (ft. BGL) | U.S.C.S | Graphic Log | Lithologic Description | Contact Depth | Well Diagram |
|-----------|-------------|--------------|-----------------|--------|-----------------|---------|-------------|---|---------------|--------------|
| NA | NA | NA | CT | NA | | | | See MW-20B boring log for Lithologic Description | | |
| | | | | | 10 | | | | 10.0 | |
| | | | | | 20 | | | | 20.0 | |
| | | | | | 30 | | | | 30.0 | |
| | | | | | 40 | | | | 40.0 | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | The boring was terminated and the well was set at 41' bgs. The well was completed with a protective stickup which requires approximately 3 feet of additional casing above grade. | | |

Luminant

Log of Boring: PDP-22

| | | | | |
|---|--------------------|---------------------------|---------------------------|-------|
| Martin Lake Steam Electric Station Tatum, TX | Completion Date: | 9/9/2015 | Drilling Method: | Sonic |
| | Drilling Company: | Walker-Hill Environmental | Borehole Diameter (in.): | 6.5 |
| PBW Project No. 5164B | Driller: | Timmy Beach | Total Depth (ft): | 60 |
| | Driller's License: | 5814M | TOC Elevation (ft. AMSL): | |
| | Logged By: | Ryan Francis | Northing: | |
| | Sampling Method: | 4"x10' Core barrel | Easting: | |

| Depth (ft) | Well Materials | Recovery (ft/ft) | USCS | Lithologic Description |
|------------|----------------|------------------|------|--|
| 0 | | | SP | (0 - 3) Fine SAND, tan, dry, very soft, small iron concretions, grass roots |
| 4 | | 8.0/10.0 | CL | (3 - 10) Sandy CLAY, red/orange mottled, dry, firm, moderate cementation, flat to subrounded, sharp contact |
| 8 | | | | |
| 12 | | 10.0/10.0 | CH | (10 - 20) Silty CLAY with minor sand, dry, firm, moderate cementation, flat to subrounded, medium to high plasticity, micro laminated structure, increasing sand content with depth, transition from red/gray at 10' to tan at 20' |
| 16 | | | | |
| 20 | | 10.0/10.0 | SM | (20 - 28) Sandy SILT, gray and tan, dry, firm, moderate cementation, flat to subrounded, grass lense (fill), transition to gray at 26' |
| 24 | | | | |
| 28 | | | | (28 - 30) Silty SAND, iron-rich, dry, soft, weak cementation, subrounded, sharp contact |
| 32 | | 10.0/10.0 | | |
| 36 | | | | |
| 40 | | | SC | (30 - 53) SAND, gray with small streaks and iron at 32', moist to wet, soft, moderate plasticity at 30', transition to low plasticity at 40', minor clay content |
| 44 | | 10.0/10.0 | | |
| 48 | | | | |
| 52 | | | | |
| 56 | | 10.0/10.0 | CL | (53 - 60) Silty CLAY, gray, dry, firm, moderate cementation, dry, flat, transition to very hard gray/dark gray clay at 56' |
| 60 | | | | |

PBW

Pastor, Behling & Wheeler, LLC
 2201 Double Creek Dr., Suite 4004
 Round Rock, TX 78664
 Tel (512) 671-3434 Fax (512) 671-3446

Notes:

1. This log should not be used separately from the report to which it is attached.

Well Materials

(0-35) Casing, 2" Sch 40 FJT PVC
 (35-60) Screen, 2" Sch 40 FJT PVC, 0.010" slot

Annular Materials

(0'-31') Grout
 (31'-33') Bentonite pellets
 (33'-60') 20/40 sand

Luminant

Log of Boring: PDP-23

| | | | | |
|---|--------------------|---------------------------|---------------------------|-------|
| Martin Lake Steam Electric Station Tatum, TX | Completion Date: | 9/10/2015 | Drilling Method: | Sonic |
| | Drilling Company: | Walker-Hill Environmental | Borehole Diameter (in.): | 6.5 |
| PBW Project No. 5164B | Driller: | Timmy Beach | Total Depth (ft): | 50 |
| | Driller's License: | 5814M | TOC Elevation (ft. AMSL): | |
| | Logged By: | Ryan Francis | Northing: | |
| | Sampling Method: | 4"x10' Core barrel | Easting: | |

| Depth (ft) | Well Materials | Recovery (ft/ft) | USCS | Lithologic Description |
|------------|----------------|------------------|------|--|
| 0 | | | | |
| 4 | | 10.0/10.0 | | |
| 8 | | | | |
| 12 | | | | |
| 16 | | 10.0/10.0 | | (0 - 30) Sandy CLAY, brown to red to tan, dry, soft to firm, weak cementation, iron rich at 5', none to moderate plasticity, black mottling and some organics present at 10', iron banding and iron nodules with increasing sand content at 16', microlaminated iron rich banded gray, tan, and red sandy clay (21' - 30') |
| 20 | | | CL | |
| 24 | | 10.0/10.0 | | |
| 28 | | | | |
| 32 | | | | |
| 36 | | 10.0/10.0 | | (30 - 39) CLAY, gray, micro laminated, minor sand content, dry, firm to hard, weak to moderate cementation, low plasticity |
| 40 | | | | (39 - 41) Sandy CLAY, light gray, dry, firm, weak cementation, medium plasticity |
| 44 | | | SC | (41 - 44) Clayey SAND, wet, soft, weak cementation, subrounded, medium to high plasticity |
| 48 | | 10.0/10.0 | CL | (44 - 50) Sandy CLAY, dark gray, dry, hard, moderate cementation |
| 52 | | | | |

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Notes:

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Well Materials

(0-35) Casing, 2" Sch 40 FJT PVC
 (35-45) Screen, 2" Sch 40 FJT PVC, 0.010" slot

Annular Materials

(0'-31') Grout
 (31'-33') Bentonite pellets
 (33'-45') 20/40 sand

Luminant

Log of Boring: PDP-24

| | | | | |
|---|--------------------|---------------------------|---------------------------|-------|
| Martin Lake Steam Electric Station Tatum, TX | Completion Date: | 9/11/2015 | Drilling Method: | Sonic |
| | Drilling Company: | Walker-Hill Environmental | Borehole Diameter (in.): | 6.5 |
| PBW Project No. 5164B | Driller: | Timmy Beach | Total Depth (ft): | 50 |
| | Driller's License: | 5814M | TOC Elevation (ft. AMSL): | |
| | Logged By: | Ryan Francis | Northing: | |
| | Sampling Method: | 4"x10' Core barrel | Easting: | |

| Depth (ft) | Well Materials | Recovery (ft/ft) | USCS | Lithologic Description |
|------------|----------------|------------------|-------|--|
| 0 | | | | |
| 4 | | 8.0/10.0 | | |
| 8 | | | | |
| 12 | | | | |
| 16 | | 7.0/10.0 | CL | (0 - 30) Sandy CLAY, red and tan mottling, fine sand, dry to moist, firm, weak cementation, low to medium plasticity, occasional black inclusions, minor very fine sand content in gray and orange clay and high plasticity (20'-30') |
| 20 | | | | |
| 24 | | 10.0/10.0 | | |
| 28 | | | | |
| 32 | | | | |
| 36 | | 10.0/10.0 | CL/SC | (30 - 45) Sandy CLAY/Clayey SAND, gray, moist to wet, very fine grained, firm, weak cementation, medium plasticity, softens and increasing wetness with depth (35'-39'), brown with increased iron content (39'-42'), dark gray, dry, and none to low plasticity (39'-45') |
| 40 | | | | |
| 44 | | 10.0/10.0 | SP | (45 - 47) Clayey SAND, wet, soft, weak cementation, medium to high plasticity |
| 48 | | | CL | (47 - 50) Sandy CLAY, dark gray, fine grained, dry, firm to hard, weak cementation |
| 52 | | | | |

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Notes:

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Well Materials

(0-30) Casing, 2" Sch 40 FJT PVC
(30-40) Screen, 2" Sch 40 FJT PVC, 0.010" slot

Annular Materials

(0'-26') Grout
(26'-28') Bentonite pellets
(28'-40') 20/40 sand

Luminant

Log of Boring: PDP-25

| | | | | |
|---|--------------------|---------------------------|---------------------------|-------|
| Martin Lake Steam Electric Station Tatum, TX | Completion Date: | 9/11/2015 | Drilling Method: | Sonic |
| | Drilling Company: | Walker-Hill Environmental | Borehole Diameter (in.): | 6.5 |
| PBW Project No. 5164B | Driller: | Timmy Beach | Total Depth (ft): | 70 |
| | Driller's License: | 5814M | TOC Elevation (ft. AMSL): | |
| | Logged By: | Ryan Francis | Northing: | |
| | Sampling Method: | 4"x10' Core barrel | Easting: | |

| Depth (ft) | Well Materials | Recovery (ft/ft) | USCS | Lithologic Description |
|------------|----------------|------------------|------|--|
| 0 | | | | |
| 4 | | 10.0/10.0 | | |
| 8 | | | | |
| 12 | | | | |
| 16 | | 10.0/10.0 | | |
| 20 | | | | |
| 24 | | 10.0/10.0 | CL | (0 - 44) Sandy CLAY, red to gray and tan, very fine grained, dry to moist, firm, low to medium plasticity, weak to moderate cementation, micro laminated, minor organics, variable sand content with depth, high plasticity and very low sand content (22'-23'), higher sand content and high iron content with occasional subrounded pebbles (27'-30'), red, orange, tan, and gray mottling (30'-44') |
| 28 | | | | |
| 32 | | | | |
| 36 | | 10.0/10.0 | | |
| 40 | | | | |
| 44 | | 10.0/10.0 | | |
| 48 | | | | |
| 52 | | | | |
| 56 | | 10.0/10.0 | SP | (44 - 68) Clayey SAND, gray, moist, soft to firm, minor orange streaking, low plasticity, weak cementation, subrounded, minor wet and soft clay zone (62'-64') |
| 60 | | | | |
| 64 | | 10.0/10.0 | | |
| 68 | | | | |
| 72 | | | CL | (68 - 70) CLAY, black, minor silt, dry, very hard, moderate cementation, smooth shiny surface when fractured |

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Notes:

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Well Materials

(0-50) Casing, 2" Sch 40 FJT PVC
 (50-60) Screen, 2" Sch 40 FJT PVC, 0.010" slot

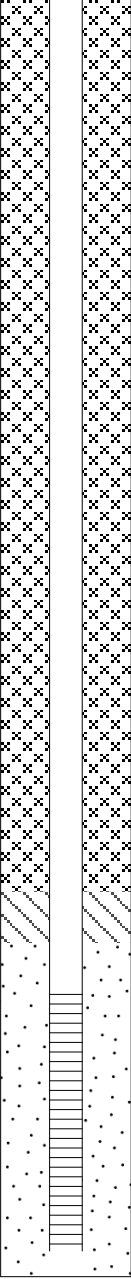
Annular Materials

(0'-46') Grout
 (46'-48') Bentonite pellets
 (48'-60') 20/40 sand

Luminant

Log of Boring: PDP-26

| | | | | |
|---|--------------------|---------------------------|---------------------------|-------|
| Martin Lake Steam Electric Station Tatum, TX | Completion Date: | 9/9/2015 | Drilling Method: | Sonic |
| | Drilling Company: | Walker-Hill Environmental | Borehole Diameter (in.): | 6.5 |
| PBW Project No. 5164B | Driller: | Timmy Beach | Total Depth (ft): | 50 |
| | Driller's License: | 5814M | TOC Elevation (ft. AMSL): | |
| | Logged By: | Ryan Francis | Northing: | |
| | Sampling Method: | 4"x10' Core barrel | Easting: | |

| Depth (ft) | Well Materials | Recovery (ft/ft) | USCS | Lithologic Description | |
|------------|--|------------------|--|---|--|
| 0 |  | 10.0/10.0 | SP | (0 - 3) SAND, tan, dry, very soft, weak cementation | |
| 4 | | | SC | (3 - 6) Clayey SAND, dry, firm, black lignite present | |
| 8 | | | CL | (6 - 9) CLAY with minor sand, red, moist, firm, medium plasticity, smear zone black lignite | |
| 12 | | | SC | (9 - 16) Clayey SAND, tan, moist, soft, low plasticity, more clay content with depth | |
| 16 | | | CL | 10.0/10.0 | (16 - 40) CLAY, tan, micro laminated orange and gray, moist, soft, medium plasticity, dry and silty clay (19'-27'), micro laminated gray and dark gray (27'-36'), increasing sand content (30'-36'), organics layer (36.5'-37'), high iron content (39'-40') |
| 20 | | | | | |
| 24 | | | | | |
| 28 | | | | | |
| 32 | | | SP | 10.0/10.0 | (40 - 48) SAND, tan, medium, moist to wet, soft, subrounded |
| 36 | | | | | |
| 40 | CL | 10.0/10.0 | (48 - 50) CLAY, gray, micro laminated, dry, firm, moderate cementation | | |
| 44 | | | | | |
| 48 | | | | | |
| 52 | | | | | |

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Notes:

1. This log should not be used separately from the report to which it is attached.

Well Materials

(0-39) Casing, 2" Sch 40 FJT PVC
 (39-49) Screen, 2" Sch 40 FJT PVC, 0.010" slot

Annular Materials

(0'-35') Grout
 (35'-37') Bentonite pellets
 (37'-49') 20/40 sand

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Appendix B

Photographs of CCR Groundwater Monitoring Wells

**Appendix B – Photographs of CCR Groundwater Monitoring Wells
Martin Lake Steam Electric Station – PDP 5 Area**



Photograph 1: PDP22



Photograph 2: PDP23

**Appendix B – Photographs of CCR Groundwater Monitoring Wells
Martin Lake Steam Electric Station – PDP 5 Area**



Photograph 3: PDP24



Photograph 4: PDP25

**Appendix B – Photographs of CCR Groundwater Monitoring Wells
Martin Lake Steam Electric Station – PDP 5 Area**



Photograph 5: PDP26



Photograph 6: MW-17A

**Appendix B – Photographs of CCR Groundwater Monitoring Wells
Martin Lake Steam Electric Station – PDP 5 Area**



Photograph 7: MW-18A



Photograph 8: MW-19

**Appendix B – Photographs of CCR Groundwater Monitoring Wells
Martin Lake Steam Electric Station – PDP 5 Area**



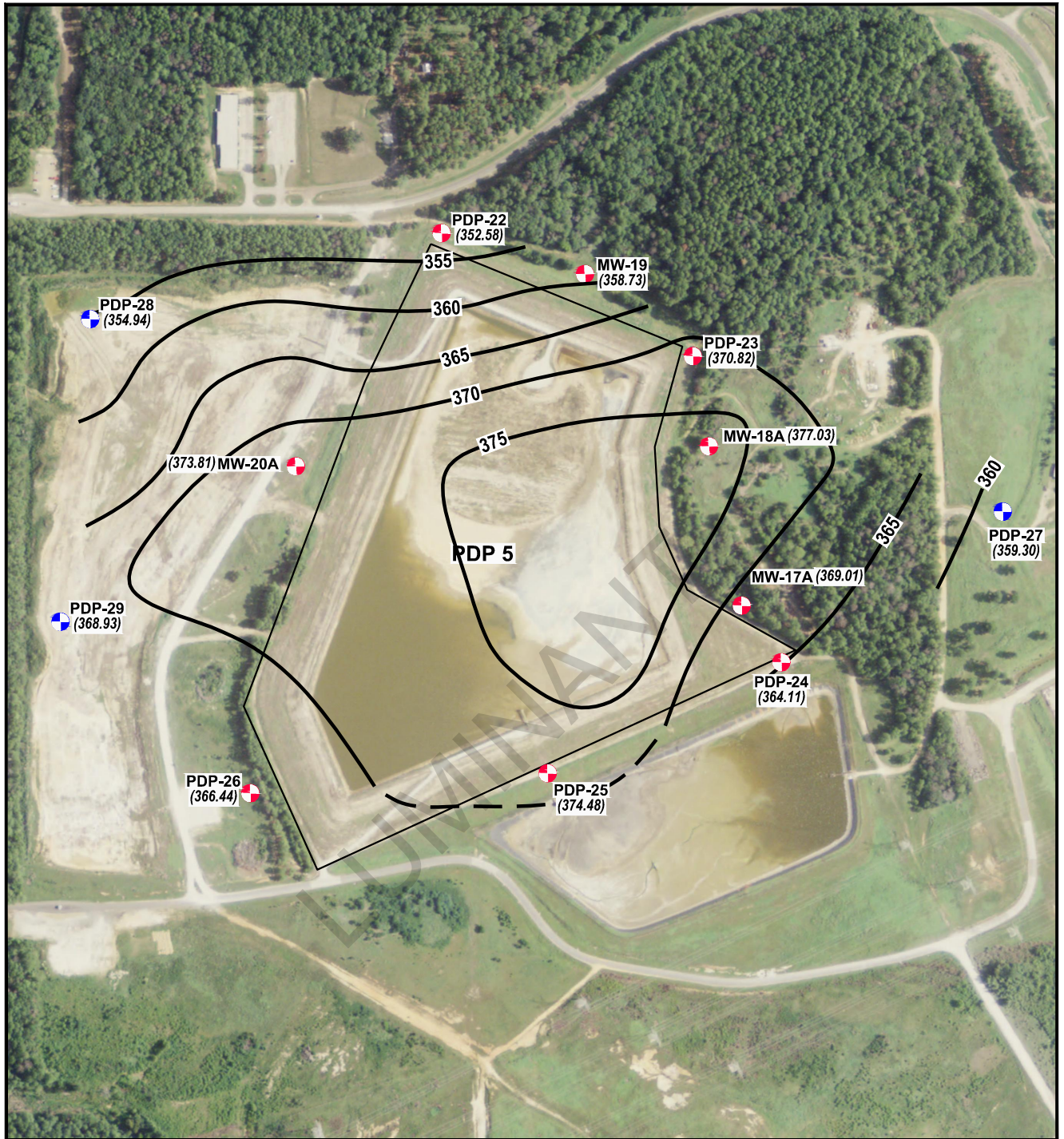
Photograph 9: MW-20A

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

LUMINANT

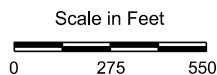
Appendix C

Groundwater Potentiometric Surface Maps



EXPLANATION

-  CCR Monitoring Well Location
-  Non-CCR Monitoring Well Used to Further Evaluate Groundwater Flow Direction
-  (374.34) Groundwater Potentiometric Surface (ft. MSL)
-  — 360 — Groundwater Potentiometric Surface Contour (C.I. = 5 ft.)



SOURCE:
Imagery from www.tnris.gov, Rusk County, aerial photographs, 2012.

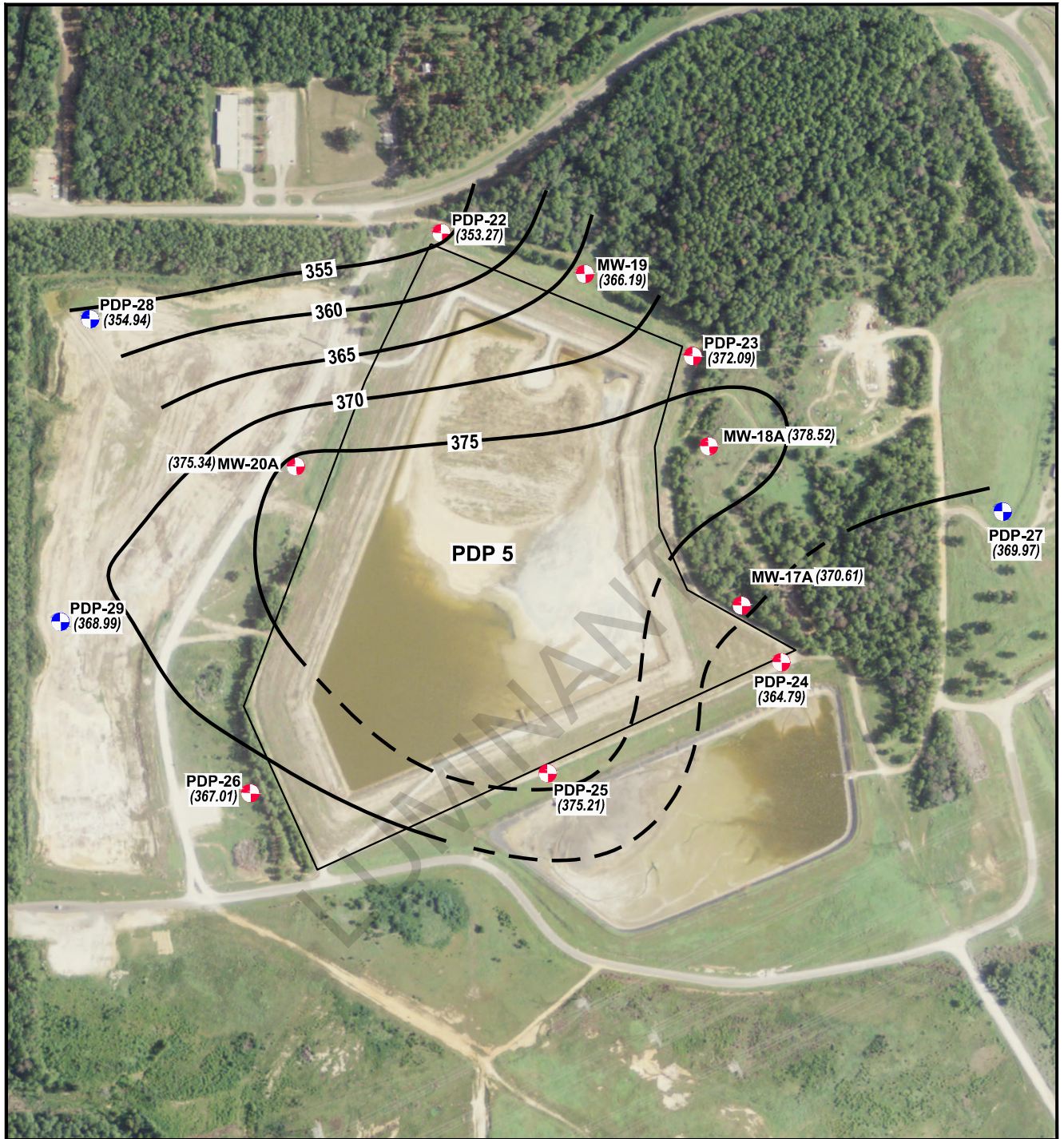
**MARTIN LAKE STEAM ELECTRIC STATION
TATUM, TEXAS**

Figure 1



**PDP 5 - GROUNDWATER ZONE A
POTENTIOMETRIC SURFACE MAP
OCTOBER 20, 2015**

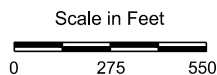
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|-------------------|--------------|-----------|
| PROJECT: 5164B | BY: AJD | REVISIONS |
| DATE: SEPT., 2017 | CHECKED: PJB | |

PASTOR, BEHLING & WHEELER, LLC
CONSULTING ENGINEERS AND SCIENTISTS



EXPLANATION

-  CCR Monitoring Well Location
-  Non-CCR Monitoring Well Used to Further Evaluate Groundwater Flow Direction
- (374.34) Groundwater Potentiometric Surface (ft. MSL)
- 360 — Groundwater Potentiometric Surface Contour (C.I. = 5 ft.)



SOURCE:
Imagery from www.tnris.gov, Rusk County, aerial photographs, 2012.

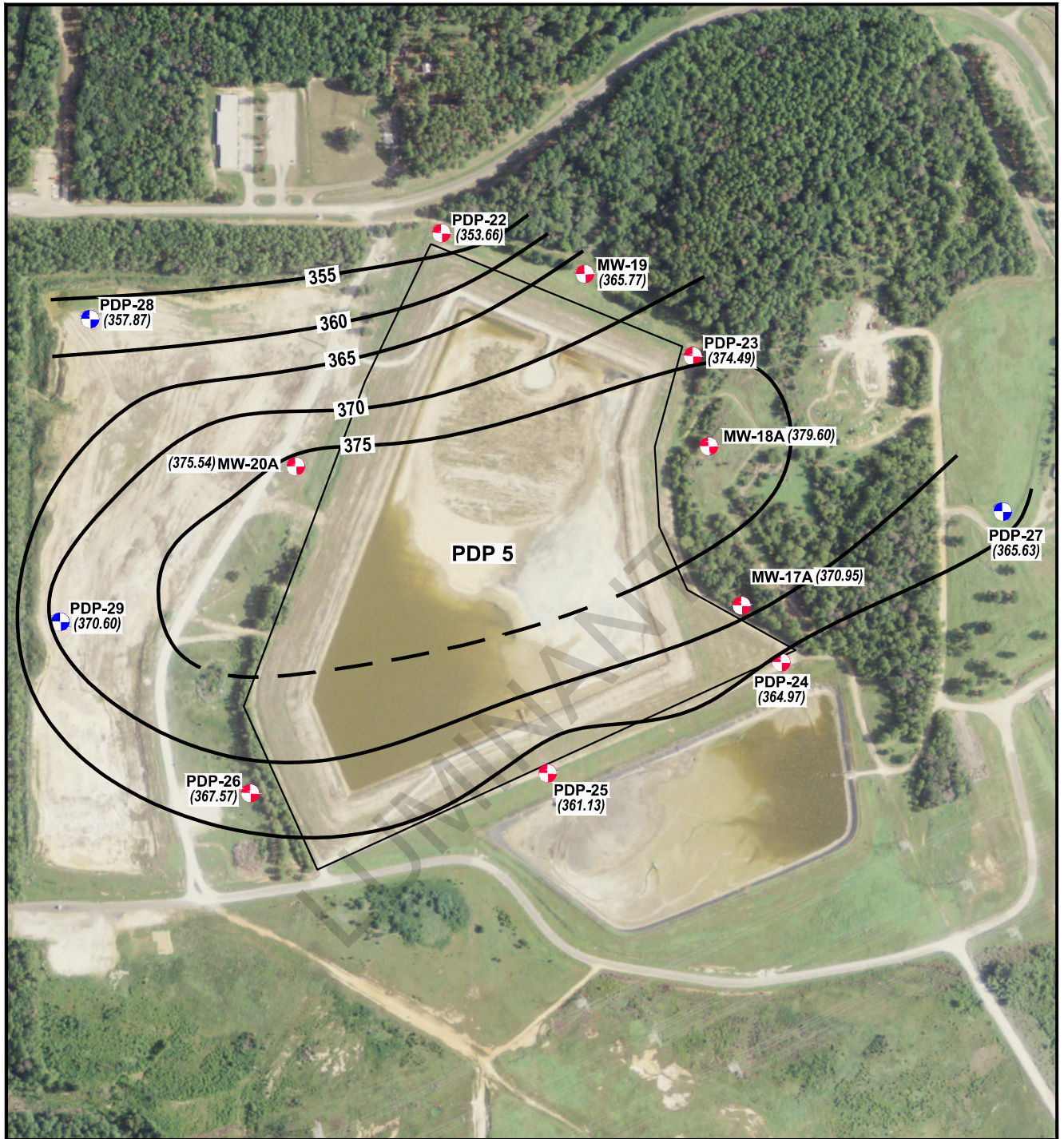
**MARTIN LAKE STEAM ELECTRIC STATION
TATUM, TEXAS**

Figure 2



**PDP 5 - GROUNDWATER
ZONE A POTENTIOMETRIC
SURFACE MAP - DEC. 14, 2015**

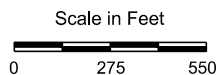
| | | |
|-------------------|--------------|-----------|
| PROJECT: 5164B | BY: AJD | REVISIONS |
| DATE: SEPT., 2017 | CHECKED: PJB | |

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CONSULTING ENGINEERS AND SCIENTISTS



EXPLANATION

-  CCR Monitoring Well Location
-  Non-CCR Monitoring Well Used to Further Evaluate Groundwater Flow Direction
- (374.34) Groundwater Potentiometric Surface (ft. MSL)
- 360 — Groundwater Potentiometric Surface Contour (C.I. = 5 ft.)



SOURCE:
Imagery from www.tnris.gov, Rusk County, aerial photographs, 2012.

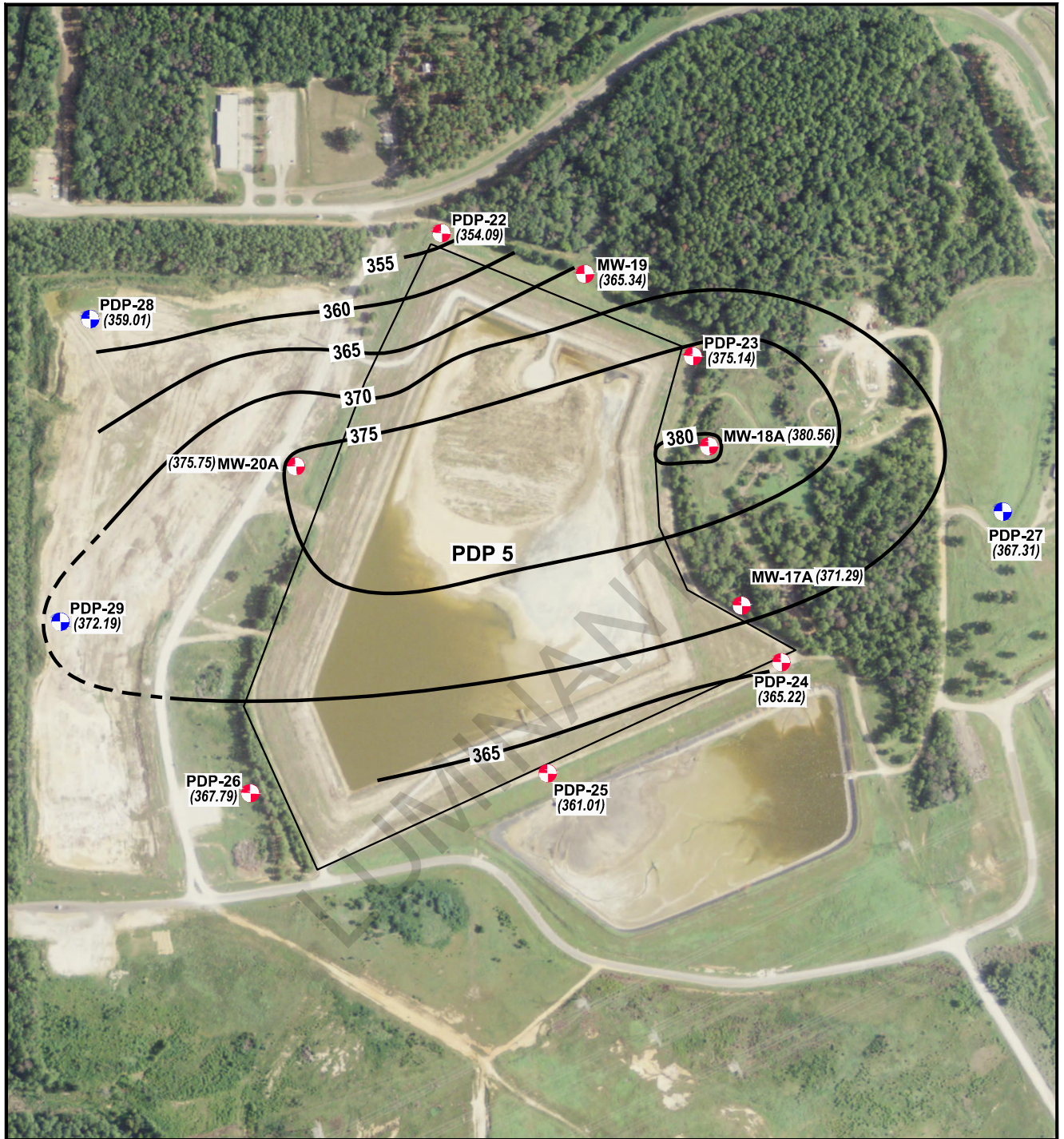
**MARTIN LAKE STEAM ELECTRIC STATION
TATUM, TEXAS**

Figure 3



**PDP 5 - GROUNDWATER
ZONE A POTENTIOMETRIC
SURFACE MAP - FEB. 24, 2016**

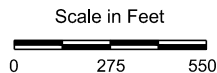
| | | |
|-------------------|--------------|-----------|
| PROJECT: 5164B | BY: AJD | REVISIONS |
| DATE: SEPT., 2017 | CHECKED: PJB | |

PASTOR, BEHLING & WHEELER, LLC
CONSULTING ENGINEERS AND SCIENTISTS



EXPLANATION

-  CCR Monitoring Well Location
-  Non-CCR Monitoring Well Used to Further Evaluate Groundwater Flow Direction
- (374.34) Groundwater Potentiometric Surface (ft. MSL)
- 360 — Groundwater Potentiometric Surface Contour (C.I. = 5 ft.)



SOURCE:
Imagery from www.tnris.gov, Rusk County, aerial photographs, 2012.

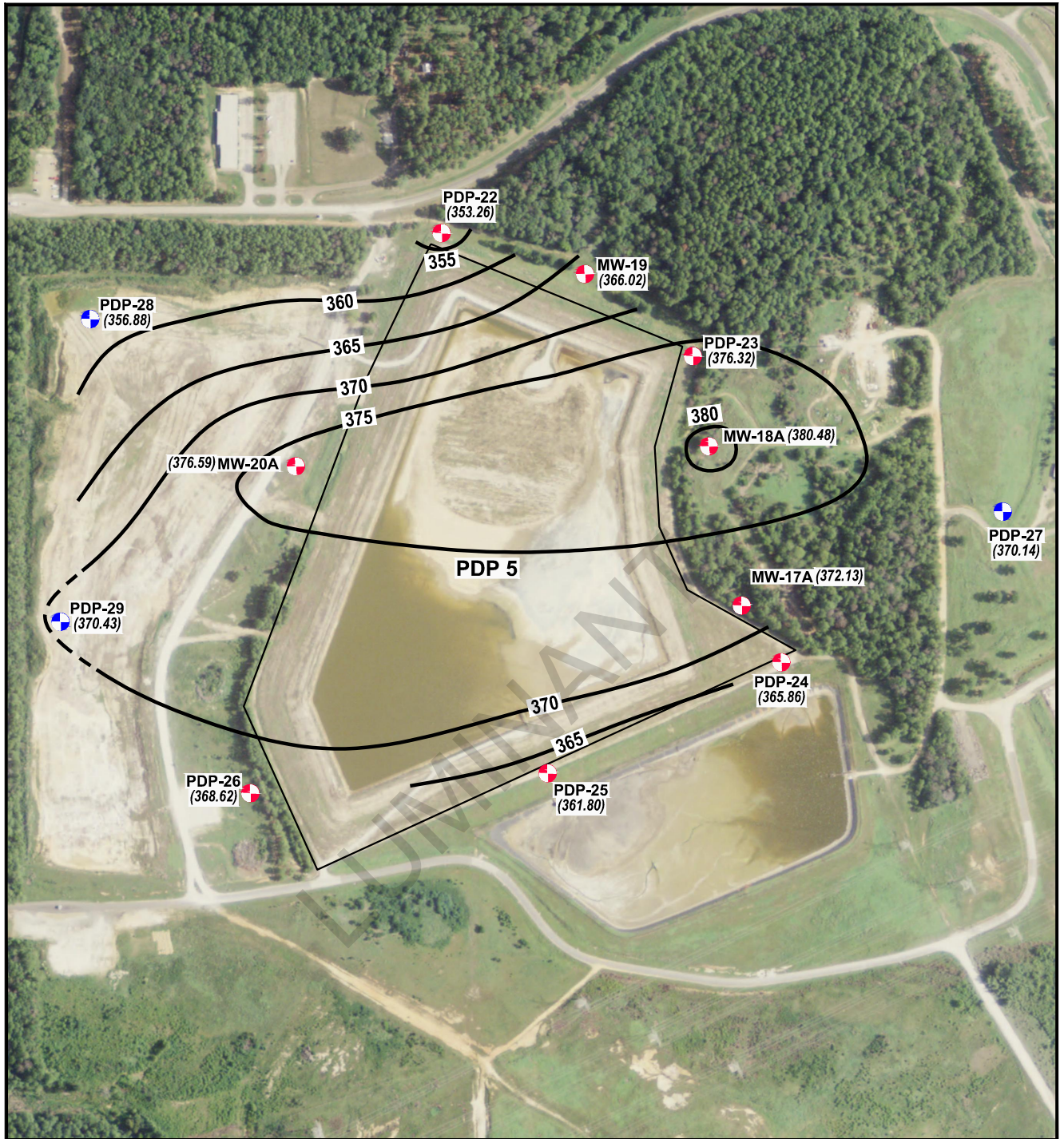
**MARTIN LAKE STEAM ELECTRIC STATION
TATUM, TEXAS**

Figure 4



**PDP 5 - GROUNDWATER
ZONE A POTENTIOMETRIC
SURFACE MAP - APRIL 5, 2016**

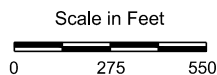
| | | |
|-------------------|--------------|-----------|
| PROJECT: 5164B | BY: AJD | REVISIONS |
| DATE: SEPT., 2017 | CHECKED: PJB | |

PASTOR, BEHLING & WHEELER, LLC
CONSULTING ENGINEERS AND SCIENTISTS



EXPLANATION

-  CCR Monitoring Well Location
-  Non-CCR Monitoring Well Used to Further Evaluate Groundwater Flow Direction
- (374.34) Groundwater Potentiometric Surface (ft. MSL)
- 360 — Groundwater Potentiometric Surface Contour (C.I. = 5 ft.)



SOURCE:
Imagery from www.tnris.gov, Rusk County, aerial photographs, 2012.

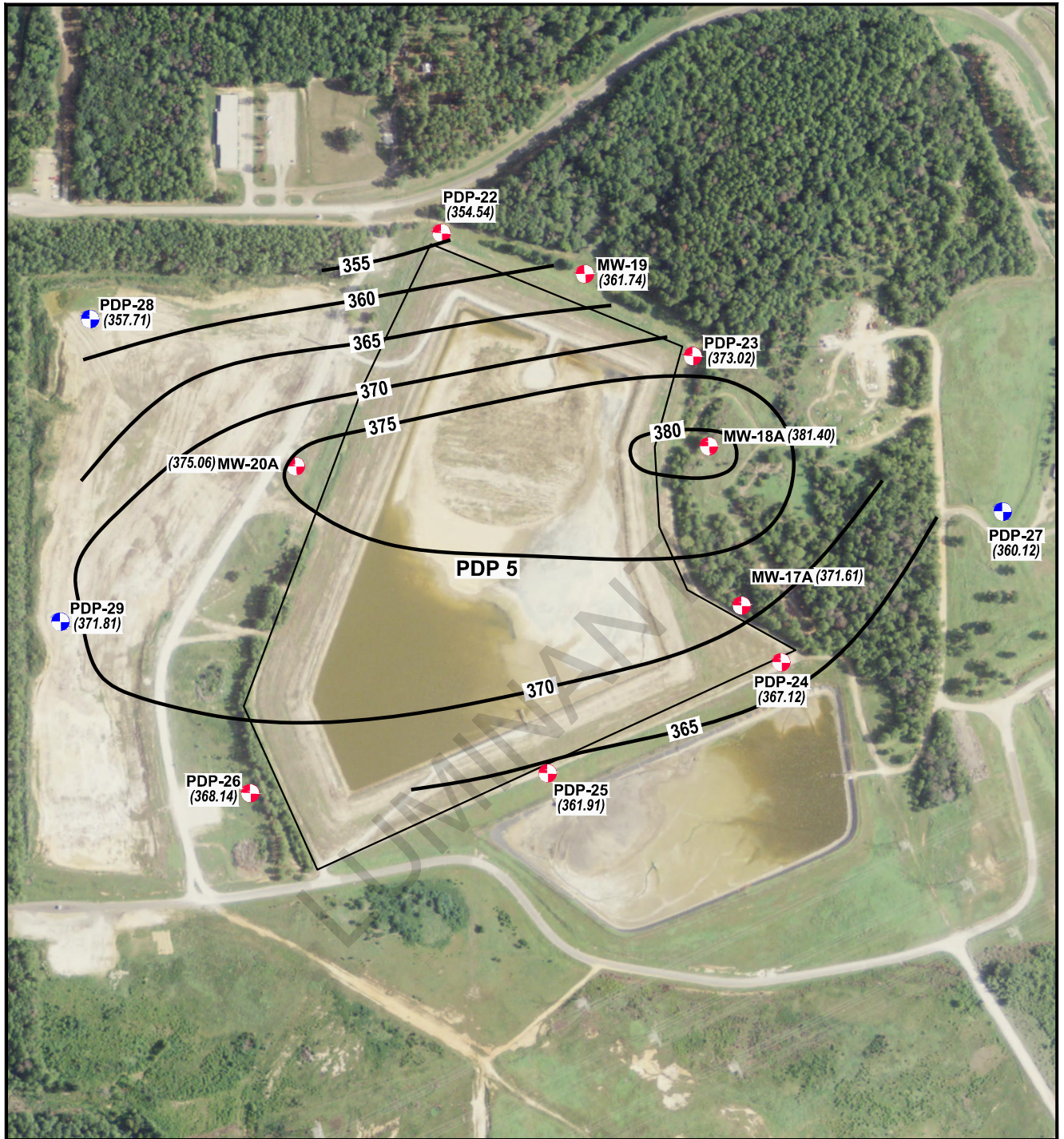
**MARTIN LAKE STEAM ELECTRIC STATION
TATUM, TEXAS**

Figure 5



**PDP 5 - GROUNDWATER
ZONE A POTENTIOMETRIC
SURFACE MAP - JUNE 6, 2016**

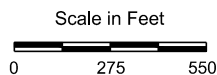
| | | |
|-------------------|--------------|-----------|
| PROJECT: 5164B | BY: AJD | REVISIONS |
| DATE: SEPT., 2017 | CHECKED: PJB | |

PASTOR, BEHLING & WHEELER, LLC
CONSULTING ENGINEERS AND SCIENTISTS



EXPLANATION

-  CCR Monitoring Well Location
-  Non-CCR Monitoring Well Used to Further Evaluate Groundwater Flow Direction
- (374.34) Groundwater Potentiometric Surface (ft. MSL)
- 360 — Groundwater Potentiometric Surface Contour (C.I. = 5 ft.)



SOURCE:
Imagery from www.tnris.gov, Rusk County, aerial photographs, 2012.

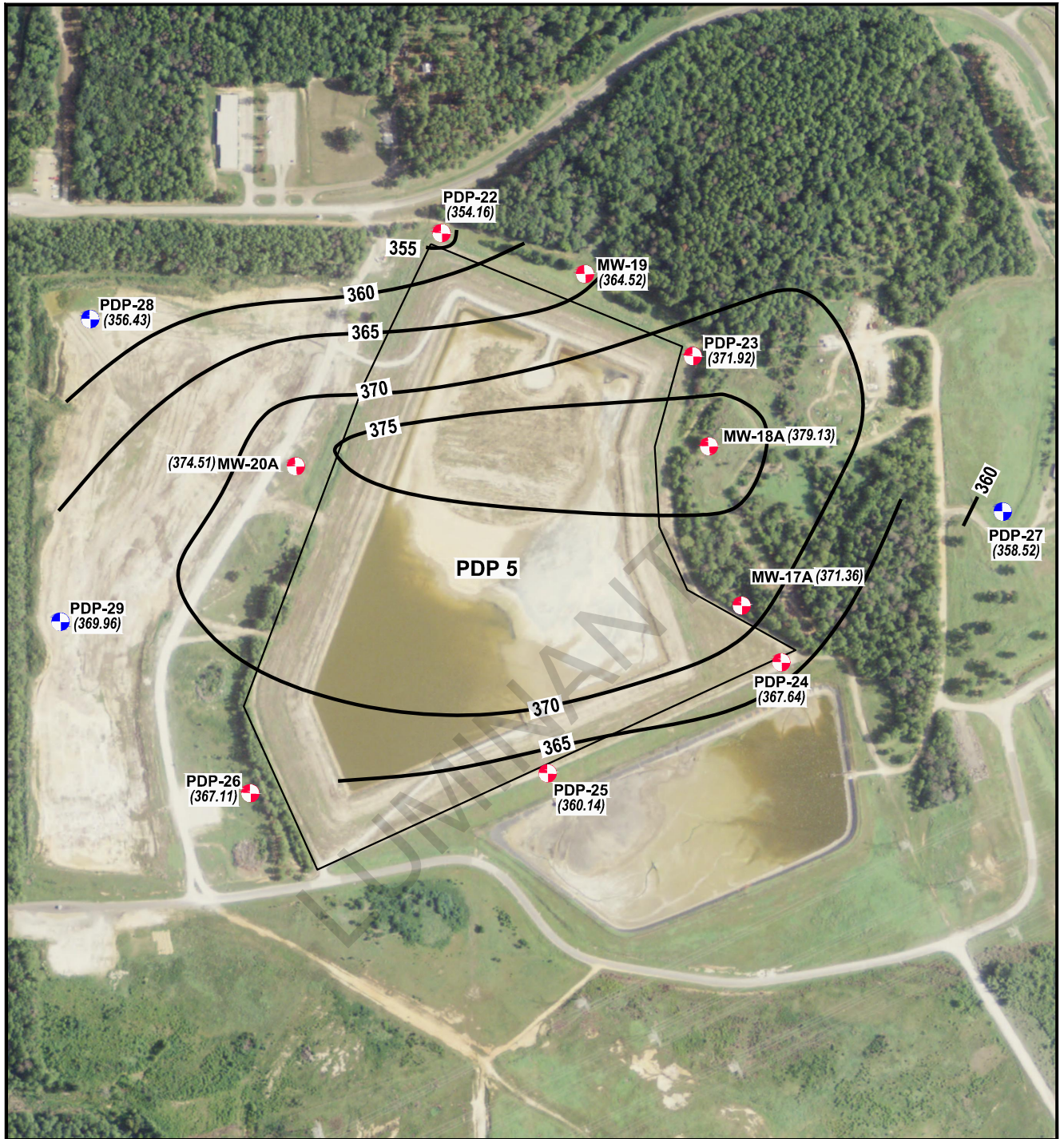
**MARTIN LAKE STEAM ELECTRIC STATION
TATUM, TEXAS**

Figure 6



**PDP 5 - GROUNDWATER
ZONE A POTENTIOMETRIC
SURFACE MAP - AUGUST 9, 2016**

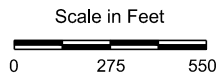
| | | |
|-------------------|--------------|-----------|
| PROJECT: 5164B | BY: AJD | REVISIONS |
| DATE: SEPT., 2017 | CHECKED: PJB | |

PASTOR, BEHLING & WHEELER, LLC
CONSULTING ENGINEERS AND SCIENTISTS



EXPLANATION

-  CCR Monitoring Well Location
-  Non-CCR Monitoring Well Used to Further Evaluate Groundwater Flow Direction
- (374.34) Groundwater Potentiometric Surface (ft. MSL)
- 360 — Groundwater Potentiometric Surface Contour (C.I. = 5 ft.)



SOURCE:
Imagery from www.tnris.gov, Rusk County, aerial photographs, 2012.

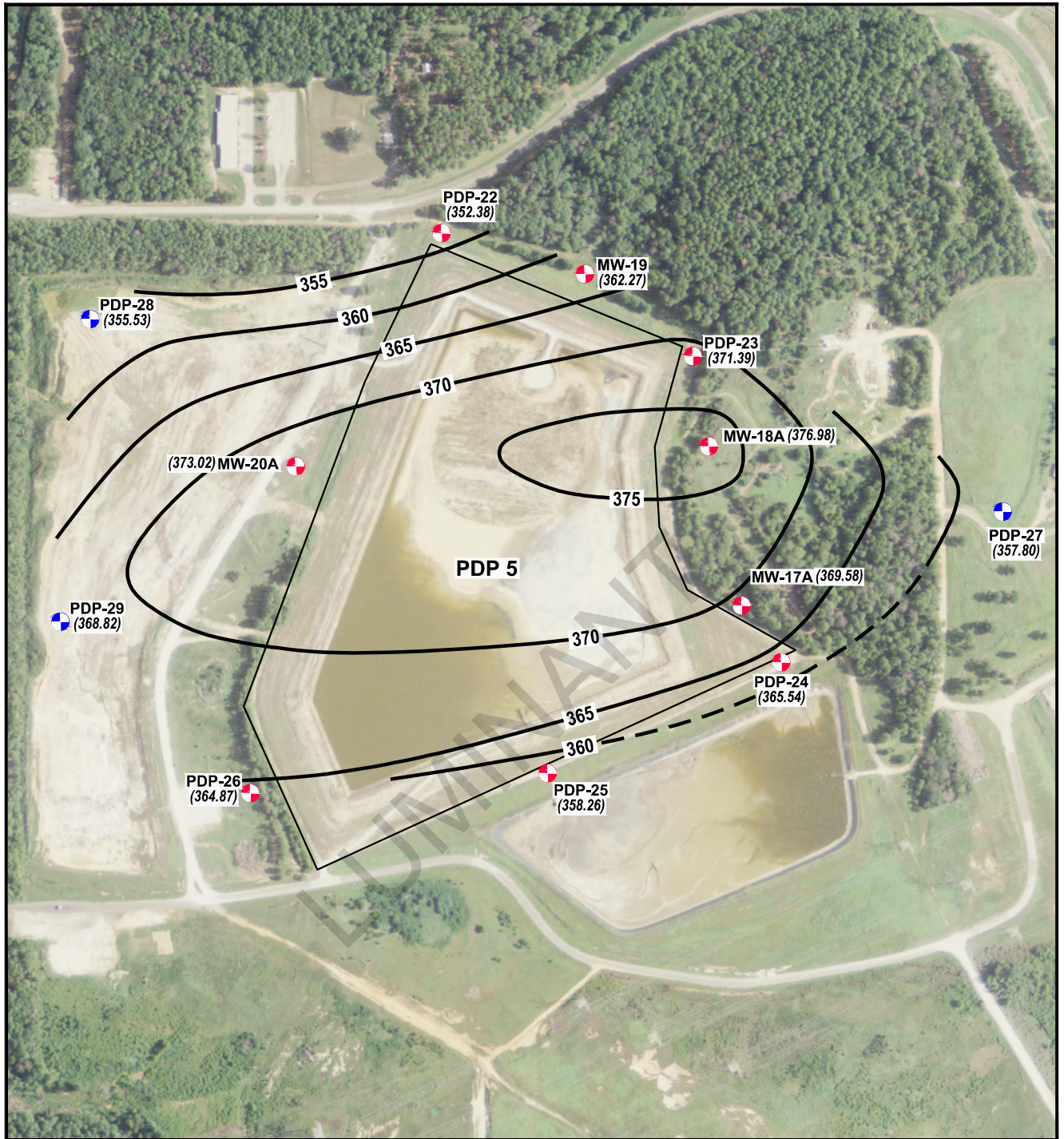
**MARTIN LAKE STEAM ELECTRIC STATION
TATUM, TEXAS**

Figure 7



**PDP 5 - GROUNDWATER
ZONE A POTENTIOMETRIC
SURFACE MAP - OCTOBER 17, 2016**

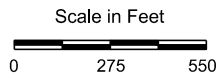
| | | |
|-------------------|--------------|-----------|
| PROJECT: 5164B | BY: AJD | REVISIONS |
| DATE: SEPT., 2017 | CHECKED: PJB | |

PASTOR, BEHLING & WHEELER, LLC
CONSULTING ENGINEERS AND SCIENTISTS



EXPLANATION

-  CCR Monitoring Well Location
-  Non-CCR Monitoring Well Used to Further Evaluate Groundwater Flow Direction
- (374.34) Groundwater Potentiometric Surface (ft. MSL)
- 360 — Groundwater Potentiometric Surface Contour (C.I. = 5 ft.)



SOURCE:
Imagery from www.tnris.gov, Rusk County, aerial photographs, 2012.

**MARTIN LAKE STEAM ELECTRIC STATION
TATUM, TEXAS**

Figure 8

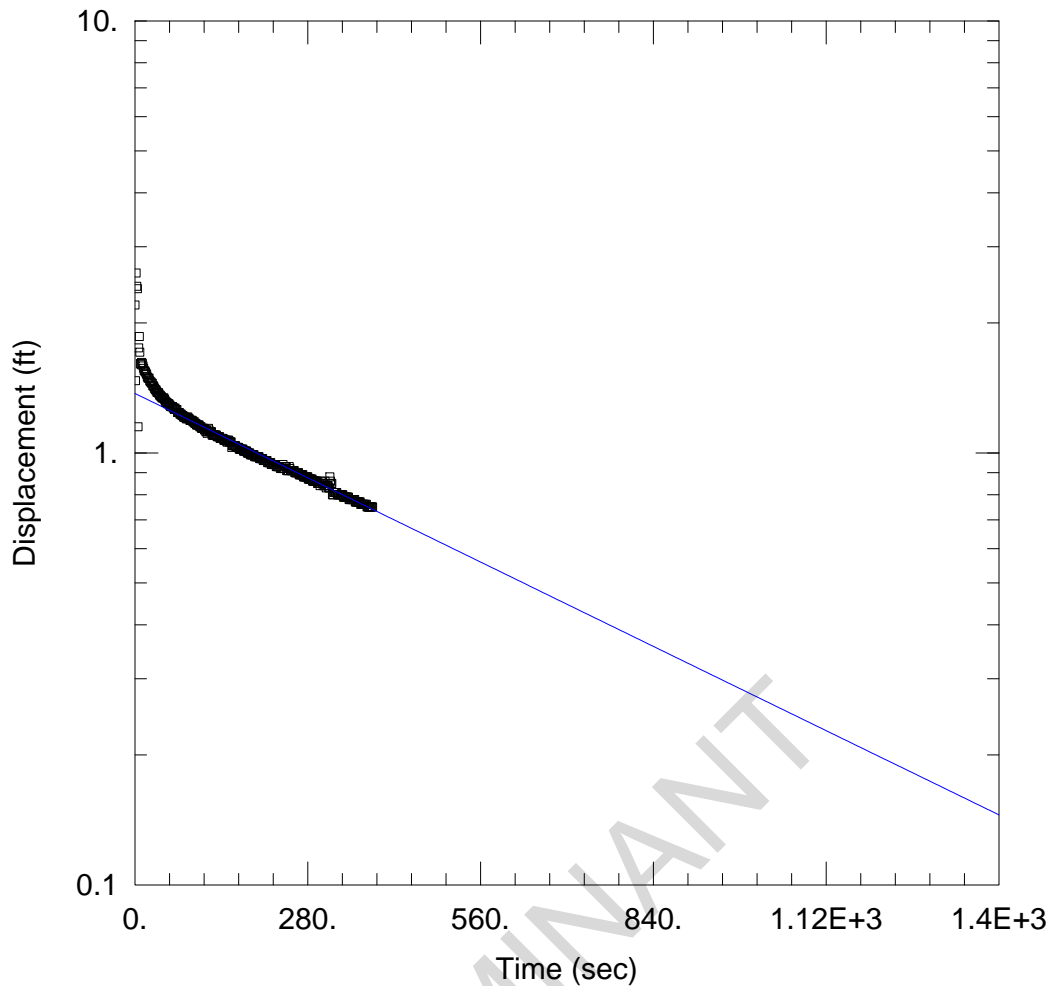
**PDP 5 - GROUNDWATER
ZONE A POTENTIOMETRIC
SURFACE MAP - DECEMBER 11, 2016**

| | | |
|-------------------|--------------|-----------|
| PROJECT: 5164B | BY: AJD | REVISIONS |
| DATE: SEPT., 2017 | CHECKED: PJB | |

PASTOR, BEHLING & WHEELER, LLC
CONSULTING ENGINEERS AND SCIENTISTS

Appendix D
Aquifer Test Data

LUMINANT



PDP-22 SLUG IN

Data Set: J:\...\PDP-22 Slug In.aqt
 Date: 12/16/15

Time: 10:25:03

PROJECT INFORMATION

Company: PBW
 Client: Luminant
 Project: 5164
 Location: MLSES
 Test Well: PDP-22
 Test Date: 10/7/15

AQUIFER DATA

Saturated Thickness: 22.84 ft

Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (PDP-22)

Initial Displacement: 2.2 ft
 Total Well Penetration Depth: 14.84 ft
 Casing Radius: 0.083 ft

Static Water Column Height: 22.84 ft
 Screen Length: 10. ft
 Well Radius: 0.27 ft

SOLUTION

Aquifer Model: Unconfined
 K = 4.362E-5 cm/sec

Solution Method: Bouwer-Rice
 y0 = 1.373 ft

Data Set: J:\5164 - Luminant CCR Well Installation and GW Sampling\5164-B_Martin Lake\Slug Tests\PDP5\Aqtes
 Title: PDP-22 Slug In
 Date: 12/16/15
 Time: 10:26:54

PROJECT INFORMATION

Company: PBW
 Client: Luminant
 Project: 5164
 Location: MLSES
 Test Date: 10/7/15
 Test Well: PDP-22

AQUIFER DATA

Saturated Thickness: 22.84 ft
 Anisotropy Ratio (Kz/Kr): 1.

SLUG TEST WELL DATA

Test Well: PDP-22

X Location: 0. ft
 Y Location: 0. ft

Initial Displacement: 2.2 ft
 Static Water Column Height: 22.84 ft
 Casing Radius: 0.083 ft
 Well Radius: 0.27 ft
 Well Skin Radius: 0.27 ft
 Screen Length: 10. ft
 Total Well Penetration Depth: 14.84 ft

No. of Observations: 385

| Observation Data | | | |
|------------------|-------------------|------------|-------------------|
| Time (sec) | Displacement (ft) | Time (sec) | Displacement (ft) |
| 1. | 1.47 | 194. | 0.98 |
| 2. | 2.61 | 195. | 0.98 |
| 3. | 2.43 | 196. | 0.98 |
| 4. | 2.4 | 197. | 0.98 |
| 5. | 1.15 | 198. | 0.98 |
| 6. | 1.75 | 199. | 0.98 |
| 7. | 1.86 | 200. | 0.98 |
| 8. | 1.71 | 201. | 0.98 |
| 9. | 1.61 | 202. | 0.97 |
| 10. | 1.6 | 203. | 0.97 |
| 11. | 1.62 | 204. | 0.97 |
| 12. | 1.61 | 205. | 0.97 |
| 13. | 1.59 | 206. | 0.97 |
| 14. | 1.57 | 207. | 0.97 |
| 15. | 1.55 | 208. | 0.96 |
| 16. | 1.55 | 209. | 0.96 |
| 17. | 1.54 | 210. | 0.96 |
| 18. | 1.53 | 211. | 0.96 |
| 19. | 1.52 | 212. | 0.96 |
| 20. | 1.5 | 213. | 0.96 |
| 21. | 1.49 | 214. | 0.96 |
| 22. | 1.49 | 215. | 0.95 |
| 23. | 1.49 | 216. | 0.95 |
| 24. | 1.47 | 217. | 0.95 |
| 25. | 1.46 | 218. | 0.95 |
| 26. | 1.46 | 219. | 0.95 |
| 27. | 1.45 | 220. | 0.95 |
| 28. | 1.45 | 221. | 0.94 |
| 29. | 1.43 | 222. | 0.94 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 30. | 1.43 | 223. | 0.94 |
| 31. | 1.42 | 224. | 0.94 |
| 32. | 1.41 | 225. | 0.94 |
| 33. | 1.4 | 226. | 0.94 |
| 34. | 1.4 | 227. | 0.94 |
| 35. | 1.39 | 228. | 0.94 |
| 36. | 1.38 | 229. | 0.93 |
| 37. | 1.38 | 230. | 0.93 |
| 38. | 1.38 | 231. | 0.93 |
| 39. | 1.37 | 232. | 0.93 |
| 40. | 1.36 | 233. | 0.93 |
| 41. | 1.36 | 234. | 0.93 |
| 42. | 1.35 | 235. | 0.93 |
| 43. | 1.35 | 236. | 0.92 |
| 44. | 1.34 | 237. | 0.92 |
| 45. | 1.34 | 238. | 0.92 |
| 46. | 1.34 | 239. | 0.92 |
| 47. | 1.34 | 240. | 0.94 |
| 48. | 1.33 | 241. | 0.92 |
| 49. | 1.32 | 242. | 0.92 |
| 50. | 1.31 | 243. | 0.93 |
| 51. | 1.31 | 244. | 0.93 |
| 52. | 1.31 | 245. | 0.93 |
| 53. | 1.3 | 246. | 0.91 |
| 54. | 1.3 | 247. | 0.91 |
| 55. | 1.3 | 248. | 0.91 |
| 56. | 1.29 | 249. | 0.91 |
| 57. | 1.29 | 250. | 0.93 |
| 58. | 1.28 | 251. | 0.92 |
| 59. | 1.28 | 252. | 0.91 |
| 60. | 1.28 | 253. | 0.91 |
| 61. | 1.28 | 254. | 0.91 |
| 62. | 1.27 | 255. | 0.91 |
| 63. | 1.27 | 256. | 0.91 |
| 64. | 1.26 | 257. | 0.91 |
| 65. | 1.27 | 258. | 0.91 |
| 66. | 1.26 | 259. | 0.9 |
| 67. | 1.26 | 260. | 0.9 |
| 68. | 1.26 | 261. | 0.9 |
| 69. | 1.24 | 262. | 0.9 |
| 70. | 1.24 | 263. | 0.9 |
| 71. | 1.24 | 264. | 0.9 |
| 72. | 1.24 | 265. | 0.9 |
| 73. | 1.23 | 266. | 0.89 |
| 74. | 1.23 | 267. | 0.89 |
| 75. | 1.23 | 268. | 0.89 |
| 76. | 1.22 | 269. | 0.89 |
| 77. | 1.22 | 270. | 0.89 |
| 78. | 1.22 | 271. | 0.89 |
| 79. | 1.21 | 272. | 0.89 |
| 80. | 1.21 | 273. | 0.88 |
| 81. | 1.21 | 274. | 0.88 |
| 82. | 1.21 | 275. | 0.88 |
| 83. | 1.2 | 276. | 0.88 |
| 84. | 1.2 | 277. | 0.88 |
| 85. | 1.21 | 278. | 0.88 |
| 86. | 1.21 | 279. | 0.88 |
| 87. | 1.2 | 280. | 0.88 |
| 88. | 1.2 | 281. | 0.87 |
| 89. | 1.19 | 282. | 0.87 |
| 90. | 1.19 | 283. | 0.87 |
| 91. | 1.19 | 284. | 0.87 |
| 92. | 1.19 | 285. | 0.87 |
| 93. | 1.19 | 286. | 0.87 |
| 94. | 1.18 | 287. | 0.87 |
| 95. | 1.18 | 288. | 0.86 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 96. | 1.18 | 289. | 0.86 |
| 97. | 1.17 | 290. | 0.86 |
| 98. | 1.17 | 291. | 0.86 |
| 99. | 1.17 | 292. | 0.86 |
| 100. | 1.16 | 293. | 0.86 |
| 101. | 1.16 | 294. | 0.86 |
| 102. | 1.16 | 295. | 0.86 |
| 103. | 1.16 | 296. | 0.85 |
| 104. | 1.16 | 297. | 0.85 |
| 105. | 1.15 | 298. | 0.85 |
| 106. | 1.15 | 299. | 0.85 |
| 107. | 1.15 | 300. | 0.84 |
| 108. | 1.14 | 301. | 0.85 |
| 109. | 1.14 | 302. | 0.86 |
| 110. | 1.14 | 303. | 0.85 |
| 111. | 1.14 | 304. | 0.85 |
| 112. | 1.14 | 305. | 0.84 |
| 113. | 1.13 | 306. | 0.85 |
| 114. | 1.13 | 307. | 0.84 |
| 115. | 1.12 | 308. | 0.86 |
| 116. | 1.13 | 309. | 0.84 |
| 117. | 1.11 | 310. | 0.83 |
| 118. | 1.12 | 311. | 0.84 |
| 119. | 1.14 | 312. | 0.84 |
| 120. | 1.13 | 313. | 0.84 |
| 121. | 1.12 | 314. | 0.83 |
| 122. | 1.12 | 315. | 0.83 |
| 123. | 1.12 | 316. | 0.88 |
| 124. | 1.12 | 317. | 0.86 |
| 125. | 1.1 | 318. | 0.85 |
| 126. | 1.1 | 319. | 0.85 |
| 127. | 1.1 | 320. | 0.8 |
| 128. | 1.1 | 321. | 0.8 |
| 129. | 1.1 | 322. | 0.81 |
| 130. | 1.1 | 323. | 0.81 |
| 131. | 1.1 | 324. | 0.81 |
| 132. | 1.1 | 325. | 0.81 |
| 133. | 1.09 | 326. | 0.81 |
| 134. | 1.09 | 327. | 0.81 |
| 135. | 1.09 | 328. | 0.8 |
| 136. | 1.09 | 329. | 0.8 |
| 137. | 1.09 | 330. | 0.8 |
| 138. | 1.08 | 331. | 0.8 |
| 139. | 1.08 | 332. | 0.8 |
| 140. | 1.08 | 333. | 0.8 |
| 141. | 1.08 | 334. | 0.8 |
| 142. | 1.08 | 335. | 0.8 |
| 143. | 1.08 | 336. | 0.8 |
| 144. | 1.07 | 337. | 0.8 |
| 145. | 1.07 | 338. | 0.79 |
| 146. | 1.07 | 339. | 0.79 |
| 147. | 1.07 | 340. | 0.79 |
| 148. | 1.07 | 341. | 0.79 |
| 149. | 1.06 | 342. | 0.79 |
| 150. | 1.06 | 343. | 0.79 |
| 151. | 1.07 | 344. | 0.79 |
| 152. | 1.07 | 345. | 0.79 |
| 153. | 1.06 | 346. | 0.79 |
| 154. | 1.06 | 347. | 0.78 |
| 155. | 1.06 | 348. | 0.78 |
| 156. | 1.06 | 349. | 0.78 |
| 157. | 1.03 | 350. | 0.78 |
| 158. | 1.04 | 351. | 0.78 |
| 159. | 1.04 | 352. | 0.78 |
| 160. | 1.04 | 353. | 0.78 |
| 161. | 1.04 | 354. | 0.78 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 162. | 1.04 | 355. | 0.78 |
| 163. | 1.04 | 356. | 0.78 |
| 164. | 1.03 | 357. | 0.77 |
| 165. | 1.03 | 358. | 0.77 |
| 166. | 1.03 | 359. | 0.77 |
| 167. | 1.03 | 360. | 0.77 |
| 168. | 1.03 | 361. | 0.77 |
| 169. | 1.02 | 362. | 0.77 |
| 170. | 1.02 | 363. | 0.77 |
| 171. | 1.02 | 364. | 0.77 |
| 172. | 1.02 | 365. | 0.77 |
| 173. | 1.02 | 366. | 0.76 |
| 174. | 1.02 | 367. | 0.76 |
| 175. | 1.02 | 368. | 0.76 |
| 176. | 1.01 | 369. | 0.76 |
| 177. | 1.01 | 370. | 0.76 |
| 178. | 1.01 | 371. | 0.76 |
| 179. | 1.01 | 372. | 0.76 |
| 180. | 1.01 | 373. | 0.76 |
| 181. | 1.01 | 374. | 0.76 |
| 182. | 1. | 375. | 0.76 |
| 183. | 1. | 376. | 0.75 |
| 184. | 1. | 377. | 0.75 |
| 185. | 1. | 378. | 0.75 |
| 186. | 1. | 379. | 0.75 |
| 187. | 0.99 | 380. | 0.75 |
| 188. | 0.99 | 381. | 0.75 |
| 189. | 0.99 | 382. | 0.75 |
| 190. | 0.99 | 383. | 0.75 |
| 191. | 0.99 | 384. | 0.75 |
| 192. | 0.99 | 385. | 0.75 |
| 193. | 0.99 | | |

SOLUTION

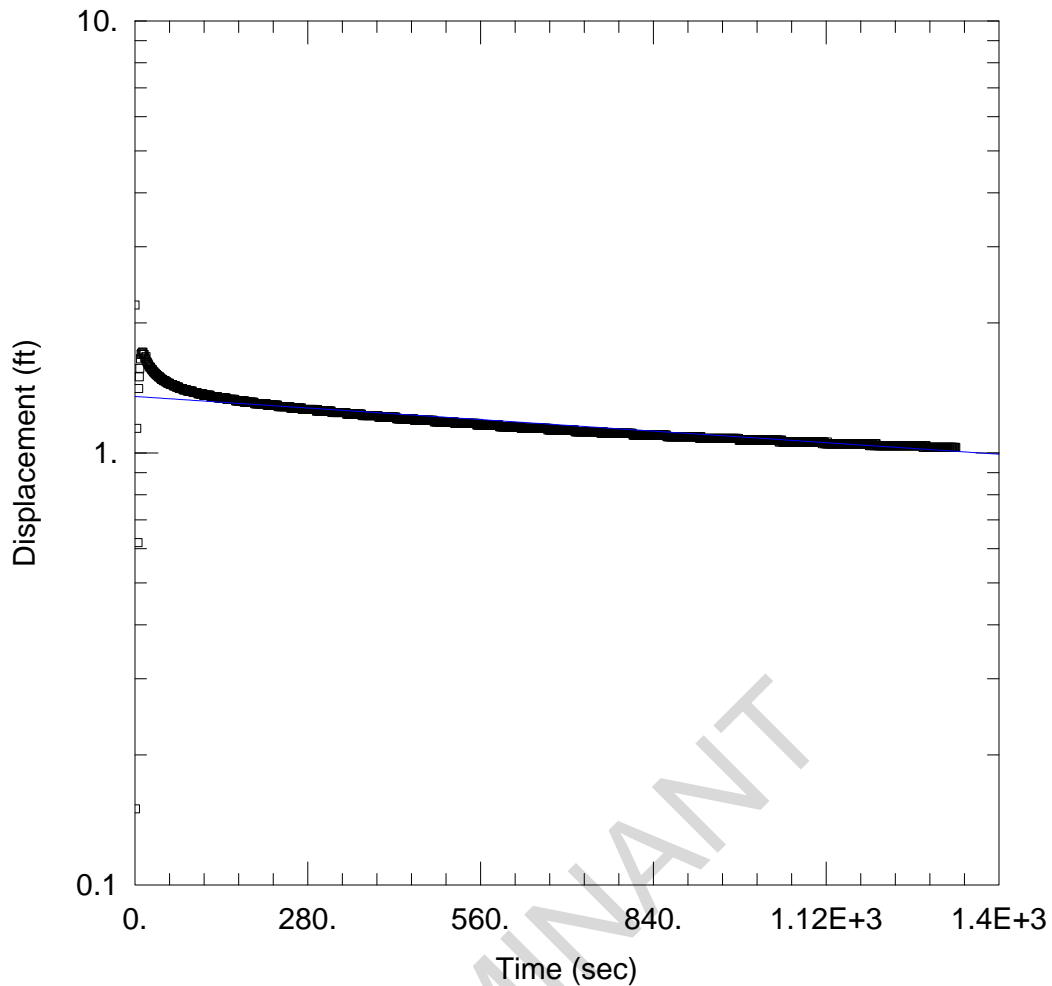
Slug Test
 Aquifer Model: Unconfined
 Solution Method: Bouwer-Rice
 ln(Re/rw): 2.589

VISUAL ESTIMATION RESULTS

Estimated Parameters

| <u>Parameter</u> | <u>Estimate</u> | |
|------------------|-----------------|--------|
| K | 4.362E-5 | cm/sec |
| y0 | 1.373 | ft |

$T = K*b = 0.03037 \text{ cm}^2/\text{sec}$



PDP-22 SLUG OUT

Data Set: J:\...\PDP-22 Slug Out.aqt
 Date: 12/16/15

Time: 10:25:15

PROJECT INFORMATION

Company: PBW
 Client: Luminant
 Project: 5164
 Location: MLSES
 Test Well: PDP-22
 Test Date: 10/7/15

AQUIFER DATA

Saturated Thickness: 22.84 ft

Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (PDP-22)

Initial Displacement: 2.2 ft
 Total Well Penetration Depth: 14.84 ft
 Casing Radius: 0.083 ft

Static Water Column Height: 22.84 ft
 Screen Length: 10. ft
 Well Radius: 0.27 ft

SOLUTION

Aquifer Model: Unconfined
 K = 5.977E-6 cm/sec

Solution Method: Bouwer-Rice
 y0 = 1.351 ft

Data Set: J:\5164 - Luminant CCR Well Installation and GW Sampling\5164-B_Martin Lake\Slug Tests\PDP5\Aqtes
 Title: PDP-22 Slug Out
 Date: 12/16/15
 Time: 10:26:45

PROJECT INFORMATION

Company: PBW
 Client: Luminant
 Project: 5164
 Location: MLSES
 Test Date: 10/7/15
 Test Well: PDP-22

AQUIFER DATA

Saturated Thickness: 22.84 ft
 Anisotropy Ratio (Kz/Kr): 1.

SLUG TEST WELL DATA

Test Well: PDP-22

X Location: 0. ft
 Y Location: 0. ft

Initial Displacement: 2.2 ft
 Static Water Column Height: 22.84 ft
 Casing Radius: 0.083 ft
 Well Radius: 0.27 ft
 Well Skin Radius: 0.27 ft
 Screen Length: 10. ft
 Total Well Penetration Depth: 14.84 ft

No. of Observations: 1329

| Observation Data | | | |
|------------------|-------------------|------------|-------------------|
| Time (sec) | Displacement (ft) | Time (sec) | Displacement (ft) |
| 1. | 0.15 | 667. | 1.14 |
| 2. | 0.09 | 668. | 1.14 |
| 3. | 1.14 | 669. | 1.13 |
| 5. | 0.62 | 670. | 1.14 |
| 6. | 1.41 | 671. | 1.13 |
| 7. | 1.5 | 672. | 1.13 |
| 8. | 1.57 | 673. | 1.13 |
| 9. | 1.65 | 674. | 1.13 |
| 10. | 1.69 | 675. | 1.13 |
| 11. | 1.7 | 676. | 1.13 |
| 12. | 1.71 | 677. | 1.13 |
| 13. | 1.71 | 678. | 1.13 |
| 14. | 1.69 | 679. | 1.13 |
| 15. | 1.69 | 680. | 1.13 |
| 16. | 1.66 | 681. | 1.13 |
| 17. | 1.65 | 682. | 1.13 |
| 18. | 1.67 | 683. | 1.13 |
| 19. | 1.63 | 684. | 1.13 |
| 20. | 1.62 | 685. | 1.13 |
| 21. | 1.61 | 686. | 1.13 |
| 22. | 1.6 | 687. | 1.13 |
| 23. | 1.59 | 688. | 1.13 |
| 24. | 1.58 | 689. | 1.13 |
| 25. | 1.58 | 690. | 1.13 |
| 26. | 1.57 | 691. | 1.13 |
| 27. | 1.56 | 692. | 1.13 |
| 28. | 1.56 | 693. | 1.13 |
| 29. | 1.55 | 694. | 1.13 |
| 30. | 1.54 | 695. | 1.13 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 31. | 1.54 | 696. | 1.13 |
| 32. | 1.53 | 697. | 1.13 |
| 33. | 1.53 | 698. | 1.13 |
| 34. | 1.52 | 699. | 1.13 |
| 35. | 1.52 | 700. | 1.13 |
| 36. | 1.51 | 701. | 1.13 |
| 37. | 1.51 | 702. | 1.13 |
| 38. | 1.5 | 703. | 1.13 |
| 39. | 1.5 | 704. | 1.13 |
| 40. | 1.5 | 705. | 1.13 |
| 41. | 1.49 | 706. | 1.13 |
| 42. | 1.49 | 707. | 1.13 |
| 43. | 1.48 | 708. | 1.13 |
| 44. | 1.48 | 709. | 1.13 |
| 45. | 1.48 | 710. | 1.13 |
| 46. | 1.47 | 711. | 1.13 |
| 47. | 1.47 | 712. | 1.13 |
| 48. | 1.47 | 713. | 1.12 |
| 49. | 1.47 | 714. | 1.12 |
| 50. | 1.46 | 715. | 1.12 |
| 51. | 1.46 | 716. | 1.12 |
| 52. | 1.46 | 717. | 1.12 |
| 53. | 1.45 | 718. | 1.12 |
| 54. | 1.45 | 719. | 1.12 |
| 55. | 1.45 | 720. | 1.12 |
| 56. | 1.45 | 721. | 1.12 |
| 57. | 1.44 | 722. | 1.12 |
| 58. | 1.44 | 723. | 1.12 |
| 59. | 1.44 | 724. | 1.12 |
| 60. | 1.44 | 725. | 1.12 |
| 61. | 1.44 | 726. | 1.12 |
| 62. | 1.43 | 727. | 1.12 |
| 63. | 1.43 | 728. | 1.12 |
| 64. | 1.43 | 729. | 1.12 |
| 65. | 1.43 | 730. | 1.12 |
| 66. | 1.43 | 731. | 1.12 |
| 67. | 1.42 | 732. | 1.12 |
| 68. | 1.42 | 733. | 1.12 |
| 69. | 1.42 | 734. | 1.12 |
| 70. | 1.42 | 735. | 1.12 |
| 71. | 1.42 | 736. | 1.12 |
| 72. | 1.41 | 737. | 1.12 |
| 73. | 1.41 | 738. | 1.12 |
| 74. | 1.41 | 739. | 1.12 |
| 75. | 1.41 | 740. | 1.12 |
| 76. | 1.41 | 741. | 1.12 |
| 77. | 1.41 | 742. | 1.12 |
| 78. | 1.4 | 743. | 1.12 |
| 79. | 1.4 | 744. | 1.12 |
| 80. | 1.4 | 745. | 1.12 |
| 81. | 1.4 | 746. | 1.12 |
| 82. | 1.4 | 747. | 1.12 |
| 83. | 1.4 | 748. | 1.12 |
| 84. | 1.4 | 749. | 1.12 |
| 85. | 1.39 | 750. | 1.12 |
| 86. | 1.39 | 751. | 1.12 |
| 87. | 1.39 | 752. | 1.12 |
| 88. | 1.39 | 753. | 1.12 |
| 89. | 1.39 | 754. | 1.12 |
| 90. | 1.39 | 755. | 1.11 |
| 91. | 1.39 | 756. | 1.12 |
| 92. | 1.39 | 757. | 1.11 |
| 93. | 1.39 | 758. | 1.12 |
| 94. | 1.38 | 759. | 1.12 |
| 95. | 1.38 | 760. | 1.11 |
| 96. | 1.38 | 761. | 1.11 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 97. | 1.38 | 762. | 1.11 |
| 98. | 1.38 | 763. | 1.11 |
| 99. | 1.38 | 764. | 1.11 |
| 100. | 1.38 | 765. | 1.11 |
| 101. | 1.38 | 766. | 1.11 |
| 102. | 1.37 | 767. | 1.11 |
| 103. | 1.37 | 768. | 1.11 |
| 104. | 1.37 | 769. | 1.11 |
| 105. | 1.37 | 770. | 1.11 |
| 106. | 1.37 | 771. | 1.11 |
| 107. | 1.37 | 772. | 1.11 |
| 108. | 1.37 | 773. | 1.11 |
| 109. | 1.37 | 774. | 1.11 |
| 110. | 1.37 | 775. | 1.11 |
| 111. | 1.36 | 776. | 1.11 |
| 112. | 1.36 | 777. | 1.11 |
| 113. | 1.36 | 778. | 1.11 |
| 114. | 1.36 | 779. | 1.11 |
| 115. | 1.36 | 780. | 1.11 |
| 116. | 1.36 | 781. | 1.11 |
| 117. | 1.36 | 782. | 1.11 |
| 118. | 1.36 | 783. | 1.11 |
| 119. | 1.36 | 784. | 1.11 |
| 120. | 1.36 | 785. | 1.11 |
| 121. | 1.36 | 786. | 1.11 |
| 122. | 1.36 | 787. | 1.11 |
| 123. | 1.35 | 788. | 1.11 |
| 124. | 1.35 | 789. | 1.11 |
| 125. | 1.35 | 790. | 1.11 |
| 126. | 1.35 | 791. | 1.11 |
| 127. | 1.35 | 792. | 1.11 |
| 128. | 1.35 | 793. | 1.11 |
| 129. | 1.35 | 794. | 1.11 |
| 130. | 1.35 | 795. | 1.11 |
| 131. | 1.35 | 796. | 1.11 |
| 132. | 1.35 | 797. | 1.11 |
| 133. | 1.35 | 798. | 1.11 |
| 134. | 1.35 | 799. | 1.11 |
| 135. | 1.34 | 800. | 1.11 |
| 136. | 1.34 | 801. | 1.11 |
| 137. | 1.34 | 802. | 1.11 |
| 138. | 1.34 | 803. | 1.11 |
| 139. | 1.34 | 804. | 1.11 |
| 140. | 1.34 | 805. | 1.11 |
| 141. | 1.34 | 806. | 1.11 |
| 142. | 1.34 | 807. | 1.1 |
| 143. | 1.34 | 808. | 1.1 |
| 144. | 1.34 | 809. | 1.1 |
| 145. | 1.34 | 810. | 1.1 |
| 146. | 1.34 | 811. | 1.1 |
| 147. | 1.34 | 812. | 1.1 |
| 148. | 1.34 | 813. | 1.1 |
| 149. | 1.33 | 814. | 1.1 |
| 150. | 1.33 | 815. | 1.1 |
| 151. | 1.33 | 816. | 1.1 |
| 152. | 1.33 | 817. | 1.1 |
| 153. | 1.33 | 818. | 1.1 |
| 154. | 1.33 | 819. | 1.1 |
| 155. | 1.33 | 820. | 1.1 |
| 156. | 1.33 | 821. | 1.1 |
| 157. | 1.33 | 822. | 1.1 |
| 158. | 1.33 | 823. | 1.1 |
| 159. | 1.33 | 824. | 1.1 |
| 160. | 1.33 | 825. | 1.1 |
| 161. | 1.33 | 826. | 1.1 |
| 162. | 1.33 | 827. | 1.1 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 163. | 1.32 | 828. | 1.1 |
| 164. | 1.32 | 829. | 1.1 |
| 165. | 1.32 | 830. | 1.1 |
| 166. | 1.32 | 831. | 1.1 |
| 167. | 1.32 | 832. | 1.1 |
| 168. | 1.32 | 833. | 1.1 |
| 169. | 1.32 | 834. | 1.1 |
| 170. | 1.32 | 835. | 1.1 |
| 171. | 1.32 | 836. | 1.1 |
| 172. | 1.32 | 837. | 1.1 |
| 173. | 1.32 | 838. | 1.1 |
| 174. | 1.32 | 839. | 1.1 |
| 175. | 1.32 | 840. | 1.1 |
| 176. | 1.32 | 841. | 1.1 |
| 177. | 1.31 | 842. | 1.1 |
| 178. | 1.32 | 843. | 1.1 |
| 179. | 1.31 | 844. | 1.1 |
| 180. | 1.31 | 845. | 1.1 |
| 181. | 1.31 | 846. | 1.1 |
| 182. | 1.31 | 847. | 1.1 |
| 183. | 1.31 | 848. | 1.1 |
| 184. | 1.31 | 849. | 1.1 |
| 185. | 1.31 | 850. | 1.1 |
| 186. | 1.31 | 851. | 1.1 |
| 187. | 1.31 | 852. | 1.1 |
| 188. | 1.31 | 853. | 1.1 |
| 189. | 1.31 | 854. | 1.1 |
| 190. | 1.31 | 855. | 1.1 |
| 191. | 1.31 | 856. | 1.1 |
| 192. | 1.31 | 857. | 1.1 |
| 193. | 1.31 | 858. | 1.1 |
| 194. | 1.3 | 859. | 1.1 |
| 195. | 1.3 | 860. | 1.1 |
| 196. | 1.3 | 861. | 1.1 |
| 197. | 1.3 | 862. | 1.09 |
| 198. | 1.3 | 863. | 1.09 |
| 199. | 1.3 | 864. | 1.09 |
| 200. | 1.3 | 865. | 1.09 |
| 201. | 1.3 | 866. | 1.09 |
| 202. | 1.3 | 867. | 1.09 |
| 203. | 1.3 | 868. | 1.09 |
| 204. | 1.3 | 869. | 1.09 |
| 205. | 1.3 | 870. | 1.09 |
| 206. | 1.3 | 871. | 1.09 |
| 207. | 1.3 | 872. | 1.09 |
| 208. | 1.3 | 873. | 1.09 |
| 209. | 1.3 | 874. | 1.09 |
| 210. | 1.3 | 875. | 1.09 |
| 211. | 1.3 | 876. | 1.09 |
| 212. | 1.3 | 877. | 1.09 |
| 213. | 1.3 | 878. | 1.09 |
| 214. | 1.29 | 879. | 1.09 |
| 215. | 1.29 | 880. | 1.09 |
| 216. | 1.29 | 881. | 1.09 |
| 217. | 1.29 | 882. | 1.09 |
| 218. | 1.29 | 883. | 1.09 |
| 219. | 1.29 | 884. | 1.09 |
| 220. | 1.29 | 885. | 1.09 |
| 221. | 1.29 | 886. | 1.09 |
| 222. | 1.29 | 887. | 1.09 |
| 223. | 1.29 | 888. | 1.09 |
| 224. | 1.29 | 889. | 1.09 |
| 225. | 1.29 | 890. | 1.09 |
| 226. | 1.29 | 891. | 1.09 |
| 227. | 1.29 | 892. | 1.09 |
| 228. | 1.29 | 893. | 1.09 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 229. | 1.29 | 894. | 1.09 |
| 230. | 1.29 | 895. | 1.09 |
| 231. | 1.29 | 896. | 1.09 |
| 232. | 1.28 | 897. | 1.09 |
| 233. | 1.28 | 898. | 1.09 |
| 234. | 1.28 | 899. | 1.09 |
| 235. | 1.28 | 900. | 1.09 |
| 236. | 1.28 | 901. | 1.09 |
| 237. | 1.28 | 902. | 1.09 |
| 238. | 1.28 | 903. | 1.09 |
| 239. | 1.28 | 904. | 1.09 |
| 240. | 1.28 | 905. | 1.09 |
| 241. | 1.28 | 906. | 1.09 |
| 242. | 1.28 | 907. | 1.09 |
| 243. | 1.28 | 908. | 1.09 |
| 244. | 1.28 | 909. | 1.09 |
| 245. | 1.28 | 910. | 1.09 |
| 246. | 1.28 | 911. | 1.09 |
| 247. | 1.28 | 912. | 1.09 |
| 248. | 1.28 | 913. | 1.09 |
| 249. | 1.28 | 914. | 1.09 |
| 250. | 1.28 | 915. | 1.08 |
| 251. | 1.28 | 916. | 1.09 |
| 252. | 1.27 | 917. | 1.09 |
| 253. | 1.27 | 918. | 1.08 |
| 254. | 1.27 | 919. | 1.08 |
| 255. | 1.27 | 920. | 1.08 |
| 256. | 1.27 | 921. | 1.08 |
| 257. | 1.27 | 922. | 1.08 |
| 258. | 1.27 | 923. | 1.08 |
| 259. | 1.27 | 924. | 1.08 |
| 260. | 1.27 | 925. | 1.08 |
| 261. | 1.27 | 926. | 1.08 |
| 262. | 1.27 | 927. | 1.08 |
| 263. | 1.27 | 928. | 1.08 |
| 264. | 1.27 | 929. | 1.08 |
| 265. | 1.27 | 930. | 1.08 |
| 266. | 1.27 | 931. | 1.08 |
| 267. | 1.27 | 932. | 1.08 |
| 268. | 1.27 | 933. | 1.08 |
| 269. | 1.27 | 934. | 1.08 |
| 270. | 1.27 | 935. | 1.08 |
| 271. | 1.26 | 936. | 1.08 |
| 272. | 1.26 | 937. | 1.08 |
| 273. | 1.26 | 938. | 1.08 |
| 274. | 1.26 | 939. | 1.08 |
| 275. | 1.26 | 940. | 1.08 |
| 276. | 1.26 | 941. | 1.08 |
| 277. | 1.26 | 942. | 1.08 |
| 278. | 1.26 | 943. | 1.08 |
| 279. | 1.26 | 944. | 1.08 |
| 280. | 1.26 | 945. | 1.08 |
| 281. | 1.26 | 946. | 1.08 |
| 282. | 1.26 | 947. | 1.08 |
| 283. | 1.26 | 948. | 1.08 |
| 284. | 1.26 | 949. | 1.08 |
| 285. | 1.26 | 950. | 1.08 |
| 286. | 1.26 | 951. | 1.08 |
| 287. | 1.26 | 952. | 1.08 |
| 288. | 1.26 | 953. | 1.08 |
| 289. | 1.26 | 954. | 1.08 |
| 290. | 1.26 | 955. | 1.08 |
| 291. | 1.26 | 956. | 1.08 |
| 292. | 1.26 | 957. | 1.08 |
| 293. | 1.26 | 958. | 1.08 |
| 294. | 1.25 | 959. | 1.08 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 295. | 1.25 | 960. | 1.08 |
| 296. | 1.26 | 961. | 1.08 |
| 297. | 1.25 | 962. | 1.08 |
| 298. | 1.25 | 963. | 1.08 |
| 299. | 1.25 | 964. | 1.08 |
| 300. | 1.25 | 965. | 1.08 |
| 301. | 1.25 | 966. | 1.08 |
| 302. | 1.25 | 967. | 1.08 |
| 303. | 1.25 | 968. | 1.08 |
| 304. | 1.25 | 969. | 1.08 |
| 305. | 1.25 | 970. | 1.08 |
| 306. | 1.25 | 971. | 1.08 |
| 307. | 1.25 | 972. | 1.08 |
| 308. | 1.25 | 973. | 1.08 |
| 309. | 1.25 | 974. | 1.08 |
| 310. | 1.25 | 975. | 1.08 |
| 311. | 1.25 | 976. | 1.08 |
| 312. | 1.25 | 977. | 1.08 |
| 313. | 1.25 | 978. | 1.08 |
| 314. | 1.25 | 979. | 1.07 |
| 315. | 1.25 | 980. | 1.07 |
| 316. | 1.25 | 981. | 1.07 |
| 317. | 1.25 | 982. | 1.07 |
| 318. | 1.25 | 983. | 1.07 |
| 319. | 1.24 | 984. | 1.07 |
| 320. | 1.24 | 985. | 1.07 |
| 321. | 1.24 | 986. | 1.07 |
| 322. | 1.24 | 987. | 1.07 |
| 323. | 1.24 | 988. | 1.07 |
| 324. | 1.24 | 989. | 1.07 |
| 325. | 1.24 | 990. | 1.07 |
| 326. | 1.24 | 991. | 1.07 |
| 327. | 1.24 | 992. | 1.07 |
| 328. | 1.24 | 993. | 1.07 |
| 329. | 1.24 | 994. | 1.07 |
| 330. | 1.24 | 995. | 1.07 |
| 331. | 1.24 | 996. | 1.07 |
| 332. | 1.24 | 997. | 1.07 |
| 333. | 1.24 | 998. | 1.07 |
| 334. | 1.24 | 999. | 1.07 |
| 335. | 1.24 | 1000. | 1.07 |
| 336. | 1.24 | 1001. | 1.07 |
| 337. | 1.24 | 1002. | 1.07 |
| 338. | 1.24 | 1003. | 1.07 |
| 339. | 1.24 | 1004. | 1.07 |
| 340. | 1.24 | 1005. | 1.07 |
| 341. | 1.24 | 1006. | 1.07 |
| 342. | 1.24 | 1007. | 1.07 |
| 343. | 1.23 | 1008. | 1.07 |
| 344. | 1.23 | 1009. | 1.07 |
| 345. | 1.23 | 1010. | 1.07 |
| 346. | 1.23 | 1011. | 1.07 |
| 347. | 1.23 | 1012. | 1.07 |
| 348. | 1.23 | 1013. | 1.07 |
| 349. | 1.23 | 1014. | 1.07 |
| 350. | 1.23 | 1015. | 1.07 |
| 351. | 1.23 | 1016. | 1.07 |
| 352. | 1.23 | 1017. | 1.07 |
| 353. | 1.23 | 1018. | 1.07 |
| 354. | 1.23 | 1019. | 1.07 |
| 355. | 1.23 | 1020. | 1.07 |
| 356. | 1.23 | 1021. | 1.07 |
| 357. | 1.23 | 1022. | 1.07 |
| 358. | 1.23 | 1023. | 1.07 |
| 359. | 1.23 | 1024. | 1.07 |
| 360. | 1.23 | 1025. | 1.07 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 361. | 1.23 | 1026. | 1.07 |
| 362. | 1.23 | 1027. | 1.07 |
| 363. | 1.23 | 1028. | 1.07 |
| 364. | 1.23 | 1029. | 1.07 |
| 365. | 1.23 | 1030. | 1.07 |
| 366. | 1.23 | 1031. | 1.07 |
| 367. | 1.23 | 1032. | 1.07 |
| 368. | 1.22 | 1033. | 1.07 |
| 369. | 1.22 | 1034. | 1.07 |
| 370. | 1.22 | 1035. | 1.07 |
| 371. | 1.22 | 1036. | 1.07 |
| 372. | 1.22 | 1037. | 1.07 |
| 373. | 1.22 | 1038. | 1.07 |
| 374. | 1.22 | 1039. | 1.07 |
| 375. | 1.22 | 1040. | 1.07 |
| 376. | 1.22 | 1041. | 1.07 |
| 377. | 1.22 | 1042. | 1.07 |
| 378. | 1.22 | 1043. | 1.07 |
| 379. | 1.22 | 1044. | 1.06 |
| 380. | 1.22 | 1045. | 1.06 |
| 381. | 1.22 | 1046. | 1.07 |
| 382. | 1.22 | 1047. | 1.07 |
| 383. | 1.22 | 1048. | 1.07 |
| 384. | 1.22 | 1049. | 1.06 |
| 385. | 1.22 | 1050. | 1.06 |
| 386. | 1.22 | 1051. | 1.06 |
| 387. | 1.22 | 1052. | 1.06 |
| 388. | 1.22 | 1053. | 1.06 |
| 389. | 1.22 | 1054. | 1.06 |
| 390. | 1.22 | 1055. | 1.06 |
| 391. | 1.22 | 1056. | 1.06 |
| 392. | 1.22 | 1057. | 1.06 |
| 393. | 1.22 | 1058. | 1.06 |
| 394. | 1.22 | 1059. | 1.06 |
| 395. | 1.21 | 1060. | 1.06 |
| 396. | 1.21 | 1061. | 1.06 |
| 397. | 1.21 | 1062. | 1.06 |
| 398. | 1.21 | 1063. | 1.06 |
| 399. | 1.21 | 1064. | 1.06 |
| 400. | 1.21 | 1065. | 1.06 |
| 401. | 1.21 | 1066. | 1.06 |
| 402. | 1.21 | 1067. | 1.06 |
| 403. | 1.21 | 1068. | 1.06 |
| 404. | 1.21 | 1069. | 1.06 |
| 405. | 1.21 | 1070. | 1.06 |
| 406. | 1.21 | 1071. | 1.06 |
| 407. | 1.21 | 1072. | 1.06 |
| 408. | 1.21 | 1073. | 1.06 |
| 409. | 1.21 | 1074. | 1.06 |
| 410. | 1.21 | 1075. | 1.06 |
| 411. | 1.21 | 1076. | 1.06 |
| 412. | 1.21 | 1077. | 1.06 |
| 413. | 1.21 | 1078. | 1.06 |
| 414. | 1.21 | 1079. | 1.06 |
| 415. | 1.21 | 1080. | 1.06 |
| 416. | 1.21 | 1081. | 1.06 |
| 417. | 1.21 | 1082. | 1.06 |
| 418. | 1.21 | 1083. | 1.06 |
| 419. | 1.21 | 1084. | 1.06 |
| 420. | 1.21 | 1085. | 1.06 |
| 421. | 1.21 | 1086. | 1.06 |
| 422. | 1.21 | 1087. | 1.06 |
| 423. | 1.21 | 1088. | 1.06 |
| 424. | 1.2 | 1089. | 1.06 |
| 425. | 1.2 | 1090. | 1.06 |
| 426. | 1.2 | 1091. | 1.06 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 427. | 1.2 | 1092. | 1.06 |
| 428. | 1.2 | 1093. | 1.06 |
| 429. | 1.2 | 1094. | 1.06 |
| 430. | 1.2 | 1095. | 1.06 |
| 431. | 1.2 | 1096. | 1.06 |
| 432. | 1.2 | 1097. | 1.06 |
| 433. | 1.2 | 1098. | 1.06 |
| 434. | 1.2 | 1099. | 1.06 |
| 435. | 1.2 | 1100. | 1.06 |
| 436. | 1.2 | 1101. | 1.06 |
| 437. | 1.2 | 1102. | 1.06 |
| 438. | 1.2 | 1103. | 1.06 |
| 439. | 1.2 | 1104. | 1.06 |
| 440. | 1.2 | 1105. | 1.06 |
| 441. | 1.2 | 1106. | 1.06 |
| 442. | 1.2 | 1107. | 1.06 |
| 443. | 1.2 | 1108. | 1.06 |
| 444. | 1.2 | 1109. | 1.06 |
| 445. | 1.2 | 1110. | 1.06 |
| 446. | 1.2 | 1111. | 1.06 |
| 447. | 1.2 | 1112. | 1.06 |
| 448. | 1.2 | 1113. | 1.06 |
| 449. | 1.2 | 1114. | 1.05 |
| 450. | 1.2 | 1115. | 1.06 |
| 451. | 1.2 | 1116. | 1.06 |
| 452. | 1.2 | 1117. | 1.06 |
| 453. | 1.19 | 1118. | 1.05 |
| 454. | 1.19 | 1119. | 1.05 |
| 455. | 1.19 | 1120. | 1.05 |
| 456. | 1.19 | 1121. | 1.05 |
| 457. | 1.19 | 1122. | 1.06 |
| 458. | 1.19 | 1123. | 1.05 |
| 459. | 1.19 | 1124. | 1.05 |
| 460. | 1.19 | 1125. | 1.05 |
| 461. | 1.19 | 1126. | 1.05 |
| 462. | 1.19 | 1127. | 1.05 |
| 463. | 1.19 | 1128. | 1.05 |
| 464. | 1.19 | 1129. | 1.05 |
| 465. | 1.19 | 1130. | 1.05 |
| 466. | 1.19 | 1131. | 1.05 |
| 467. | 1.19 | 1132. | 1.05 |
| 468. | 1.19 | 1133. | 1.05 |
| 469. | 1.19 | 1134. | 1.05 |
| 470. | 1.19 | 1135. | 1.05 |
| 471. | 1.19 | 1136. | 1.05 |
| 472. | 1.19 | 1137. | 1.05 |
| 473. | 1.19 | 1138. | 1.05 |
| 474. | 1.19 | 1139. | 1.05 |
| 475. | 1.19 | 1140. | 1.05 |
| 476. | 1.19 | 1141. | 1.05 |
| 477. | 1.19 | 1142. | 1.05 |
| 478. | 1.19 | 1143. | 1.05 |
| 479. | 1.19 | 1144. | 1.05 |
| 480. | 1.19 | 1145. | 1.05 |
| 481. | 1.19 | 1146. | 1.05 |
| 482. | 1.19 | 1147. | 1.05 |
| 483. | 1.19 | 1148. | 1.05 |
| 484. | 1.19 | 1149. | 1.05 |
| 485. | 1.18 | 1150. | 1.05 |
| 486. | 1.18 | 1151. | 1.05 |
| 487. | 1.18 | 1152. | 1.05 |
| 488. | 1.18 | 1153. | 1.05 |
| 489. | 1.18 | 1154. | 1.05 |
| 490. | 1.18 | 1155. | 1.05 |
| 491. | 1.18 | 1156. | 1.05 |
| 492. | 1.18 | 1157. | 1.05 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 493. | 1.18 | 1158. | 1.05 |
| 494. | 1.18 | 1159. | 1.05 |
| 495. | 1.18 | 1160. | 1.05 |
| 496. | 1.18 | 1161. | 1.05 |
| 497. | 1.18 | 1162. | 1.05 |
| 498. | 1.18 | 1163. | 1.05 |
| 499. | 1.18 | 1164. | 1.05 |
| 500. | 1.18 | 1165. | 1.05 |
| 501. | 1.18 | 1166. | 1.05 |
| 502. | 1.18 | 1167. | 1.05 |
| 503. | 1.18 | 1168. | 1.05 |
| 504. | 1.18 | 1169. | 1.05 |
| 505. | 1.18 | 1170. | 1.05 |
| 506. | 1.18 | 1171. | 1.05 |
| 507. | 1.18 | 1172. | 1.05 |
| 508. | 1.18 | 1173. | 1.05 |
| 509. | 1.18 | 1174. | 1.05 |
| 510. | 1.18 | 1175. | 1.05 |
| 511. | 1.18 | 1176. | 1.05 |
| 512. | 1.18 | 1177. | 1.05 |
| 513. | 1.18 | 1178. | 1.05 |
| 514. | 1.18 | 1179. | 1.05 |
| 515. | 1.18 | 1180. | 1.05 |
| 516. | 1.18 | 1181. | 1.05 |
| 517. | 1.18 | 1182. | 1.05 |
| 518. | 1.17 | 1183. | 1.05 |
| 519. | 1.17 | 1184. | 1.05 |
| 520. | 1.17 | 1185. | 1.05 |
| 521. | 1.17 | 1186. | 1.05 |
| 522. | 1.17 | 1187. | 1.05 |
| 523. | 1.17 | 1188. | 1.05 |
| 524. | 1.17 | 1189. | 1.05 |
| 525. | 1.17 | 1190. | 1.04 |
| 526. | 1.17 | 1191. | 1.05 |
| 527. | 1.17 | 1192. | 1.04 |
| 528. | 1.17 | 1193. | 1.05 |
| 529. | 1.17 | 1194. | 1.05 |
| 530. | 1.17 | 1195. | 1.05 |
| 531. | 1.17 | 1196. | 1.05 |
| 532. | 1.17 | 1197. | 1.04 |
| 533. | 1.17 | 1198. | 1.04 |
| 534. | 1.17 | 1199. | 1.05 |
| 535. | 1.17 | 1200. | 1.05 |
| 536. | 1.17 | 1201. | 1.05 |
| 537. | 1.17 | 1202. | 1.04 |
| 538. | 1.17 | 1203. | 1.04 |
| 539. | 1.17 | 1204. | 1.04 |
| 540. | 1.17 | 1205. | 1.04 |
| 541. | 1.17 | 1206. | 1.04 |
| 542. | 1.17 | 1207. | 1.04 |
| 543. | 1.17 | 1208. | 1.04 |
| 544. | 1.17 | 1209. | 1.04 |
| 545. | 1.17 | 1210. | 1.04 |
| 546. | 1.17 | 1211. | 1.04 |
| 547. | 1.17 | 1212. | 1.04 |
| 548. | 1.17 | 1213. | 1.04 |
| 549. | 1.17 | 1214. | 1.04 |
| 550. | 1.17 | 1215. | 1.04 |
| 551. | 1.17 | 1216. | 1.04 |
| 552. | 1.17 | 1217. | 1.04 |
| 553. | 1.17 | 1218. | 1.04 |
| 554. | 1.16 | 1219. | 1.04 |
| 555. | 1.16 | 1220. | 1.04 |
| 556. | 1.16 | 1221. | 1.04 |
| 557. | 1.17 | 1222. | 1.04 |
| 558. | 1.16 | 1223. | 1.04 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 559. | 1.16 | 1224. | 1.04 |
| 560. | 1.16 | 1225. | 1.04 |
| 561. | 1.16 | 1226. | 1.04 |
| 562. | 1.16 | 1227. | 1.04 |
| 563. | 1.16 | 1228. | 1.04 |
| 564. | 1.16 | 1229. | 1.04 |
| 565. | 1.16 | 1230. | 1.04 |
| 566. | 1.16 | 1231. | 1.04 |
| 567. | 1.16 | 1232. | 1.04 |
| 568. | 1.16 | 1233. | 1.04 |
| 569. | 1.16 | 1234. | 1.04 |
| 570. | 1.16 | 1235. | 1.04 |
| 571. | 1.16 | 1236. | 1.04 |
| 572. | 1.16 | 1237. | 1.04 |
| 573. | 1.16 | 1238. | 1.04 |
| 574. | 1.16 | 1239. | 1.04 |
| 575. | 1.16 | 1240. | 1.04 |
| 576. | 1.16 | 1241. | 1.04 |
| 577. | 1.16 | 1242. | 1.04 |
| 578. | 1.16 | 1243. | 1.04 |
| 579. | 1.16 | 1244. | 1.04 |
| 580. | 1.16 | 1245. | 1.04 |
| 581. | 1.16 | 1246. | 1.04 |
| 582. | 1.16 | 1247. | 1.04 |
| 583. | 1.16 | 1248. | 1.04 |
| 584. | 1.16 | 1249. | 1.04 |
| 585. | 1.16 | 1250. | 1.04 |
| 586. | 1.16 | 1251. | 1.04 |
| 587. | 1.16 | 1252. | 1.04 |
| 588. | 1.16 | 1253. | 1.04 |
| 589. | 1.16 | 1254. | 1.04 |
| 590. | 1.16 | 1255. | 1.04 |
| 591. | 1.15 | 1256. | 1.04 |
| 592. | 1.15 | 1257. | 1.04 |
| 593. | 1.15 | 1258. | 1.04 |
| 594. | 1.15 | 1259. | 1.04 |
| 595. | 1.15 | 1260. | 1.04 |
| 596. | 1.15 | 1261. | 1.04 |
| 597. | 1.15 | 1262. | 1.04 |
| 598. | 1.15 | 1263. | 1.04 |
| 599. | 1.15 | 1264. | 1.04 |
| 600. | 1.15 | 1265. | 1.04 |
| 601. | 1.15 | 1266. | 1.04 |
| 602. | 1.15 | 1267. | 1.04 |
| 603. | 1.15 | 1268. | 1.04 |
| 604. | 1.15 | 1269. | 1.04 |
| 605. | 1.15 | 1270. | 1.04 |
| 606. | 1.15 | 1271. | 1.04 |
| 607. | 1.15 | 1272. | 1.04 |
| 608. | 1.15 | 1273. | 1.04 |
| 609. | 1.15 | 1274. | 1.04 |
| 610. | 1.15 | 1275. | 1.04 |
| 611. | 1.15 | 1276. | 1.04 |
| 612. | 1.15 | 1277. | 1.03 |
| 613. | 1.15 | 1278. | 1.03 |
| 614. | 1.15 | 1279. | 1.04 |
| 615. | 1.15 | 1280. | 1.04 |
| 616. | 1.15 | 1281. | 1.04 |
| 617. | 1.15 | 1282. | 1.04 |
| 618. | 1.15 | 1283. | 1.03 |
| 619. | 1.15 | 1284. | 1.03 |
| 620. | 1.15 | 1285. | 1.03 |
| 621. | 1.15 | 1286. | 1.03 |
| 622. | 1.15 | 1287. | 1.03 |
| 623. | 1.15 | 1288. | 1.03 |
| 624. | 1.15 | 1289. | 1.03 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 625. | 1.15 | 1290. | 1.03 |
| 626. | 1.14 | 1291. | 1.03 |
| 627. | 1.14 | 1292. | 1.03 |
| 628. | 1.14 | 1293. | 1.03 |
| 629. | 1.14 | 1294. | 1.03 |
| 630. | 1.14 | 1295. | 1.03 |
| 631. | 1.14 | 1296. | 1.03 |
| 632. | 1.14 | 1297. | 1.03 |
| 633. | 1.14 | 1298. | 1.03 |
| 634. | 1.14 | 1299. | 1.03 |
| 635. | 1.14 | 1300. | 1.03 |
| 636. | 1.14 | 1301. | 1.03 |
| 637. | 1.14 | 1302. | 1.03 |
| 638. | 1.14 | 1303. | 1.03 |
| 639. | 1.14 | 1304. | 1.03 |
| 640. | 1.14 | 1305. | 1.03 |
| 641. | 1.14 | 1306. | 1.03 |
| 642. | 1.14 | 1307. | 1.03 |
| 643. | 1.14 | 1308. | 1.03 |
| 644. | 1.14 | 1309. | 1.03 |
| 645. | 1.14 | 1310. | 1.03 |
| 646. | 1.14 | 1311. | 1.03 |
| 647. | 1.14 | 1312. | 1.03 |
| 648. | 1.14 | 1313. | 1.03 |
| 649. | 1.14 | 1314. | 1.03 |
| 650. | 1.14 | 1315. | 1.03 |
| 651. | 1.14 | 1316. | 1.03 |
| 652. | 1.14 | 1317. | 1.03 |
| 653. | 1.14 | 1318. | 1.03 |
| 654. | 1.14 | 1319. | 1.03 |
| 655. | 1.14 | 1320. | 1.03 |
| 656. | 1.14 | 1321. | 1.03 |
| 657. | 1.14 | 1322. | 1.03 |
| 658. | 1.14 | 1323. | 1.03 |
| 659. | 1.14 | 1324. | 1.03 |
| 660. | 1.14 | 1325. | 1.03 |
| 661. | 1.14 | 1326. | 1.03 |
| 662. | 1.14 | 1327. | 1.03 |
| 663. | 1.14 | 1328. | 1.03 |
| 664. | 1.14 | 1329. | 1.03 |
| 665. | 1.14 | 1330. | 1.03 |
| 666. | 1.14 | | |

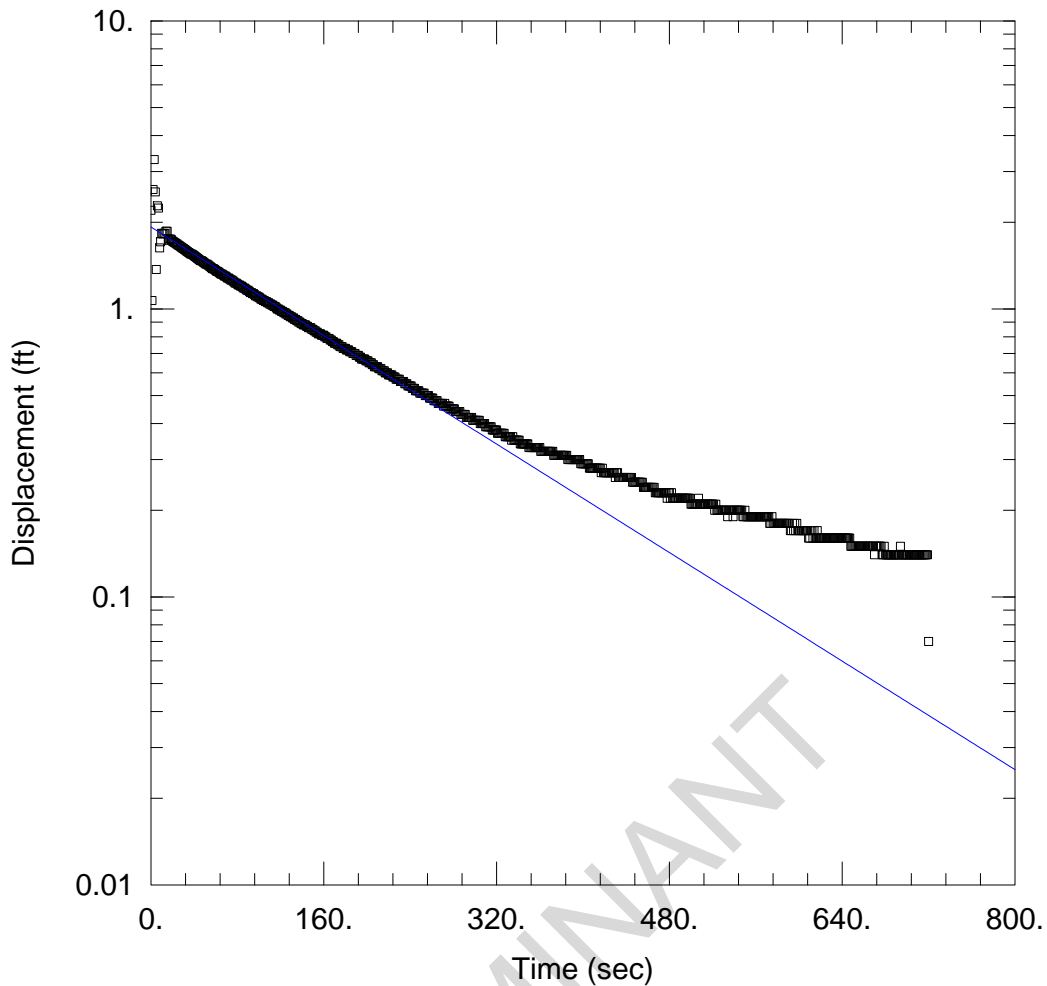
SOLUTION

Slug Test
 Aquifer Model: Unconfined
 Solution Method: Bouwer-Rice
 ln(Re/rw): 2.589

VISUAL ESTIMATION RESULTSEstimated Parameters

| <u>Parameter</u> | <u>Estimate</u> | |
|------------------|-----------------|--------|
| K | 5.977E-6 | cm/sec |
| y0 | 1.351 | ft |

$$T = K \cdot b = 0.004161 \text{ cm}^2/\text{sec}$$



PDP-25 SLUG IN

Data Set: J:\...\PDP-25 Slug In.aqt
 Date: 12/16/15

Time: 10:25:24

PROJECT INFORMATION

Company: PBW
 Client: Luminant
 Project: 5164
 Location: MLSES
 Test Well: PDP-25
 Test Date: 10/7/15

AQUIFER DATA

Saturated Thickness: 24. ft

Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (PDP-25)

Initial Displacement: 2.2 ft
 Total Well Penetration Depth: 16. ft
 Casing Radius: 0.083 ft

Static Water Column Height: 38.89 ft
 Screen Length: 10. ft
 Well Radius: 0.27 ft

SOLUTION

Aquifer Model: Confined
 K = 0.0001494 cm/sec

Solution Method: Bowser-Rice
 y0 = 1.925 ft

Data Set: J:\5164 - Luminant CCR Well Installation and GW Sampling\5164-B_Martin Lake\Slug Tests\PDP5\Aqtes
 Title: PDP-25 Slug In
 Date: 12/16/15
 Time: 10:26:36

PROJECT INFORMATION

Company: PBW
 Client: Luminant
 Project: 5164
 Location: MLSES
 Test Date: 10/7/15
 Test Well: PDP-25

AQUIFER DATA

Saturated Thickness: 24. ft
 Anisotropy Ratio (Kz/Kr): 1.

SLUG TEST WELL DATA

Test Well: PDP-25

X Location: 0. ft
 Y Location: 0. ft

Initial Displacement: 2.2 ft
 Static Water Column Height: 38.89 ft
 Casing Radius: 0.083 ft
 Well Radius: 0.27 ft
 Well Skin Radius: 0.27 ft
 Screen Length: 10. ft
 Total Well Penetration Depth: 16. ft

No. of Observations: 720

| Observation Data | | | |
|------------------|-------------------|------------|-------------------|
| Time (sec) | Displacement (ft) | Time (sec) | Displacement (ft) |
| 1. | 1.07 | 361. | 0.32 |
| 2. | 2.6 | 362. | 0.32 |
| 3. | 3.3 | 363. | 0.32 |
| 4. | 2.55 | 364. | 0.32 |
| 5. | 1.37 | 365. | 0.32 |
| 6. | 2.28 | 366. | 0.32 |
| 7. | 2.24 | 367. | 0.32 |
| 8. | 1.63 | 368. | 0.32 |
| 9. | 1.71 | 369. | 0.32 |
| 10. | 1.83 | 370. | 0.32 |
| 11. | 1.82 | 371. | 0.32 |
| 12. | 1.83 | 372. | 0.32 |
| 13. | 1.83 | 373. | 0.31 |
| 14. | 1.86 | 374. | 0.31 |
| 15. | 1.86 | 375. | 0.31 |
| 16. | 1.75 | 376. | 0.31 |
| 17. | 1.73 | 377. | 0.31 |
| 18. | 1.75 | 378. | 0.31 |
| 19. | 1.74 | 379. | 0.31 |
| 20. | 1.72 | 380. | 0.31 |
| 21. | 1.71 | 381. | 0.31 |
| 22. | 1.7 | 382. | 0.31 |
| 23. | 1.69 | 383. | 0.31 |
| 24. | 1.68 | 384. | 0.31 |
| 25. | 1.67 | 385. | 0.31 |
| 26. | 1.66 | 386. | 0.3 |
| 27. | 1.65 | 387. | 0.3 |
| 28. | 1.64 | 388. | 0.3 |
| 29. | 1.63 | 389. | 0.3 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 30. | 1.62 | 390. | 0.3 |
| 31. | 1.61 | 391. | 0.3 |
| 32. | 1.6 | 392. | 0.3 |
| 33. | 1.59 | 393. | 0.3 |
| 34. | 1.58 | 394. | 0.3 |
| 35. | 1.57 | 395. | 0.3 |
| 36. | 1.56 | 396. | 0.3 |
| 37. | 1.55 | 397. | 0.3 |
| 38. | 1.55 | 398. | 0.29 |
| 39. | 1.54 | 399. | 0.29 |
| 40. | 1.53 | 400. | 0.29 |
| 41. | 1.52 | 401. | 0.29 |
| 42. | 1.51 | 402. | 0.29 |
| 43. | 1.5 | 403. | 0.29 |
| 44. | 1.49 | 404. | 0.29 |
| 45. | 1.48 | 405. | 0.29 |
| 46. | 1.47 | 406. | 0.28 |
| 47. | 1.47 | 407. | 0.28 |
| 48. | 1.46 | 408. | 0.28 |
| 49. | 1.45 | 409. | 0.28 |
| 50. | 1.44 | 410. | 0.28 |
| 51. | 1.43 | 411. | 0.28 |
| 52. | 1.43 | 412. | 0.28 |
| 53. | 1.42 | 413. | 0.28 |
| 54. | 1.41 | 414. | 0.28 |
| 55. | 1.4 | 415. | 0.28 |
| 56. | 1.39 | 416. | 0.28 |
| 57. | 1.38 | 417. | 0.27 |
| 58. | 1.38 | 418. | 0.28 |
| 59. | 1.37 | 419. | 0.27 |
| 60. | 1.36 | 420. | 0.27 |
| 61. | 1.35 | 421. | 0.27 |
| 62. | 1.35 | 422. | 0.27 |
| 63. | 1.34 | 423. | 0.27 |
| 64. | 1.33 | 424. | 0.27 |
| 65. | 1.32 | 425. | 0.27 |
| 66. | 1.32 | 426. | 0.27 |
| 67. | 1.31 | 427. | 0.27 |
| 68. | 1.3 | 428. | 0.27 |
| 69. | 1.3 | 429. | 0.27 |
| 70. | 1.29 | 430. | 0.26 |
| 71. | 1.28 | 431. | 0.27 |
| 72. | 1.28 | 432. | 0.27 |
| 73. | 1.27 | 433. | 0.26 |
| 74. | 1.26 | 434. | 0.26 |
| 75. | 1.26 | 435. | 0.26 |
| 76. | 1.25 | 436. | 0.26 |
| 77. | 1.24 | 437. | 0.26 |
| 78. | 1.23 | 438. | 0.26 |
| 79. | 1.23 | 439. | 0.26 |
| 80. | 1.22 | 440. | 0.26 |
| 81. | 1.21 | 441. | 0.26 |
| 82. | 1.21 | 442. | 0.26 |
| 83. | 1.2 | 443. | 0.26 |
| 84. | 1.2 | 444. | 0.26 |
| 85. | 1.19 | 445. | 0.26 |
| 86. | 1.18 | 446. | 0.25 |
| 87. | 1.18 | 447. | 0.25 |
| 88. | 1.17 | 448. | 0.25 |
| 89. | 1.16 | 449. | 0.25 |
| 90. | 1.16 | 450. | 0.25 |
| 91. | 1.15 | 451. | 0.25 |
| 92. | 1.14 | 452. | 0.25 |
| 93. | 1.14 | 453. | 0.25 |
| 94. | 1.13 | 454. | 0.25 |
| 95. | 1.13 | 455. | 0.25 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 96. | 1.12 | 456. | 0.24 |
| 97. | 1.11 | 457. | 0.24 |
| 98. | 1.11 | 458. | 0.24 |
| 99. | 1.1 | 459. | 0.24 |
| 100. | 1.1 | 460. | 0.24 |
| 101. | 1.09 | 461. | 0.24 |
| 102. | 1.08 | 462. | 0.24 |
| 103. | 1.08 | 463. | 0.24 |
| 104. | 1.07 | 464. | 0.24 |
| 105. | 1.07 | 465. | 0.24 |
| 106. | 1.06 | 466. | 0.24 |
| 107. | 1.06 | 467. | 0.23 |
| 108. | 1.05 | 468. | 0.23 |
| 109. | 1.05 | 469. | 0.23 |
| 110. | 1.04 | 470. | 0.23 |
| 111. | 1.04 | 471. | 0.23 |
| 112. | 1.03 | 472. | 0.23 |
| 113. | 1.03 | 473. | 0.23 |
| 114. | 1.02 | 474. | 0.23 |
| 115. | 1.02 | 475. | 0.23 |
| 116. | 1.01 | 476. | 0.23 |
| 117. | 1. | 477. | 0.23 |
| 118. | 1. | 478. | 0.22 |
| 119. | 0.99 | 479. | 0.23 |
| 120. | 0.99 | 480. | 0.23 |
| 121. | 0.98 | 481. | 0.22 |
| 122. | 0.98 | 482. | 0.23 |
| 123. | 0.97 | 483. | 0.22 |
| 124. | 0.97 | 484. | 0.22 |
| 125. | 0.96 | 485. | 0.22 |
| 126. | 0.96 | 486. | 0.22 |
| 127. | 0.95 | 487. | 0.22 |
| 128. | 0.95 | 488. | 0.22 |
| 129. | 0.94 | 489. | 0.22 |
| 130. | 0.94 | 490. | 0.22 |
| 131. | 0.93 | 491. | 0.22 |
| 132. | 0.93 | 492. | 0.22 |
| 133. | 0.92 | 493. | 0.22 |
| 134. | 0.92 | 494. | 0.22 |
| 135. | 0.91 | 495. | 0.22 |
| 136. | 0.91 | 496. | 0.22 |
| 137. | 0.9 | 497. | 0.22 |
| 138. | 0.9 | 498. | 0.22 |
| 139. | 0.89 | 499. | 0.22 |
| 140. | 0.89 | 500. | 0.21 |
| 141. | 0.88 | 501. | 0.21 |
| 142. | 0.88 | 502. | 0.21 |
| 143. | 0.88 | 503. | 0.21 |
| 144. | 0.87 | 504. | 0.21 |
| 145. | 0.87 | 505. | 0.21 |
| 146. | 0.86 | 506. | 0.21 |
| 147. | 0.86 | 507. | 0.22 |
| 148. | 0.86 | 508. | 0.21 |
| 149. | 0.85 | 509. | 0.21 |
| 150. | 0.85 | 510. | 0.21 |
| 151. | 0.84 | 511. | 0.21 |
| 152. | 0.84 | 512. | 0.21 |
| 153. | 0.83 | 513. | 0.21 |
| 154. | 0.83 | 514. | 0.21 |
| 155. | 0.82 | 515. | 0.21 |
| 156. | 0.82 | 516. | 0.21 |
| 157. | 0.82 | 517. | 0.21 |
| 158. | 0.81 | 518. | 0.21 |
| 159. | 0.81 | 519. | 0.21 |
| 160. | 0.81 | 520. | 0.21 |
| 161. | 0.8 | 521. | 0.21 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 162. | 0.8 | 522. | 0.2 |
| 163. | 0.79 | 523. | 0.21 |
| 164. | 0.79 | 524. | 0.2 |
| 165. | 0.79 | 525. | 0.2 |
| 166. | 0.78 | 526. | 0.2 |
| 167. | 0.78 | 527. | 0.2 |
| 168. | 0.77 | 528. | 0.2 |
| 169. | 0.77 | 529. | 0.2 |
| 170. | 0.76 | 530. | 0.2 |
| 171. | 0.76 | 531. | 0.2 |
| 172. | 0.76 | 532. | 0.2 |
| 173. | 0.75 | 533. | 0.2 |
| 174. | 0.75 | 534. | 0.19 |
| 175. | 0.74 | 535. | 0.2 |
| 176. | 0.74 | 536. | 0.2 |
| 177. | 0.74 | 537. | 0.2 |
| 178. | 0.73 | 538. | 0.2 |
| 179. | 0.73 | 539. | 0.19 |
| 180. | 0.73 | 540. | 0.2 |
| 181. | 0.72 | 541. | 0.2 |
| 182. | 0.72 | 542. | 0.2 |
| 183. | 0.72 | 543. | 0.2 |
| 184. | 0.71 | 544. | 0.2 |
| 185. | 0.71 | 545. | 0.2 |
| 186. | 0.71 | 546. | 0.2 |
| 187. | 0.7 | 547. | 0.2 |
| 188. | 0.7 | 548. | 0.19 |
| 189. | 0.7 | 549. | 0.19 |
| 190. | 0.69 | 550. | 0.2 |
| 191. | 0.69 | 551. | 0.19 |
| 192. | 0.69 | 552. | 0.19 |
| 193. | 0.68 | 553. | 0.19 |
| 194. | 0.68 | 554. | 0.19 |
| 195. | 0.67 | 555. | 0.19 |
| 196. | 0.67 | 556. | 0.19 |
| 197. | 0.67 | 557. | 0.19 |
| 198. | 0.67 | 558. | 0.19 |
| 199. | 0.66 | 559. | 0.19 |
| 200. | 0.66 | 560. | 0.19 |
| 201. | 0.66 | 561. | 0.19 |
| 202. | 0.65 | 562. | 0.19 |
| 203. | 0.65 | 563. | 0.19 |
| 204. | 0.65 | 564. | 0.19 |
| 205. | 0.64 | 565. | 0.19 |
| 206. | 0.64 | 566. | 0.19 |
| 207. | 0.63 | 567. | 0.19 |
| 208. | 0.63 | 568. | 0.19 |
| 209. | 0.63 | 569. | 0.19 |
| 210. | 0.63 | 570. | 0.19 |
| 211. | 0.62 | 571. | 0.19 |
| 212. | 0.62 | 572. | 0.19 |
| 213. | 0.62 | 573. | 0.18 |
| 214. | 0.61 | 574. | 0.18 |
| 215. | 0.61 | 575. | 0.19 |
| 216. | 0.61 | 576. | 0.18 |
| 217. | 0.6 | 577. | 0.18 |
| 218. | 0.6 | 578. | 0.18 |
| 219. | 0.6 | 579. | 0.18 |
| 220. | 0.59 | 580. | 0.18 |
| 221. | 0.59 | 581. | 0.18 |
| 222. | 0.59 | 582. | 0.18 |
| 223. | 0.59 | 583. | 0.18 |
| 224. | 0.58 | 584. | 0.18 |
| 225. | 0.58 | 585. | 0.18 |
| 226. | 0.58 | 586. | 0.18 |
| 227. | 0.57 | 587. | 0.18 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 228. | 0.57 | 588. | 0.18 |
| 229. | 0.57 | 589. | 0.18 |
| 230. | 0.57 | 590. | 0.18 |
| 231. | 0.56 | 591. | 0.18 |
| 232. | 0.56 | 592. | 0.17 |
| 233. | 0.56 | 593. | 0.17 |
| 234. | 0.56 | 594. | 0.18 |
| 235. | 0.55 | 595. | 0.17 |
| 236. | 0.55 | 596. | 0.18 |
| 237. | 0.55 | 597. | 0.17 |
| 238. | 0.54 | 598. | 0.18 |
| 239. | 0.54 | 599. | 0.17 |
| 240. | 0.54 | 600. | 0.17 |
| 241. | 0.54 | 601. | 0.17 |
| 242. | 0.53 | 602. | 0.17 |
| 243. | 0.53 | 603. | 0.17 |
| 244. | 0.53 | 604. | 0.17 |
| 245. | 0.52 | 605. | 0.17 |
| 246. | 0.52 | 606. | 0.17 |
| 247. | 0.52 | 607. | 0.17 |
| 248. | 0.52 | 608. | 0.17 |
| 249. | 0.51 | 609. | 0.16 |
| 250. | 0.51 | 610. | 0.16 |
| 251. | 0.51 | 611. | 0.17 |
| 252. | 0.51 | 612. | 0.17 |
| 253. | 0.51 | 613. | 0.16 |
| 254. | 0.5 | 614. | 0.17 |
| 255. | 0.5 | 615. | 0.16 |
| 256. | 0.5 | 616. | 0.16 |
| 257. | 0.5 | 617. | 0.17 |
| 258. | 0.49 | 618. | 0.16 |
| 259. | 0.49 | 619. | 0.16 |
| 260. | 0.49 | 620. | 0.16 |
| 261. | 0.49 | 621. | 0.16 |
| 262. | 0.48 | 622. | 0.16 |
| 263. | 0.48 | 623. | 0.16 |
| 264. | 0.48 | 624. | 0.16 |
| 265. | 0.48 | 625. | 0.16 |
| 266. | 0.47 | 626. | 0.16 |
| 267. | 0.47 | 627. | 0.16 |
| 268. | 0.47 | 628. | 0.16 |
| 269. | 0.47 | 629. | 0.16 |
| 270. | 0.47 | 630. | 0.16 |
| 271. | 0.46 | 631. | 0.16 |
| 272. | 0.47 | 632. | 0.16 |
| 273. | 0.46 | 633. | 0.16 |
| 274. | 0.46 | 634. | 0.16 |
| 275. | 0.46 | 635. | 0.16 |
| 276. | 0.46 | 636. | 0.16 |
| 277. | 0.45 | 637. | 0.16 |
| 278. | 0.45 | 638. | 0.16 |
| 279. | 0.45 | 639. | 0.16 |
| 280. | 0.45 | 640. | 0.16 |
| 281. | 0.45 | 641. | 0.16 |
| 282. | 0.44 | 642. | 0.16 |
| 283. | 0.44 | 643. | 0.16 |
| 284. | 0.44 | 644. | 0.16 |
| 285. | 0.44 | 645. | 0.16 |
| 286. | 0.44 | 646. | 0.16 |
| 287. | 0.43 | 647. | 0.16 |
| 288. | 0.43 | 648. | 0.15 |
| 289. | 0.43 | 649. | 0.15 |
| 290. | 0.43 | 650. | 0.15 |
| 291. | 0.43 | 651. | 0.15 |
| 292. | 0.42 | 652. | 0.15 |
| 293. | 0.42 | 653. | 0.15 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 294. | 0.42 | 654. | 0.15 |
| 295. | 0.42 | 655. | 0.15 |
| 296. | 0.42 | 656. | 0.15 |
| 297. | 0.42 | 657. | 0.15 |
| 298. | 0.41 | 658. | 0.15 |
| 299. | 0.41 | 659. | 0.15 |
| 300. | 0.41 | 660. | 0.15 |
| 301. | 0.41 | 661. | 0.15 |
| 302. | 0.41 | 662. | 0.15 |
| 303. | 0.41 | 663. | 0.15 |
| 304. | 0.41 | 664. | 0.15 |
| 305. | 0.4 | 665. | 0.15 |
| 306. | 0.4 | 666. | 0.15 |
| 307. | 0.4 | 667. | 0.15 |
| 308. | 0.4 | 668. | 0.15 |
| 309. | 0.4 | 669. | 0.15 |
| 310. | 0.39 | 670. | 0.14 |
| 311. | 0.39 | 671. | 0.15 |
| 312. | 0.39 | 672. | 0.15 |
| 313. | 0.39 | 673. | 0.15 |
| 314. | 0.39 | 674. | 0.15 |
| 315. | 0.39 | 675. | 0.15 |
| 316. | 0.38 | 676. | 0.15 |
| 317. | 0.38 | 677. | 0.14 |
| 318. | 0.38 | 678. | 0.14 |
| 319. | 0.38 | 679. | 0.15 |
| 320. | 0.38 | 680. | 0.14 |
| 321. | 0.37 | 681. | 0.14 |
| 322. | 0.37 | 682. | 0.14 |
| 323. | 0.37 | 683. | 0.14 |
| 324. | 0.37 | 684. | 0.14 |
| 325. | 0.37 | 685. | 0.14 |
| 326. | 0.37 | 686. | 0.14 |
| 327. | 0.37 | 687. | 0.14 |
| 328. | 0.36 | 688. | 0.14 |
| 329. | 0.36 | 689. | 0.14 |
| 330. | 0.36 | 690. | 0.14 |
| 331. | 0.36 | 691. | 0.14 |
| 332. | 0.36 | 692. | 0.14 |
| 333. | 0.36 | 693. | 0.14 |
| 334. | 0.35 | 694. | 0.15 |
| 335. | 0.36 | 695. | 0.14 |
| 336. | 0.35 | 696. | 0.14 |
| 337. | 0.35 | 697. | 0.14 |
| 338. | 0.35 | 698. | 0.14 |
| 339. | 0.35 | 699. | 0.14 |
| 340. | 0.35 | 700. | 0.14 |
| 341. | 0.35 | 701. | 0.14 |
| 342. | 0.34 | 702. | 0.14 |
| 343. | 0.34 | 703. | 0.14 |
| 344. | 0.34 | 704. | 0.14 |
| 345. | 0.34 | 705. | 0.14 |
| 346. | 0.34 | 706. | 0.14 |
| 347. | 0.34 | 707. | 0.14 |
| 348. | 0.34 | 708. | 0.14 |
| 349. | 0.34 | 709. | 0.14 |
| 350. | 0.33 | 710. | 0.14 |
| 351. | 0.33 | 711. | 0.14 |
| 352. | 0.33 | 712. | 0.14 |
| 353. | 0.33 | 713. | 0.14 |
| 354. | 0.33 | 714. | 0.14 |
| 355. | 0.33 | 715. | 0.14 |
| 356. | 0.33 | 716. | 0.14 |
| 357. | 0.33 | 717. | 0.14 |
| 358. | 0.33 | 718. | 0.14 |
| 359. | 0.33 | 719. | 0.14 |

Time (sec)
360.

Displacement (ft)
0.33

Time (sec)
720.

Displacement (ft)
0.07

SOLUTION

Slug Test
Aquifer Model: Confined
Solution Method: Bouwer-Rice
ln(Re/rw): 2.624

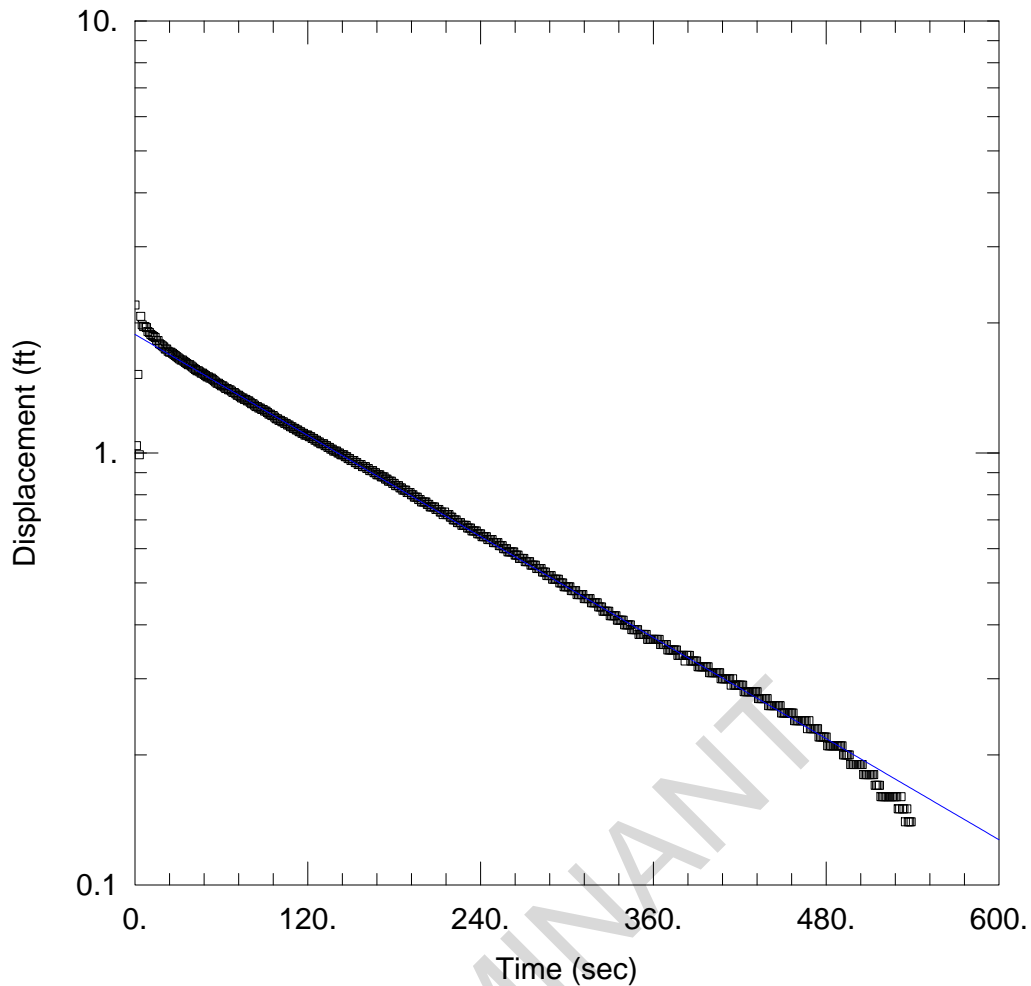
VISUAL ESTIMATION RESULTS

Estimated Parameters

| <u>Parameter</u> | <u>Estimate</u> | |
|------------------|-----------------|--------|
| K | 0.0001494 | cm/sec |
| y0 | 1.925 | ft |

$$T = K \cdot b = 0.1093 \text{ cm}^2/\text{sec}$$

LUMINANT



PDP-25 SLUG OUT

Data Set: J:\...\PDP-25 Slug Out.aqt
 Date: 12/16/15

Time: 10:25:32

PROJECT INFORMATION

Company: PBW
 Client: Luminant
 Project: 5164
 Location: MLSES
 Test Well: PDP-25
 Test Date: 10/7/15

AQUIFER DATA

Saturated Thickness: 24. ft

Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (PDP-25)

Initial Displacement: 2.2 ft
 Total Well Penetration Depth: 16. ft
 Casing Radius: 0.083 ft

Static Water Column Height: 38.89 ft
 Screen Length: 10. ft
 Well Radius: 0.27 ft

SOLUTION

Aquifer Model: Confined
 K = 0.0001237 cm/sec

Solution Method: Bower-Rice
 y0 = 1.881 ft

Data Set: J:\5164 - Luminant CCR Well Installation and GW Sampling\5164-B_Martin Lake\Slug Tests\PDP5\Aqtes
 Title: PDP-25 Slug Out
 Date: 12/16/15
 Time: 10:26:27

PROJECT INFORMATION

Company: PBW
 Client: Luminant
 Project: 5164
 Location: MLSES
 Test Date: 10/7/15
 Test Well: PDP-25

AQUIFER DATA

Saturated Thickness: 24. ft
 Anisotropy Ratio (Kz/Kr): 1.

SLUG TEST WELL DATA

Test Well: PDP-25

X Location: 0. ft
 Y Location: 0. ft

Initial Displacement: 2.2 ft
 Static Water Column Height: 38.89 ft
 Casing Radius: 0.083 ft
 Well Radius: 0.27 ft
 Well Skin Radius: 0.27 ft
 Screen Length: 10. ft
 Total Well Penetration Depth: 16. ft

No. of Observations: 539

| Time (sec) | Observation Data | | Displacement (ft) |
|------------|-------------------|------------|-------------------|
| | Displacement (ft) | Time (sec) | |
| 1. | 1.04 | 271. | 0.56 |
| 2. | 1.52 | 272. | 0.56 |
| 3. | 0.99 | 273. | 0.56 |
| 4. | 2.07 | 274. | 0.56 |
| 5. | 1.98 | 275. | 0.55 |
| 6. | 1.96 | 276. | 0.55 |
| 7. | 1.96 | 277. | 0.55 |
| 8. | 1.95 | 278. | 0.55 |
| 9. | 1.91 | 279. | 0.54 |
| 10. | 1.9 | 280. | 0.54 |
| 11. | 1.88 | 281. | 0.54 |
| 12. | 1.87 | 282. | 0.54 |
| 13. | 1.86 | 283. | 0.53 |
| 14. | 1.85 | 284. | 0.53 |
| 15. | 1.82 | 285. | 0.53 |
| 16. | 1.82 | 286. | 0.52 |
| 17. | 1.79 | 287. | 0.52 |
| 18. | 1.78 | 288. | 0.52 |
| 19. | 1.77 | 289. | 0.52 |
| 20. | 1.76 | 290. | 0.51 |
| 21. | 1.74 | 291. | 0.51 |
| 22. | 1.74 | 292. | 0.51 |
| 23. | 1.72 | 293. | 0.51 |
| 24. | 1.71 | 294. | 0.51 |
| 25. | 1.71 | 295. | 0.5 |
| 26. | 1.7 | 296. | 0.5 |
| 27. | 1.69 | 297. | 0.5 |
| 28. | 1.68 | 298. | 0.49 |
| 29. | 1.67 | 299. | 0.49 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 30. | 1.66 | 300. | 0.49 |
| 31. | 1.65 | 301. | 0.49 |
| 32. | 1.64 | 302. | 0.49 |
| 33. | 1.64 | 303. | 0.48 |
| 34. | 1.63 | 304. | 0.48 |
| 35. | 1.62 | 305. | 0.48 |
| 36. | 1.61 | 306. | 0.48 |
| 37. | 1.6 | 307. | 0.47 |
| 38. | 1.6 | 308. | 0.47 |
| 39. | 1.59 | 309. | 0.47 |
| 40. | 1.58 | 310. | 0.47 |
| 41. | 1.57 | 311. | 0.47 |
| 42. | 1.56 | 312. | 0.46 |
| 43. | 1.55 | 313. | 0.46 |
| 44. | 1.55 | 314. | 0.46 |
| 45. | 1.54 | 315. | 0.46 |
| 46. | 1.53 | 316. | 0.46 |
| 47. | 1.53 | 317. | 0.45 |
| 48. | 1.52 | 318. | 0.45 |
| 49. | 1.51 | 319. | 0.45 |
| 50. | 1.5 | 320. | 0.45 |
| 51. | 1.5 | 321. | 0.45 |
| 52. | 1.49 | 322. | 0.44 |
| 53. | 1.49 | 323. | 0.44 |
| 54. | 1.48 | 324. | 0.44 |
| 55. | 1.47 | 325. | 0.43 |
| 56. | 1.46 | 326. | 0.43 |
| 57. | 1.45 | 327. | 0.43 |
| 58. | 1.45 | 328. | 0.43 |
| 59. | 1.44 | 329. | 0.43 |
| 60. | 1.43 | 330. | 0.42 |
| 61. | 1.43 | 331. | 0.42 |
| 62. | 1.42 | 332. | 0.42 |
| 63. | 1.41 | 333. | 0.42 |
| 64. | 1.41 | 334. | 0.42 |
| 65. | 1.4 | 335. | 0.41 |
| 66. | 1.4 | 336. | 0.41 |
| 67. | 1.39 | 337. | 0.41 |
| 68. | 1.38 | 338. | 0.41 |
| 69. | 1.38 | 339. | 0.41 |
| 70. | 1.37 | 340. | 0.4 |
| 71. | 1.36 | 341. | 0.4 |
| 72. | 1.36 | 342. | 0.4 |
| 73. | 1.35 | 343. | 0.4 |
| 74. | 1.34 | 344. | 0.4 |
| 75. | 1.34 | 345. | 0.39 |
| 76. | 1.33 | 346. | 0.39 |
| 77. | 1.33 | 347. | 0.39 |
| 78. | 1.32 | 348. | 0.39 |
| 79. | 1.32 | 349. | 0.39 |
| 80. | 1.31 | 350. | 0.38 |
| 81. | 1.3 | 351. | 0.38 |
| 82. | 1.3 | 352. | 0.38 |
| 83. | 1.29 | 353. | 0.38 |
| 84. | 1.28 | 354. | 0.38 |
| 85. | 1.28 | 355. | 0.38 |
| 86. | 1.27 | 356. | 0.37 |
| 87. | 1.27 | 357. | 0.37 |
| 88. | 1.26 | 358. | 0.37 |
| 89. | 1.26 | 359. | 0.37 |
| 90. | 1.25 | 360. | 0.37 |
| 91. | 1.25 | 361. | 0.37 |
| 92. | 1.24 | 362. | 0.37 |
| 93. | 1.23 | 363. | 0.37 |
| 94. | 1.23 | 364. | 0.37 |
| 95. | 1.22 | 365. | 0.36 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 96. | 1.22 | 366. | 0.36 |
| 97. | 1.21 | 367. | 0.36 |
| 98. | 1.2 | 368. | 0.36 |
| 99. | 1.2 | 369. | 0.36 |
| 100. | 1.19 | 370. | 0.35 |
| 101. | 1.19 | 371. | 0.35 |
| 102. | 1.18 | 372. | 0.35 |
| 103. | 1.18 | 373. | 0.35 |
| 104. | 1.17 | 374. | 0.35 |
| 105. | 1.17 | 375. | 0.35 |
| 106. | 1.16 | 376. | 0.35 |
| 107. | 1.16 | 377. | 0.34 |
| 108. | 1.15 | 378. | 0.34 |
| 109. | 1.15 | 379. | 0.34 |
| 110. | 1.14 | 380. | 0.34 |
| 111. | 1.14 | 381. | 0.34 |
| 112. | 1.13 | 382. | 0.33 |
| 113. | 1.13 | 383. | 0.34 |
| 114. | 1.12 | 384. | 0.34 |
| 115. | 1.12 | 385. | 0.34 |
| 116. | 1.11 | 386. | 0.33 |
| 117. | 1.11 | 387. | 0.33 |
| 118. | 1.1 | 388. | 0.33 |
| 119. | 1.1 | 389. | 0.33 |
| 120. | 1.1 | 390. | 0.33 |
| 121. | 1.09 | 391. | 0.32 |
| 122. | 1.09 | 392. | 0.32 |
| 123. | 1.08 | 393. | 0.32 |
| 124. | 1.08 | 394. | 0.32 |
| 125. | 1.07 | 395. | 0.32 |
| 126. | 1.07 | 396. | 0.32 |
| 127. | 1.06 | 397. | 0.32 |
| 128. | 1.06 | 398. | 0.32 |
| 129. | 1.05 | 399. | 0.31 |
| 130. | 1.05 | 400. | 0.31 |
| 131. | 1.05 | 401. | 0.31 |
| 132. | 1.04 | 402. | 0.31 |
| 133. | 1.04 | 403. | 0.31 |
| 134. | 1.03 | 404. | 0.31 |
| 135. | 1.03 | 405. | 0.31 |
| 136. | 1.02 | 406. | 0.31 |
| 137. | 1.02 | 407. | 0.3 |
| 138. | 1.01 | 408. | 0.3 |
| 139. | 1.01 | 409. | 0.3 |
| 140. | 1.01 | 410. | 0.3 |
| 141. | 1. | 411. | 0.3 |
| 142. | 1. | 412. | 0.3 |
| 143. | 0.99 | 413. | 0.3 |
| 144. | 0.99 | 414. | 0.29 |
| 145. | 0.99 | 415. | 0.3 |
| 146. | 0.98 | 416. | 0.29 |
| 147. | 0.98 | 417. | 0.29 |
| 148. | 0.97 | 418. | 0.29 |
| 149. | 0.97 | 419. | 0.29 |
| 150. | 0.96 | 420. | 0.29 |
| 151. | 0.96 | 421. | 0.29 |
| 152. | 0.96 | 422. | 0.29 |
| 153. | 0.95 | 423. | 0.28 |
| 154. | 0.95 | 424. | 0.28 |
| 155. | 0.94 | 425. | 0.28 |
| 156. | 0.94 | 426. | 0.28 |
| 157. | 0.94 | 427. | 0.28 |
| 158. | 0.93 | 428. | 0.28 |
| 159. | 0.93 | 429. | 0.28 |
| 160. | 0.93 | 430. | 0.28 |
| 161. | 0.92 | 431. | 0.28 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 162. | 0.92 | 432. | 0.28 |
| 163. | 0.91 | 433. | 0.27 |
| 164. | 0.91 | 434. | 0.27 |
| 165. | 0.91 | 435. | 0.27 |
| 166. | 0.9 | 436. | 0.27 |
| 167. | 0.9 | 437. | 0.27 |
| 168. | 0.89 | 438. | 0.27 |
| 169. | 0.89 | 439. | 0.27 |
| 170. | 0.89 | 440. | 0.26 |
| 171. | 0.88 | 441. | 0.26 |
| 172. | 0.88 | 442. | 0.26 |
| 173. | 0.88 | 443. | 0.26 |
| 174. | 0.87 | 444. | 0.26 |
| 175. | 0.87 | 445. | 0.26 |
| 176. | 0.86 | 446. | 0.26 |
| 177. | 0.86 | 447. | 0.26 |
| 178. | 0.86 | 448. | 0.26 |
| 179. | 0.85 | 449. | 0.25 |
| 180. | 0.85 | 450. | 0.25 |
| 181. | 0.84 | 451. | 0.25 |
| 182. | 0.84 | 452. | 0.25 |
| 183. | 0.84 | 453. | 0.25 |
| 184. | 0.83 | 454. | 0.25 |
| 185. | 0.83 | 455. | 0.25 |
| 186. | 0.82 | 456. | 0.25 |
| 187. | 0.82 | 457. | 0.25 |
| 188. | 0.82 | 458. | 0.24 |
| 189. | 0.81 | 459. | 0.24 |
| 190. | 0.81 | 460. | 0.24 |
| 191. | 0.81 | 461. | 0.24 |
| 192. | 0.8 | 462. | 0.24 |
| 193. | 0.8 | 463. | 0.24 |
| 194. | 0.79 | 464. | 0.24 |
| 195. | 0.79 | 465. | 0.24 |
| 196. | 0.79 | 466. | 0.24 |
| 197. | 0.78 | 467. | 0.23 |
| 198. | 0.78 | 468. | 0.24 |
| 199. | 0.77 | 469. | 0.23 |
| 200. | 0.77 | 470. | 0.23 |
| 201. | 0.77 | 471. | 0.23 |
| 202. | 0.77 | 472. | 0.23 |
| 203. | 0.76 | 473. | 0.23 |
| 204. | 0.76 | 474. | 0.23 |
| 205. | 0.75 | 475. | 0.22 |
| 206. | 0.75 | 476. | 0.22 |
| 207. | 0.75 | 477. | 0.22 |
| 208. | 0.75 | 478. | 0.22 |
| 209. | 0.74 | 479. | 0.22 |
| 210. | 0.74 | 480. | 0.22 |
| 211. | 0.74 | 481. | 0.21 |
| 212. | 0.73 | 482. | 0.21 |
| 213. | 0.73 | 483. | 0.21 |
| 214. | 0.72 | 484. | 0.21 |
| 215. | 0.73 | 485. | 0.21 |
| 216. | 0.72 | 486. | 0.21 |
| 217. | 0.72 | 487. | 0.21 |
| 218. | 0.72 | 488. | 0.21 |
| 219. | 0.71 | 489. | 0.21 |
| 220. | 0.71 | 490. | 0.21 |
| 221. | 0.7 | 491. | 0.21 |
| 222. | 0.7 | 492. | 0.2 |
| 223. | 0.7 | 493. | 0.2 |
| 224. | 0.69 | 494. | 0.2 |
| 225. | 0.69 | 495. | 0.2 |
| 226. | 0.69 | 496. | 0.2 |
| 227. | 0.68 | 497. | 0.19 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 228. | 0.68 | 498. | 0.19 |
| 229. | 0.68 | 499. | 0.19 |
| 230. | 0.68 | 500. | 0.19 |
| 231. | 0.67 | 501. | 0.19 |
| 232. | 0.67 | 502. | 0.19 |
| 233. | 0.67 | 503. | 0.19 |
| 234. | 0.66 | 504. | 0.19 |
| 235. | 0.66 | 505. | 0.19 |
| 236. | 0.66 | 506. | 0.18 |
| 237. | 0.66 | 507. | 0.18 |
| 238. | 0.65 | 508. | 0.18 |
| 239. | 0.65 | 509. | 0.18 |
| 240. | 0.65 | 510. | 0.18 |
| 241. | 0.64 | 511. | 0.18 |
| 242. | 0.64 | 512. | 0.18 |
| 243. | 0.64 | 513. | 0.18 |
| 244. | 0.64 | 514. | 0.17 |
| 245. | 0.63 | 515. | 0.17 |
| 246. | 0.63 | 516. | 0.17 |
| 247. | 0.63 | 517. | 0.17 |
| 248. | 0.63 | 518. | 0.16 |
| 249. | 0.62 | 519. | 0.16 |
| 250. | 0.62 | 520. | 0.16 |
| 251. | 0.62 | 521. | 0.16 |
| 252. | 0.62 | 522. | 0.16 |
| 253. | 0.61 | 523. | 0.16 |
| 254. | 0.61 | 524. | 0.16 |
| 255. | 0.61 | 525. | 0.16 |
| 256. | 0.6 | 526. | 0.16 |
| 257. | 0.6 | 527. | 0.16 |
| 258. | 0.6 | 528. | 0.16 |
| 259. | 0.59 | 529. | 0.16 |
| 260. | 0.59 | 530. | 0.15 |
| 261. | 0.59 | 531. | 0.15 |
| 262. | 0.59 | 532. | 0.16 |
| 263. | 0.59 | 533. | 0.15 |
| 264. | 0.58 | 534. | 0.15 |
| 265. | 0.58 | 535. | 0.14 |
| 266. | 0.58 | 536. | 0.15 |
| 267. | 0.57 | 537. | 0.14 |
| 268. | 0.57 | 538. | 0.14 |
| 269. | 0.57 | 539. | 0.14 |
| 270. | 0.57 | | |

SOLUTION

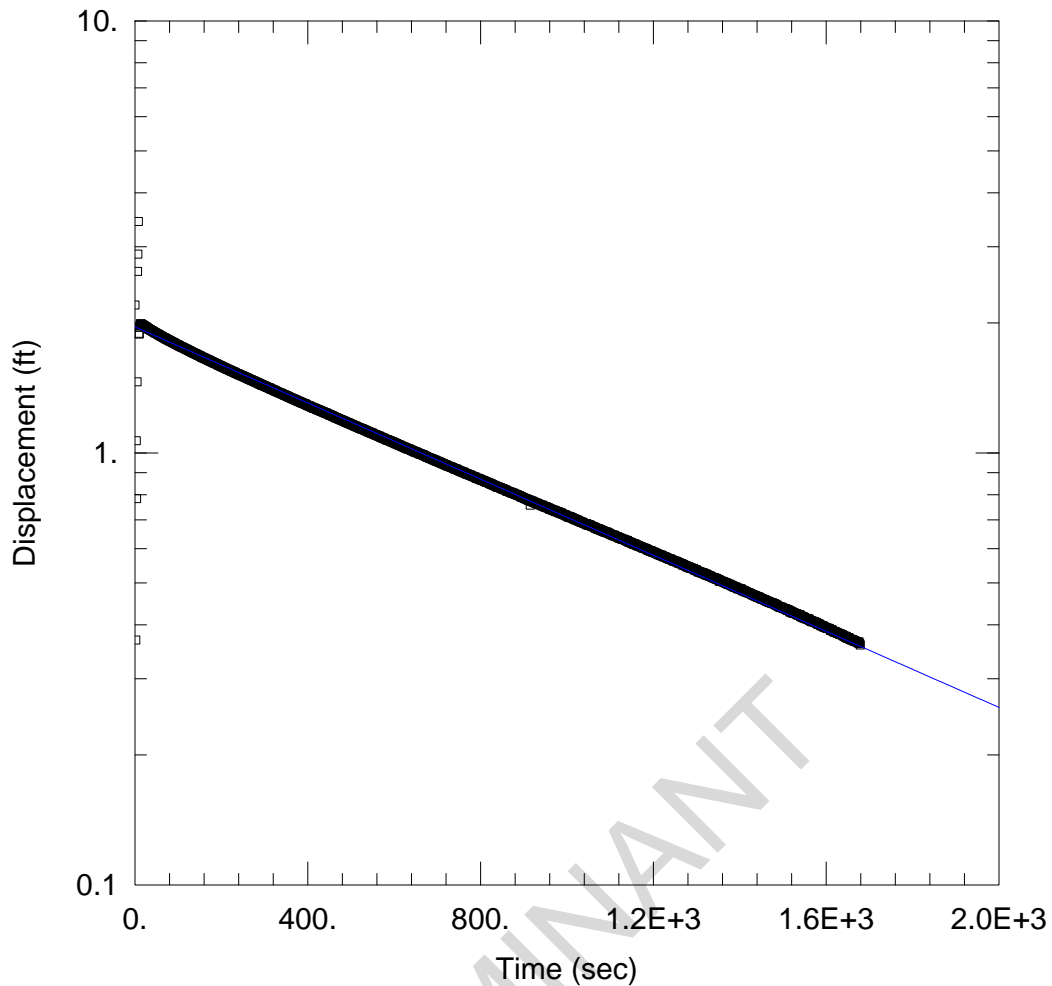
Slug Test
 Aquifer Model: Confined
 Solution Method: Bouwer-Rice
 ln(Re/rw): 2.624

VISUAL ESTIMATION RESULTS

Estimated Parameters

| <u>Parameter</u> | <u>Estimate</u> | |
|------------------|-----------------|--------|
| K | 0.0001237 | cm/sec |
| y0 | 1.881 | ft |

$T = K \cdot b = 0.09046 \text{ cm}^2/\text{sec}$



PDP-26 SLUG IN

Data Set: J:\...\PDP-26 Slug In.aqt
 Date: 12/16/15

Time: 10:25:41

PROJECT INFORMATION

Company: PBW
 Client: Luminant
 Project: 5164
 Location: MLSES
 Test Well: PDP-26
 Test Date: 10/6/15

AQUIFER DATA

Saturated Thickness: 8. ft

Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (PDP-26)

Initial Displacement: 2.2 ft
 Total Well Penetration Depth: 8. ft
 Casing Radius: 0.083 ft

Static Water Column Height: 20.02 ft
 Screen Length: 8. ft
 Well Radius: 0.27 ft

SOLUTION

Aquifer Model: Unconfined
 K = 3.407E-5 cm/sec

Solution Method: Bouwer-Rice
 y0 = 1.958 ft

Data Set: J:\5164 - Luminant CCR Well Installation and GW Sampling\5164-B_Martin Lake\Slug Tests\PDP5\Aqtes
 Title: PDP-26 Slug In
 Date: 12/16/15
 Time: 10:26:18

PROJECT INFORMATION

Company: PBW
 Client: Luminant
 Project: 5164
 Location: MLSES
 Test Date: 10/6/15
 Test Well: PDP-26

AQUIFER DATA

Saturated Thickness: 8. ft
 Anisotropy Ratio (Kz/Kr): 1.

SLUG TEST WELL DATA

Test Well: PDP-26

X Location: 0. ft
 Y Location: 0. ft

Initial Displacement: 2.2 ft
 Static Water Column Height: 20.02 ft
 Casing Radius: 0.083 ft
 Well Radius: 0.27 ft
 Well Skin Radius: 0.27 ft
 Screen Length: 8. ft
 Total Well Penetration Depth: 8. ft

No. of Observations: 1678

| Time (sec) | Observation Data | | Displacement (ft) |
|------------|-------------------|------------|-------------------|
| | Displacement (ft) | Time (sec) | |
| 2. | 0.3688 | 841. | 0.8334 |
| 3. | 1.067 | 842. | 0.833 |
| 4. | 0.7836 | 843. | 0.8319 |
| 5. | 1.461 | 844. | 0.8315 |
| 6. | 2.631 | 845. | 0.8311 |
| 7. | 2.886 | 846. | 0.8291 |
| 8. | 3.433 | 847. | 0.8298 |
| 9. | 1.891 | 848. | 0.8273 |
| 10. | 1.884 | 849. | 0.8279 |
| 11. | 1.953 | 850. | 0.8254 |
| 12. | 1.979 | 851. | 0.8269 |
| 13. | 1.986 | 852. | 0.8246 |
| 14. | 1.991 | 853. | 0.8249 |
| 15. | 1.988 | 854. | 0.8235 |
| 16. | 1.984 | 855. | 0.8228 |
| 17. | 1.982 | 856. | 0.8227 |
| 18. | 1.979 | 857. | 0.8203 |
| 19. | 1.976 | 858. | 0.8212 |
| 20. | 1.973 | 859. | 0.8192 |
| 21. | 1.97 | 860. | 0.8176 |
| 22. | 1.968 | 861. | 0.8161 |
| 23. | 1.963 | 862. | 0.8159 |
| 24. | 1.96 | 863. | 0.8155 |
| 25. | 1.958 | 864. | 0.8148 |
| 26. | 1.957 | 865. | 0.8137 |
| 27. | 1.953 | 866. | 0.8132 |
| 28. | 1.95 | 867. | 0.8137 |
| 29. | 1.947 | 868. | 0.812 |
| 30. | 1.941 | 869. | 0.8111 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 31. | 1.939 | 870. | 0.8099 |
| 32. | 1.936 | 871. | 0.8091 |
| 33. | 1.934 | 872. | 0.8103 |
| 34. | 1.931 | 873. | 0.807 |
| 35. | 1.93 | 874. | 0.8071 |
| 36. | 1.926 | 875. | 0.8072 |
| 37. | 1.923 | 876. | 0.8068 |
| 38. | 1.92 | 877. | 0.8063 |
| 39. | 1.919 | 878. | 0.8043 |
| 40. | 1.915 | 879. | 0.8035 |
| 41. | 1.913 | 880. | 0.8028 |
| 42. | 1.912 | 881. | 0.802 |
| 43. | 1.908 | 882. | 0.8017 |
| 44. | 1.905 | 883. | 0.8008 |
| 45. | 1.902 | 884. | 0.8004 |
| 46. | 1.9 | 885. | 0.7994 |
| 47. | 1.897 | 886. | 0.7985 |
| 48. | 1.895 | 887. | 0.7965 |
| 49. | 1.892 | 888. | 0.7966 |
| 50. | 1.889 | 889. | 0.7968 |
| 51. | 1.888 | 890. | 0.796 |
| 52. | 1.885 | 891. | 0.7954 |
| 53. | 1.883 | 892. | 0.7934 |
| 54. | 1.881 | 893. | 0.7912 |
| 55. | 1.878 | 894. | 0.7915 |
| 56. | 1.875 | 895. | 0.7915 |
| 57. | 1.874 | 896. | 0.79 |
| 58. | 1.869 | 897. | 0.7885 |
| 59. | 1.868 | 898. | 0.7886 |
| 60. | 1.865 | 899. | 0.7879 |
| 61. | 1.863 | 900. | 0.7865 |
| 62. | 1.861 | 901. | 0.7857 |
| 63. | 1.859 | 902. | 0.7846 |
| 64. | 1.857 | 903. | 0.7838 |
| 65. | 1.853 | 904. | 0.7839 |
| 66. | 1.849 | 905. | 0.7832 |
| 67. | 1.849 | 906. | 0.7826 |
| 68. | 1.847 | 907. | 0.7802 |
| 69. | 1.845 | 908. | 0.7813 |
| 70. | 1.842 | 909. | 0.7796 |
| 71. | 1.838 | 910. | 0.7796 |
| 72. | 1.836 | 911. | 0.7769 |
| 73. | 1.835 | 912. | 0.7783 |
| 74. | 1.834 | 913. | 0.7781 |
| 75. | 1.831 | 914. | 0.7762 |
| 76. | 1.827 | 915. | 0.7569 |
| 77. | 1.825 | 916. | 0.7759 |
| 78. | 1.825 | 917. | 0.7727 |
| 79. | 1.822 | 918. | 0.774 |
| 80. | 1.818 | 919. | 0.7726 |
| 81. | 1.816 | 920. | 0.7731 |
| 82. | 1.816 | 921. | 0.7702 |
| 83. | 1.813 | 922. | 0.7703 |
| 84. | 1.811 | 923. | 0.7707 |
| 85. | 1.808 | 924. | 0.7683 |
| 86. | 1.807 | 925. | 0.7686 |
| 87. | 1.804 | 926. | 0.7669 |
| 88. | 1.8 | 927. | 0.766 |
| 89. | 1.799 | 928. | 0.7655 |
| 90. | 1.8 | 929. | 0.7649 |
| 91. | 1.795 | 930. | 0.7656 |
| 92. | 1.792 | 931. | 0.7637 |
| 93. | 1.792 | 932. | 0.7639 |
| 94. | 1.788 | 933. | 0.763 |
| 95. | 1.785 | 934. | 0.7615 |
| 96. | 1.785 | 935. | 0.7603 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 97. | 1.782 | 936. | 0.7602 |
| 98. | 1.78 | 937. | 0.7583 |
| 99. | 1.777 | 938. | 0.7594 |
| 100. | 1.777 | 939. | 0.7584 |
| 101. | 1.774 | 940. | 0.7569 |
| 102. | 1.771 | 941. | 0.7561 |
| 103. | 1.769 | 942. | 0.7551 |
| 104. | 1.768 | 943. | 0.7539 |
| 105. | 1.764 | 944. | 0.7567 |
| 106. | 1.763 | 945. | 0.7537 |
| 107. | 1.761 | 946. | 0.7534 |
| 108. | 1.758 | 947. | 0.7518 |
| 109. | 1.76 | 948. | 0.7511 |
| 110. | 1.754 | 949. | 0.7485 |
| 111. | 1.754 | 950. | 0.7511 |
| 112. | 1.754 | 951. | 0.751 |
| 113. | 1.751 | 952. | 0.7475 |
| 114. | 1.748 | 953. | 0.7488 |
| 115. | 1.745 | 954. | 0.7487 |
| 116. | 1.742 | 955. | 0.7461 |
| 117. | 1.743 | 956. | 0.7464 |
| 118. | 1.74 | 957. | 0.7454 |
| 119. | 1.736 | 958. | 0.7457 |
| 120. | 1.737 | 959. | 0.7418 |
| 121. | 1.734 | 960. | 0.7426 |
| 122. | 1.733 | 961. | 0.7404 |
| 123. | 1.73 | 962. | 0.7424 |
| 124. | 1.728 | 963. | 0.7399 |
| 125. | 1.726 | 964. | 0.739 |
| 126. | 1.724 | 965. | 0.7395 |
| 127. | 1.722 | 966. | 0.7383 |
| 128. | 1.719 | 967. | 0.7368 |
| 129. | 1.718 | 968. | 0.7367 |
| 130. | 1.716 | 969. | 0.7368 |
| 131. | 1.714 | 970. | 0.7343 |
| 132. | 1.711 | 971. | 0.7368 |
| 133. | 1.709 | 972. | 0.7358 |
| 134. | 1.707 | 973. | 0.7353 |
| 135. | 1.706 | 974. | 0.7311 |
| 136. | 1.704 | 975. | 0.7324 |
| 137. | 1.701 | 976. | 0.7319 |
| 138. | 1.698 | 977. | 0.7316 |
| 139. | 1.698 | 978. | 0.7311 |
| 140. | 1.696 | 979. | 0.7291 |
| 141. | 1.694 | 980. | 0.7298 |
| 142. | 1.692 | 981. | 0.7298 |
| 143. | 1.691 | 982. | 0.7282 |
| 144. | 1.689 | 983. | 0.7269 |
| 145. | 1.686 | 984. | 0.7247 |
| 146. | 1.684 | 985. | 0.7255 |
| 147. | 1.683 | 986. | 0.726 |
| 148. | 1.682 | 987. | 0.7263 |
| 149. | 1.679 | 988. | 0.7234 |
| 150. | 1.679 | 989. | 0.7219 |
| 151. | 1.676 | 990. | 0.7218 |
| 152. | 1.673 | 991. | 0.7208 |
| 153. | 1.67 | 992. | 0.7204 |
| 154. | 1.668 | 993. | 0.7204 |
| 155. | 1.667 | 994. | 0.7191 |
| 156. | 1.666 | 995. | 0.7182 |
| 157. | 1.663 | 996. | 0.7171 |
| 158. | 1.661 | 997. | 0.7184 |
| 159. | 1.659 | 998. | 0.7169 |
| 160. | 1.658 | 999. | 0.7157 |
| 161. | 1.657 | 1000. | 0.7131 |
| 162. | 1.655 | 1001. | 0.7141 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 163. | 1.653 | 1002. | 0.7131 |
| 164. | 1.651 | 1003. | 0.7125 |
| 165. | 1.65 | 1004. | 0.7096 |
| 166. | 1.646 | 1005. | 0.7109 |
| 167. | 1.646 | 1006. | 0.713 |
| 168. | 1.644 | 1007. | 0.71 |
| 169. | 1.64 | 1008. | 0.71 |
| 170. | 1.639 | 1009. | 0.7106 |
| 171. | 1.641 | 1010. | 0.7075 |
| 172. | 1.638 | 1011. | 0.7074 |
| 173. | 1.633 | 1012. | 0.7068 |
| 174. | 1.632 | 1013. | 0.707 |
| 175. | 1.632 | 1014. | 0.7056 |
| 176. | 1.629 | 1015. | 0.7044 |
| 177. | 1.626 | 1016. | 0.7038 |
| 178. | 1.626 | 1017. | 0.7011 |
| 179. | 1.623 | 1018. | 0.7037 |
| 180. | 1.622 | 1019. | 0.702 |
| 181. | 1.619 | 1020. | 0.7001 |
| 182. | 1.619 | 1021. | 0.7014 |
| 183. | 1.617 | 1022. | 0.7 |
| 184. | 1.613 | 1023. | 0.6994 |
| 185. | 1.614 | 1024. | 0.6981 |
| 186. | 1.611 | 1025. | 0.6966 |
| 187. | 1.611 | 1026. | 0.6984 |
| 188. | 1.609 | 1027. | 0.6956 |
| 189. | 1.607 | 1028. | 0.6956 |
| 190. | 1.604 | 1029. | 0.6945 |
| 191. | 1.603 | 1030. | 0.6932 |
| 192. | 1.6 | 1031. | 0.6936 |
| 193. | 1.598 | 1032. | 0.6926 |
| 194. | 1.599 | 1033. | 0.6903 |
| 195. | 1.596 | 1034. | 0.6909 |
| 196. | 1.594 | 1035. | 0.6924 |
| 197. | 1.591 | 1036. | 0.6898 |
| 198. | 1.59 | 1037. | 0.6897 |
| 199. | 1.588 | 1038. | 0.6888 |
| 200. | 1.588 | 1039. | 0.6876 |
| 201. | 1.585 | 1040. | 0.6866 |
| 202. | 1.583 | 1041. | 0.6861 |
| 203. | 1.582 | 1042. | 0.6861 |
| 204. | 1.58 | 1043. | 0.6853 |
| 205. | 1.578 | 1044. | 0.6853 |
| 206. | 1.578 | 1045. | 0.6834 |
| 207. | 1.575 | 1046. | 0.686 |
| 208. | 1.573 | 1047. | 0.6818 |
| 209. | 1.571 | 1048. | 0.6818 |
| 210. | 1.57 | 1049. | 0.6807 |
| 211. | 1.569 | 1050. | 0.6808 |
| 212. | 1.565 | 1051. | 0.6796 |
| 213. | 1.564 | 1052. | 0.6814 |
| 214. | 1.561 | 1053. | 0.6815 |
| 215. | 1.562 | 1054. | 0.6791 |
| 216. | 1.56 | 1055. | 0.6784 |
| 217. | 1.559 | 1056. | 0.677 |
| 218. | 1.556 | 1057. | 0.6777 |
| 219. | 1.555 | 1058. | 0.676 |
| 220. | 1.554 | 1059. | 0.6751 |
| 221. | 1.551 | 1060. | 0.6757 |
| 222. | 1.549 | 1061. | 0.6748 |
| 223. | 1.547 | 1062. | 0.6745 |
| 224. | 1.546 | 1063. | 0.6735 |
| 225. | 1.545 | 1064. | 0.6724 |
| 226. | 1.543 | 1065. | 0.6706 |
| 227. | 1.542 | 1066. | 0.6701 |
| 228. | 1.54 | 1067. | 0.6702 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 229. | 1.54 | 1068. | 0.6696 |
| 230. | 1.537 | 1069. | 0.6689 |
| 231. | 1.536 | 1070. | 0.6662 |
| 232. | 1.535 | 1071. | 0.6686 |
| 233. | 1.53 | 1072. | 0.667 |
| 234. | 1.53 | 1073. | 0.666 |
| 235. | 1.528 | 1074. | 0.6665 |
| 236. | 1.526 | 1075. | 0.6641 |
| 237. | 1.525 | 1076. | 0.6659 |
| 238. | 1.525 | 1077. | 0.6635 |
| 239. | 1.523 | 1078. | 0.6622 |
| 240. | 1.52 | 1079. | 0.6638 |
| 241. | 1.517 | 1080. | 0.662 |
| 242. | 1.518 | 1081. | 0.6603 |
| 243. | 1.516 | 1082. | 0.6601 |
| 244. | 1.514 | 1083. | 0.659 |
| 245. | 1.512 | 1084. | 0.6603 |
| 246. | 1.51 | 1085. | 0.6582 |
| 247. | 1.509 | 1086. | 0.6581 |
| 248. | 1.509 | 1087. | 0.6559 |
| 249. | 1.507 | 1088. | 0.6577 |
| 250. | 1.505 | 1089. | 0.6556 |
| 251. | 1.506 | 1090. | 0.6557 |
| 252. | 1.502 | 1091. | 0.6563 |
| 253. | 1.501 | 1092. | 0.6535 |
| 254. | 1.499 | 1093. | 0.6536 |
| 255. | 1.497 | 1094. | 0.6552 |
| 256. | 1.496 | 1095. | 0.6535 |
| 257. | 1.493 | 1096. | 0.6518 |
| 258. | 1.492 | 1097. | 0.6513 |
| 259. | 1.491 | 1098. | 0.6515 |
| 260. | 1.49 | 1099. | 0.6498 |
| 261. | 1.488 | 1100. | 0.6493 |
| 262. | 1.487 | 1101. | 0.6479 |
| 263. | 1.484 | 1102. | 0.6474 |
| 264. | 1.482 | 1103. | 0.6471 |
| 265. | 1.48 | 1104. | 0.6461 |
| 266. | 1.481 | 1105. | 0.6469 |
| 267. | 1.478 | 1106. | 0.6443 |
| 268. | 1.478 | 1107. | 0.6457 |
| 269. | 1.475 | 1108. | 0.6435 |
| 270. | 1.474 | 1109. | 0.6427 |
| 271. | 1.473 | 1110. | 0.6447 |
| 272. | 1.47 | 1111. | 0.6419 |
| 273. | 1.469 | 1112. | 0.6419 |
| 274. | 1.468 | 1113. | 0.6404 |
| 275. | 1.468 | 1114. | 0.641 |
| 276. | 1.464 | 1115. | 0.6397 |
| 277. | 1.464 | 1116. | 0.6398 |
| 278. | 1.462 | 1117. | 0.6394 |
| 279. | 1.46 | 1118. | 0.6387 |
| 280. | 1.459 | 1119. | 0.6375 |
| 281. | 1.458 | 1120. | 0.6358 |
| 282. | 1.456 | 1121. | 0.6361 |
| 283. | 1.454 | 1122. | 0.6351 |
| 284. | 1.452 | 1123. | 0.6357 |
| 285. | 1.452 | 1124. | 0.6346 |
| 286. | 1.451 | 1125. | 0.6337 |
| 287. | 1.446 | 1126. | 0.6326 |
| 288. | 1.446 | 1127. | 0.6322 |
| 289. | 1.445 | 1128. | 0.6314 |
| 290. | 1.443 | 1129. | 0.6319 |
| 291. | 1.442 | 1130. | 0.6306 |
| 292. | 1.439 | 1131. | 0.6312 |
| 293. | 1.438 | 1132. | 0.6307 |
| 294. | 1.437 | 1133. | 0.63 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 295. | 1.436 | 1134. | 0.6293 |
| 296. | 1.435 | 1135. | 0.6287 |
| 297. | 1.433 | 1136. | 0.6277 |
| 298. | 1.432 | 1137. | 0.6257 |
| 299. | 1.43 | 1138. | 0.6271 |
| 300. | 1.428 | 1139. | 0.6264 |
| 301. | 1.427 | 1140. | 0.6274 |
| 302. | 1.426 | 1141. | 0.6239 |
| 303. | 1.424 | 1142. | 0.6225 |
| 304. | 1.423 | 1143. | 0.622 |
| 305. | 1.422 | 1144. | 0.6217 |
| 306. | 1.419 | 1145. | 0.6223 |
| 307. | 1.417 | 1146. | 0.6209 |
| 308. | 1.417 | 1147. | 0.6198 |
| 309. | 1.415 | 1148. | 0.6189 |
| 310. | 1.414 | 1149. | 0.6205 |
| 311. | 1.413 | 1150. | 0.6186 |
| 312. | 1.411 | 1151. | 0.6179 |
| 313. | 1.412 | 1152. | 0.6172 |
| 314. | 1.408 | 1153. | 0.6167 |
| 315. | 1.406 | 1154. | 0.615 |
| 316. | 1.405 | 1155. | 0.6153 |
| 317. | 1.403 | 1156. | 0.6167 |
| 318. | 1.402 | 1157. | 0.6132 |
| 319. | 1.401 | 1158. | 0.6136 |
| 320. | 1.399 | 1159. | 0.6145 |
| 321. | 1.398 | 1160. | 0.6133 |
| 322. | 1.397 | 1161. | 0.6126 |
| 323. | 1.395 | 1162. | 0.6101 |
| 324. | 1.393 | 1163. | 0.6109 |
| 325. | 1.393 | 1164. | 0.61 |
| 326. | 1.389 | 1165. | 0.6098 |
| 327. | 1.389 | 1166. | 0.6095 |
| 328. | 1.387 | 1167. | 0.6076 |
| 329. | 1.386 | 1168. | 0.6069 |
| 330. | 1.385 | 1169. | 0.6075 |
| 331. | 1.382 | 1170. | 0.6074 |
| 332. | 1.382 | 1171. | 0.6063 |
| 333. | 1.38 | 1172. | 0.6068 |
| 334. | 1.379 | 1173. | 0.6037 |
| 335. | 1.378 | 1174. | 0.6034 |
| 336. | 1.377 | 1175. | 0.6037 |
| 337. | 1.375 | 1176. | 0.6037 |
| 338. | 1.373 | 1177. | 0.6022 |
| 339. | 1.373 | 1178. | 0.6016 |
| 340. | 1.371 | 1179. | 0.6016 |
| 341. | 1.369 | 1180. | 0.6019 |
| 342. | 1.368 | 1181. | 0.6008 |
| 343. | 1.365 | 1182. | 0.6001 |
| 344. | 1.365 | 1183. | 0.6005 |
| 345. | 1.363 | 1184. | 0.5999 |
| 346. | 1.363 | 1185. | 0.5971 |
| 347. | 1.36 | 1186. | 0.5968 |
| 348. | 1.36 | 1187. | 0.5979 |
| 349. | 1.359 | 1188. | 0.5958 |
| 350. | 1.356 | 1189. | 0.5945 |
| 351. | 1.355 | 1190. | 0.5951 |
| 352. | 1.355 | 1191. | 0.5938 |
| 353. | 1.353 | 1192. | 0.594 |
| 354. | 1.351 | 1193. | 0.5917 |
| 355. | 1.35 | 1194. | 0.5947 |
| 356. | 1.349 | 1195. | 0.5938 |
| 357. | 1.345 | 1196. | 0.5915 |
| 358. | 1.345 | 1197. | 0.5907 |
| 359. | 1.344 | 1198. | 0.5907 |
| 360. | 1.342 | 1199. | 0.5884 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 361. | 1.341 | 1200. | 0.5902 |
| 362. | 1.341 | 1201. | 0.5884 |
| 363. | 1.337 | 1202. | 0.5883 |
| 364. | 1.337 | 1203. | 0.5885 |
| 365. | 1.335 | 1204. | 0.5875 |
| 366. | 1.334 | 1205. | 0.5865 |
| 367. | 1.333 | 1206. | 0.5862 |
| 368. | 1.331 | 1207. | 0.5855 |
| 369. | 1.33 | 1208. | 0.5846 |
| 370. | 1.33 | 1209. | 0.584 |
| 371. | 1.327 | 1210. | 0.5832 |
| 372. | 1.326 | 1211. | 0.583 |
| 373. | 1.323 | 1212. | 0.5816 |
| 374. | 1.323 | 1213. | 0.5808 |
| 375. | 1.323 | 1214. | 0.5816 |
| 376. | 1.32 | 1215. | 0.5814 |
| 377. | 1.319 | 1216. | 0.5807 |
| 378. | 1.319 | 1217. | 0.5787 |
| 379. | 1.316 | 1218. | 0.5793 |
| 380. | 1.315 | 1219. | 0.5783 |
| 381. | 1.314 | 1220. | 0.5796 |
| 382. | 1.313 | 1221. | 0.5772 |
| 383. | 1.31 | 1222. | 0.5766 |
| 384. | 1.31 | 1223. | 0.576 |
| 385. | 1.309 | 1224. | 0.5749 |
| 386. | 1.308 | 1225. | 0.5756 |
| 387. | 1.305 | 1226. | 0.5746 |
| 388. | 1.304 | 1227. | 0.5744 |
| 389. | 1.305 | 1228. | 0.5738 |
| 390. | 1.302 | 1229. | 0.5733 |
| 391. | 1.301 | 1230. | 0.5728 |
| 392. | 1.299 | 1231. | 0.572 |
| 393. | 1.3 | 1232. | 0.5704 |
| 394. | 1.298 | 1233. | 0.5702 |
| 395. | 1.297 | 1234. | 0.5705 |
| 396. | 1.295 | 1235. | 0.5693 |
| 397. | 1.293 | 1236. | 0.5682 |
| 398. | 1.29 | 1237. | 0.5673 |
| 399. | 1.289 | 1238. | 0.5686 |
| 400. | 1.288 | 1239. | 0.5674 |
| 401. | 1.288 | 1240. | 0.5681 |
| 402. | 1.285 | 1241. | 0.567 |
| 403. | 1.285 | 1242. | 0.5653 |
| 404. | 1.283 | 1243. | 0.566 |
| 405. | 1.282 | 1244. | 0.565 |
| 406. | 1.281 | 1245. | 0.5636 |
| 407. | 1.279 | 1246. | 0.563 |
| 408. | 1.278 | 1247. | 0.5619 |
| 409. | 1.276 | 1248. | 0.562 |
| 410. | 1.276 | 1249. | 0.562 |
| 411. | 1.274 | 1250. | 0.5623 |
| 412. | 1.272 | 1251. | 0.5606 |
| 413. | 1.27 | 1252. | 0.5612 |
| 414. | 1.271 | 1253. | 0.5597 |
| 415. | 1.269 | 1254. | 0.5595 |
| 416. | 1.27 | 1255. | 0.5592 |
| 417. | 1.267 | 1256. | 0.559 |
| 418. | 1.265 | 1257. | 0.5576 |
| 419. | 1.265 | 1258. | 0.5561 |
| 420. | 1.264 | 1259. | 0.5575 |
| 421. | 1.26 | 1260. | 0.5559 |
| 422. | 1.261 | 1261. | 0.5565 |
| 423. | 1.26 | 1262. | 0.555 |
| 424. | 1.258 | 1263. | 0.5541 |
| 425. | 1.256 | 1264. | 0.5538 |
| 426. | 1.257 | 1265. | 0.5544 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 427. | 1.256 | 1266. | 0.5538 |
| 428. | 1.254 | 1267. | 0.5525 |
| 429. | 1.251 | 1268. | 0.5496 |
| 430. | 1.251 | 1269. | 0.551 |
| 431. | 1.25 | 1270. | 0.5505 |
| 432. | 1.247 | 1271. | 0.5506 |
| 433. | 1.248 | 1272. | 0.5495 |
| 434. | 1.245 | 1273. | 0.5485 |
| 435. | 1.245 | 1274. | 0.5484 |
| 436. | 1.244 | 1275. | 0.5471 |
| 437. | 1.243 | 1276. | 0.5486 |
| 438. | 1.24 | 1277. | 0.5455 |
| 439. | 1.239 | 1278. | 0.5454 |
| 440. | 1.239 | 1279. | 0.5443 |
| 441. | 1.237 | 1280. | 0.544 |
| 442. | 1.237 | 1281. | 0.5461 |
| 443. | 1.236 | 1282. | 0.5443 |
| 444. | 1.235 | 1283. | 0.544 |
| 445. | 1.232 | 1284. | 0.5433 |
| 446. | 1.232 | 1285. | 0.5411 |
| 447. | 1.231 | 1286. | 0.5409 |
| 448. | 1.229 | 1287. | 0.541 |
| 449. | 1.228 | 1288. | 0.5401 |
| 450. | 1.225 | 1289. | 0.5416 |
| 451. | 1.226 | 1290. | 0.5402 |
| 452. | 1.224 | 1291. | 0.5397 |
| 453. | 1.224 | 1292. | 0.5392 |
| 454. | 1.221 | 1293. | 0.5403 |
| 455. | 1.22 | 1294. | 0.5386 |
| 456. | 1.219 | 1295. | 0.536 |
| 457. | 1.218 | 1296. | 0.5365 |
| 458. | 1.217 | 1297. | 0.5368 |
| 459. | 1.215 | 1298. | 0.5345 |
| 460. | 1.214 | 1299. | 0.5348 |
| 461. | 1.213 | 1300. | 0.5362 |
| 462. | 1.211 | 1301. | 0.5334 |
| 463. | 1.21 | 1302. | 0.5329 |
| 464. | 1.207 | 1303. | 0.5321 |
| 465. | 1.208 | 1304. | 0.5299 |
| 466. | 1.207 | 1305. | 0.5318 |
| 467. | 1.204 | 1306. | 0.5309 |
| 468. | 1.203 | 1307. | 0.5298 |
| 469. | 1.202 | 1308. | 0.5296 |
| 470. | 1.202 | 1309. | 0.5303 |
| 471. | 1.2 | 1310. | 0.5278 |
| 472. | 1.198 | 1311. | 0.5284 |
| 473. | 1.197 | 1312. | 0.5284 |
| 474. | 1.196 | 1313. | 0.5277 |
| 475. | 1.194 | 1314. | 0.5267 |
| 476. | 1.194 | 1315. | 0.5276 |
| 477. | 1.195 | 1316. | 0.525 |
| 478. | 1.191 | 1317. | 0.5273 |
| 479. | 1.191 | 1318. | 0.5258 |
| 480. | 1.19 | 1319. | 0.524 |
| 481. | 1.188 | 1320. | 0.5226 |
| 482. | 1.188 | 1321. | 0.5246 |
| 483. | 1.186 | 1322. | 0.5221 |
| 484. | 1.185 | 1323. | 0.5219 |
| 485. | 1.183 | 1324. | 0.5242 |
| 486. | 1.181 | 1325. | 0.5212 |
| 487. | 1.181 | 1326. | 0.5209 |
| 488. | 1.182 | 1327. | 0.5214 |
| 489. | 1.177 | 1328. | 0.5199 |
| 490. | 1.176 | 1329. | 0.5191 |
| 491. | 1.176 | 1330. | 0.5178 |
| 492. | 1.174 | 1331. | 0.5196 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 493. | 1.175 | 1332. | 0.5181 |
| 494. | 1.172 | 1333. | 0.5174 |
| 495. | 1.171 | 1334. | 0.5177 |
| 496. | 1.171 | 1335. | 0.5162 |
| 497. | 1.169 | 1336. | 0.5159 |
| 498. | 1.167 | 1337. | 0.5145 |
| 499. | 1.167 | 1338. | 0.5145 |
| 500. | 1.165 | 1339. | 0.5139 |
| 501. | 1.166 | 1340. | 0.5147 |
| 502. | 1.162 | 1341. | 0.5133 |
| 503. | 1.163 | 1342. | 0.5138 |
| 504. | 1.16 | 1343. | 0.5114 |
| 505. | 1.16 | 1344. | 0.5126 |
| 506. | 1.159 | 1345. | 0.5114 |
| 507. | 1.157 | 1346. | 0.5106 |
| 508. | 1.156 | 1347. | 0.5121 |
| 509. | 1.155 | 1348. | 0.509 |
| 510. | 1.155 | 1349. | 0.5099 |
| 511. | 1.152 | 1350. | 0.5094 |
| 512. | 1.152 | 1351. | 0.5092 |
| 513. | 1.15 | 1352. | 0.5049 |
| 514. | 1.15 | 1353. | 0.508 |
| 515. | 1.146 | 1354. | 0.5073 |
| 516. | 1.147 | 1355. | 0.5049 |
| 517. | 1.145 | 1356. | 0.5046 |
| 518. | 1.145 | 1357. | 0.5056 |
| 519. | 1.143 | 1358. | 0.5043 |
| 520. | 1.143 | 1359. | 0.5042 |
| 521. | 1.14 | 1360. | 0.5041 |
| 522. | 1.141 | 1361. | 0.503 |
| 523. | 1.139 | 1362. | 0.5027 |
| 524. | 1.136 | 1363. | 0.503 |
| 525. | 1.139 | 1364. | 0.5024 |
| 526. | 1.138 | 1365. | 0.5014 |
| 527. | 1.134 | 1366. | 0.5003 |
| 528. | 1.133 | 1367. | 0.5009 |
| 529. | 1.134 | 1368. | 0.4999 |
| 530. | 1.132 | 1369. | 0.5 |
| 531. | 1.13 | 1370. | 0.4983 |
| 532. | 1.13 | 1371. | 0.4991 |
| 533. | 1.127 | 1372. | 0.4964 |
| 534. | 1.127 | 1373. | 0.4979 |
| 535. | 1.126 | 1374. | 0.496 |
| 536. | 1.124 | 1375. | 0.4964 |
| 537. | 1.124 | 1376. | 0.4969 |
| 538. | 1.123 | 1377. | 0.4951 |
| 539. | 1.12 | 1378. | 0.4965 |
| 540. | 1.12 | 1379. | 0.4942 |
| 541. | 1.119 | 1380. | 0.4923 |
| 542. | 1.118 | 1381. | 0.4935 |
| 543. | 1.116 | 1382. | 0.4939 |
| 544. | 1.116 | 1383. | 0.4922 |
| 545. | 1.116 | 1384. | 0.492 |
| 546. | 1.115 | 1385. | 0.4911 |
| 547. | 1.11 | 1386. | 0.4912 |
| 548. | 1.112 | 1387. | 0.4889 |
| 549. | 1.11 | 1388. | 0.4895 |
| 550. | 1.111 | 1389. | 0.4894 |
| 551. | 1.108 | 1390. | 0.4896 |
| 552. | 1.108 | 1391. | 0.4892 |
| 553. | 1.105 | 1392. | 0.4878 |
| 554. | 1.105 | 1393. | 0.4869 |
| 555. | 1.104 | 1394. | 0.486 |
| 556. | 1.102 | 1395. | 0.4846 |
| 557. | 1.102 | 1396. | 0.4858 |
| 558. | 1.1 | 1397. | 0.4866 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 559. | 1.1 | 1398. | 0.4852 |
| 560. | 1.098 | 1399. | 0.4848 |
| 561. | 1.097 | 1400. | 0.484 |
| 562. | 1.097 | 1401. | 0.4835 |
| 563. | 1.095 | 1402. | 0.4831 |
| 564. | 1.093 | 1403. | 0.485 |
| 565. | 1.093 | 1404. | 0.4821 |
| 566. | 1.091 | 1405. | 0.4823 |
| 567. | 1.093 | 1406. | 0.4799 |
| 568. | 1.089 | 1407. | 0.4794 |
| 569. | 1.087 | 1408. | 0.4805 |
| 570. | 1.086 | 1409. | 0.4807 |
| 571. | 1.087 | 1410. | 0.4798 |
| 572. | 1.086 | 1411. | 0.4795 |
| 573. | 1.082 | 1412. | 0.4778 |
| 574. | 1.082 | 1413. | 0.4774 |
| 575. | 1.083 | 1414. | 0.4768 |
| 576. | 1.081 | 1415. | 0.4781 |
| 577. | 1.081 | 1416. | 0.4764 |
| 578. | 1.079 | 1417. | 0.4755 |
| 579. | 1.077 | 1418. | 0.4748 |
| 580. | 1.075 | 1419. | 0.4753 |
| 581. | 1.075 | 1420. | 0.4751 |
| 582. | 1.072 | 1421. | 0.4741 |
| 583. | 1.073 | 1422. | 0.4738 |
| 584. | 1.072 | 1423. | 0.473 |
| 585. | 1.072 | 1424. | 0.4726 |
| 586. | 1.07 | 1425. | 0.4723 |
| 587. | 1.07 | 1426. | 0.4722 |
| 588. | 1.068 | 1427. | 0.471 |
| 589. | 1.068 | 1428. | 0.4702 |
| 590. | 1.066 | 1429. | 0.4697 |
| 591. | 1.065 | 1430. | 0.4696 |
| 592. | 1.064 | 1431. | 0.4688 |
| 593. | 1.064 | 1432. | 0.4692 |
| 594. | 1.062 | 1433. | 0.4671 |
| 595. | 1.061 | 1434. | 0.4675 |
| 596. | 1.06 | 1435. | 0.4679 |
| 597. | 1.06 | 1436. | 0.4658 |
| 598. | 1.059 | 1437. | 0.4673 |
| 599. | 1.057 | 1438. | 0.4651 |
| 600. | 1.055 | 1439. | 0.4658 |
| 601. | 1.055 | 1440. | 0.4645 |
| 602. | 1.056 | 1441. | 0.463 |
| 603. | 1.05 | 1442. | 0.4637 |
| 604. | 1.052 | 1443. | 0.4646 |
| 605. | 1.051 | 1444. | 0.4625 |
| 606. | 1.051 | 1445. | 0.4624 |
| 607. | 1.048 | 1446. | 0.4619 |
| 608. | 1.047 | 1447. | 0.463 |
| 609. | 1.045 | 1448. | 0.4608 |
| 610. | 1.046 | 1449. | 0.4601 |
| 611. | 1.043 | 1450. | 0.4594 |
| 612. | 1.042 | 1451. | 0.46 |
| 613. | 1.043 | 1452. | 0.459 |
| 614. | 1.041 | 1453. | 0.4581 |
| 615. | 1.04 | 1454. | 0.4588 |
| 616. | 1.039 | 1455. | 0.4579 |
| 617. | 1.037 | 1456. | 0.4572 |
| 618. | 1.037 | 1457. | 0.4572 |
| 619. | 1.034 | 1458. | 0.4567 |
| 620. | 1.033 | 1459. | 0.4559 |
| 621. | 1.034 | 1460. | 0.4562 |
| 622. | 1.033 | 1461. | 0.4548 |
| 623. | 1.031 | 1462. | 0.4535 |
| 624. | 1.031 | 1463. | 0.4535 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 625. | 1.028 | 1464. | 0.4539 |
| 626. | 1.028 | 1465. | 0.4539 |
| 627. | 1.028 | 1466. | 0.4532 |
| 628. | 1.026 | 1467. | 0.4512 |
| 629. | 1.025 | 1468. | 0.4528 |
| 630. | 1.024 | 1469. | 0.4502 |
| 631. | 1.022 | 1470. | 0.4513 |
| 632. | 1.022 | 1471. | 0.4508 |
| 633. | 1.022 | 1472. | 0.4501 |
| 634. | 1.02 | 1473. | 0.4499 |
| 635. | 1.021 | 1474. | 0.4486 |
| 636. | 1.019 | 1475. | 0.4481 |
| 637. | 1.018 | 1476. | 0.4498 |
| 638. | 1.017 | 1477. | 0.4479 |
| 639. | 1.016 | 1478. | 0.4479 |
| 640. | 1.014 | 1479. | 0.4474 |
| 641. | 1.014 | 1480. | 0.4476 |
| 642. | 1.012 | 1481. | 0.4474 |
| 643. | 1.011 | 1482. | 0.4466 |
| 644. | 1.009 | 1483. | 0.4457 |
| 645. | 1.01 | 1484. | 0.4443 |
| 646. | 1.007 | 1485. | 0.4438 |
| 647. | 1.005 | 1486. | 0.4445 |
| 648. | 1.007 | 1487. | 0.444 |
| 649. | 1.004 | 1488. | 0.4422 |
| 650. | 1.004 | 1489. | 0.4413 |
| 651. | 1.005 | 1490. | 0.4413 |
| 652. | 1.004 | 1491. | 0.4405 |
| 653. | 1.002 | 1492. | 0.4411 |
| 654. | 1. | 1493. | 0.4392 |
| 655. | 1.001 | 1494. | 0.4386 |
| 656. | 0.9979 | 1495. | 0.44 |
| 657. | 0.9979 | 1496. | 0.4391 |
| 658. | 0.9956 | 1497. | 0.4397 |
| 659. | 0.9952 | 1498. | 0.4387 |
| 660. | 0.9949 | 1499. | 0.4375 |
| 661. | 0.9944 | 1500. | 0.4371 |
| 662. | 0.992 | 1501. | 0.4374 |
| 663. | 0.9924 | 1502. | 0.4362 |
| 664. | 0.9919 | 1503. | 0.436 |
| 665. | 0.9904 | 1504. | 0.436 |
| 666. | 0.9897 | 1505. | 0.4355 |
| 667. | 0.989 | 1506. | 0.4358 |
| 668. | 0.9884 | 1507. | 0.4354 |
| 669. | 0.9875 | 1508. | 0.4336 |
| 670. | 0.9849 | 1509. | 0.433 |
| 671. | 0.984 | 1510. | 0.4326 |
| 672. | 0.9835 | 1511. | 0.4331 |
| 673. | 0.9821 | 1512. | 0.433 |
| 674. | 0.9812 | 1513. | 0.4328 |
| 675. | 0.9804 | 1514. | 0.4324 |
| 676. | 0.9783 | 1515. | 0.4302 |
| 677. | 0.9766 | 1516. | 0.4297 |
| 678. | 0.977 | 1517. | 0.4282 |
| 679. | 0.9757 | 1518. | 0.4309 |
| 680. | 0.9756 | 1519. | 0.4271 |
| 681. | 0.9737 | 1520. | 0.4283 |
| 682. | 0.9737 | 1521. | 0.4285 |
| 683. | 0.9709 | 1522. | 0.4255 |
| 684. | 0.9721 | 1523. | 0.4279 |
| 685. | 0.9705 | 1524. | 0.427 |
| 686. | 0.9702 | 1525. | 0.4257 |
| 687. | 0.9684 | 1526. | 0.4257 |
| 688. | 0.9685 | 1527. | 0.4255 |
| 689. | 0.9655 | 1528. | 0.4254 |
| 690. | 0.9666 | 1529. | 0.4245 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 691. | 0.9645 | 1530. | 0.4238 |
| 692. | 0.964 | 1531. | 0.4245 |
| 693. | 0.9623 | 1532. | 0.4243 |
| 694. | 0.96 | 1533. | 0.4221 |
| 695. | 0.9627 | 1534. | 0.4228 |
| 696. | 0.9588 | 1535. | 0.4215 |
| 697. | 0.9609 | 1536. | 0.4227 |
| 698. | 0.9577 | 1537. | 0.4212 |
| 699. | 0.9566 | 1538. | 0.4212 |
| 700. | 0.9571 | 1539. | 0.4224 |
| 701. | 0.9554 | 1540. | 0.4209 |
| 702. | 0.9538 | 1541. | 0.4176 |
| 703. | 0.9544 | 1542. | 0.4198 |
| 704. | 0.952 | 1543. | 0.4175 |
| 705. | 0.9528 | 1544. | 0.4172 |
| 706. | 0.95 | 1545. | 0.4181 |
| 707. | 0.9504 | 1546. | 0.4153 |
| 708. | 0.9489 | 1547. | 0.4167 |
| 709. | 0.9491 | 1548. | 0.4174 |
| 710. | 0.9449 | 1549. | 0.4148 |
| 711. | 0.9464 | 1550. | 0.416 |
| 712. | 0.9441 | 1551. | 0.4145 |
| 713. | 0.9445 | 1552. | 0.4138 |
| 714. | 0.9431 | 1553. | 0.4132 |
| 715. | 0.9429 | 1554. | 0.4137 |
| 716. | 0.9408 | 1555. | 0.4131 |
| 717. | 0.939 | 1556. | 0.4123 |
| 718. | 0.9399 | 1557. | 0.4117 |
| 719. | 0.9381 | 1558. | 0.4137 |
| 720. | 0.9368 | 1559. | 0.4122 |
| 721. | 0.9377 | 1560. | 0.4106 |
| 722. | 0.9343 | 1561. | 0.4123 |
| 723. | 0.9354 | 1562. | 0.4091 |
| 724. | 0.9325 | 1563. | 0.4096 |
| 725. | 0.9335 | 1564. | 0.4081 |
| 726. | 0.9308 | 1565. | 0.4088 |
| 727. | 0.9293 | 1566. | 0.4086 |
| 728. | 0.9305 | 1567. | 0.4064 |
| 729. | 0.9305 | 1568. | 0.4078 |
| 730. | 0.9288 | 1569. | 0.4072 |
| 731. | 0.9271 | 1570. | 0.4076 |
| 732. | 0.9279 | 1571. | 0.4066 |
| 733. | 0.9257 | 1572. | 0.4068 |
| 734. | 0.9248 | 1573. | 0.4059 |
| 735. | 0.9254 | 1574. | 0.406 |
| 736. | 0.9234 | 1575. | 0.4054 |
| 737. | 0.9224 | 1576. | 0.4045 |
| 738. | 0.921 | 1577. | 0.4042 |
| 739. | 0.9198 | 1578. | 0.405 |
| 740. | 0.9185 | 1579. | 0.4028 |
| 741. | 0.9187 | 1580. | 0.4029 |
| 742. | 0.9169 | 1581. | 0.4005 |
| 743. | 0.9188 | 1582. | 0.4012 |
| 744. | 0.9175 | 1583. | 0.4009 |
| 745. | 0.9159 | 1584. | 0.4025 |
| 746. | 0.9153 | 1585. | 0.4003 |
| 747. | 0.9151 | 1586. | 0.4 |
| 748. | 0.9115 | 1587. | 0.3995 |
| 749. | 0.911 | 1588. | 0.3978 |
| 750. | 0.9099 | 1589. | 0.3983 |
| 751. | 0.9094 | 1590. | 0.398 |
| 752. | 0.9082 | 1591. | 0.3986 |
| 753. | 0.9084 | 1592. | 0.3974 |
| 754. | 0.907 | 1593. | 0.3973 |
| 755. | 0.9062 | 1594. | 0.3974 |
| 756. | 0.9048 | 1595. | 0.3945 |

| Time (sec) | Displacement (ft) | Time (sec) | Displacement (ft) |
|------------|-------------------|------------|-------------------|
| 757. | 0.9037 | 1596. | 0.3957 |
| 758. | 0.904 | 1597. | 0.3946 |
| 759. | 0.9023 | 1598. | 0.3954 |
| 760. | 0.9038 | 1599. | 0.3947 |
| 761. | 0.9009 | 1600. | 0.3936 |
| 762. | 0.9012 | 1601. | 0.3931 |
| 763. | 0.899 | 1602. | 0.3931 |
| 764. | 0.8964 | 1603. | 0.3924 |
| 765. | 0.8977 | 1604. | 0.3927 |
| 766. | 0.896 | 1605. | 0.3927 |
| 767. | 0.895 | 1606. | 0.3927 |
| 768. | 0.8939 | 1607. | 0.3923 |
| 769. | 0.893 | 1608. | 0.3918 |
| 770. | 0.8931 | 1609. | 0.3907 |
| 771. | 0.8923 | 1610. | 0.3881 |
| 772. | 0.8912 | 1611. | 0.389 |
| 773. | 0.8914 | 1612. | 0.3881 |
| 774. | 0.8887 | 1613. | 0.39 |
| 775. | 0.89 | 1614. | 0.3875 |
| 776. | 0.8893 | 1615. | 0.3878 |
| 777. | 0.8877 | 1616. | 0.3865 |
| 778. | 0.8866 | 1617. | 0.3865 |
| 779. | 0.8858 | 1618. | 0.3848 |
| 780. | 0.8848 | 1619. | 0.3862 |
| 781. | 0.8836 | 1620. | 0.3847 |
| 782. | 0.8825 | 1621. | 0.3857 |
| 783. | 0.8811 | 1622. | 0.3848 |
| 784. | 0.8816 | 1623. | 0.385 |
| 785. | 0.8813 | 1624. | 0.3833 |
| 786. | 0.8803 | 1625. | 0.3841 |
| 787. | 0.8794 | 1626. | 0.3826 |
| 788. | 0.879 | 1627. | 0.3827 |
| 789. | 0.8758 | 1628. | 0.3826 |
| 790. | 0.8745 | 1629. | 0.3819 |
| 791. | 0.8732 | 1630. | 0.3811 |
| 792. | 0.8739 | 1631. | 0.3806 |
| 793. | 0.8744 | 1632. | 0.3805 |
| 794. | 0.8712 | 1633. | 0.3814 |
| 795. | 0.8714 | 1634. | 0.3804 |
| 796. | 0.8711 | 1635. | 0.3796 |
| 797. | 0.8711 | 1636. | 0.3792 |
| 798. | 0.8701 | 1637. | 0.3796 |
| 799. | 0.8689 | 1638. | 0.3791 |
| 800. | 0.8667 | 1639. | 0.3781 |
| 801. | 0.8659 | 1640. | 0.3776 |
| 802. | 0.8669 | 1641. | 0.3765 |
| 803. | 0.8648 | 1642. | 0.3761 |
| 804. | 0.8632 | 1643. | 0.3763 |
| 805. | 0.8635 | 1644. | 0.3765 |
| 806. | 0.8627 | 1645. | 0.3743 |
| 807. | 0.8629 | 1646. | 0.3737 |
| 808. | 0.8624 | 1647. | 0.3762 |
| 809. | 0.8598 | 1648. | 0.3736 |
| 810. | 0.8597 | 1649. | 0.3722 |
| 811. | 0.859 | 1650. | 0.3727 |
| 812. | 0.8584 | 1651. | 0.3733 |
| 813. | 0.8551 | 1652. | 0.3737 |
| 814. | 0.855 | 1653. | 0.3735 |
| 815. | 0.8559 | 1654. | 0.3714 |
| 816. | 0.8543 | 1655. | 0.3701 |
| 817. | 0.8541 | 1656. | 0.3704 |
| 818. | 0.8534 | 1657. | 0.3703 |
| 819. | 0.8523 | 1658. | 0.369 |
| 820. | 0.8516 | 1659. | 0.3702 |
| 821. | 0.8503 | 1660. | 0.3694 |
| 822. | 0.8479 | 1661. | 0.3691 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 823. | 0.85 | 1662. | 0.369 |
| 824. | 0.8486 | 1663. | 0.3688 |
| 825. | 0.8461 | 1664. | 0.3672 |
| 826. | 0.8457 | 1665. | 0.3669 |
| 827. | 0.8465 | 1666. | 0.3669 |
| 828. | 0.8434 | 1667. | 0.3675 |
| 829. | 0.8429 | 1668. | 0.3661 |
| 830. | 0.8418 | 1669. | 0.3654 |
| 831. | 0.8415 | 1670. | 0.3661 |
| 832. | 0.841 | 1671. | 0.3654 |
| 833. | 0.8399 | 1672. | 0.3651 |
| 834. | 0.8386 | 1673. | 0.3642 |
| 835. | 0.8392 | 1674. | 0.3634 |
| 836. | 0.8371 | 1675. | 0.3629 |
| 837. | 0.8358 | 1676. | 0.3653 |
| 838. | 0.8345 | 1677. | 0.3627 |
| 839. | 0.8337 | 1678. | 0.3618 |
| 840. | 0.8343 | 1679. | 0.3592 |

SOLUTION

Slug Test
 Aquifer Model: Unconfined
 Solution Method: Bouwer-Rice
 ln(Re/rw): 2.56

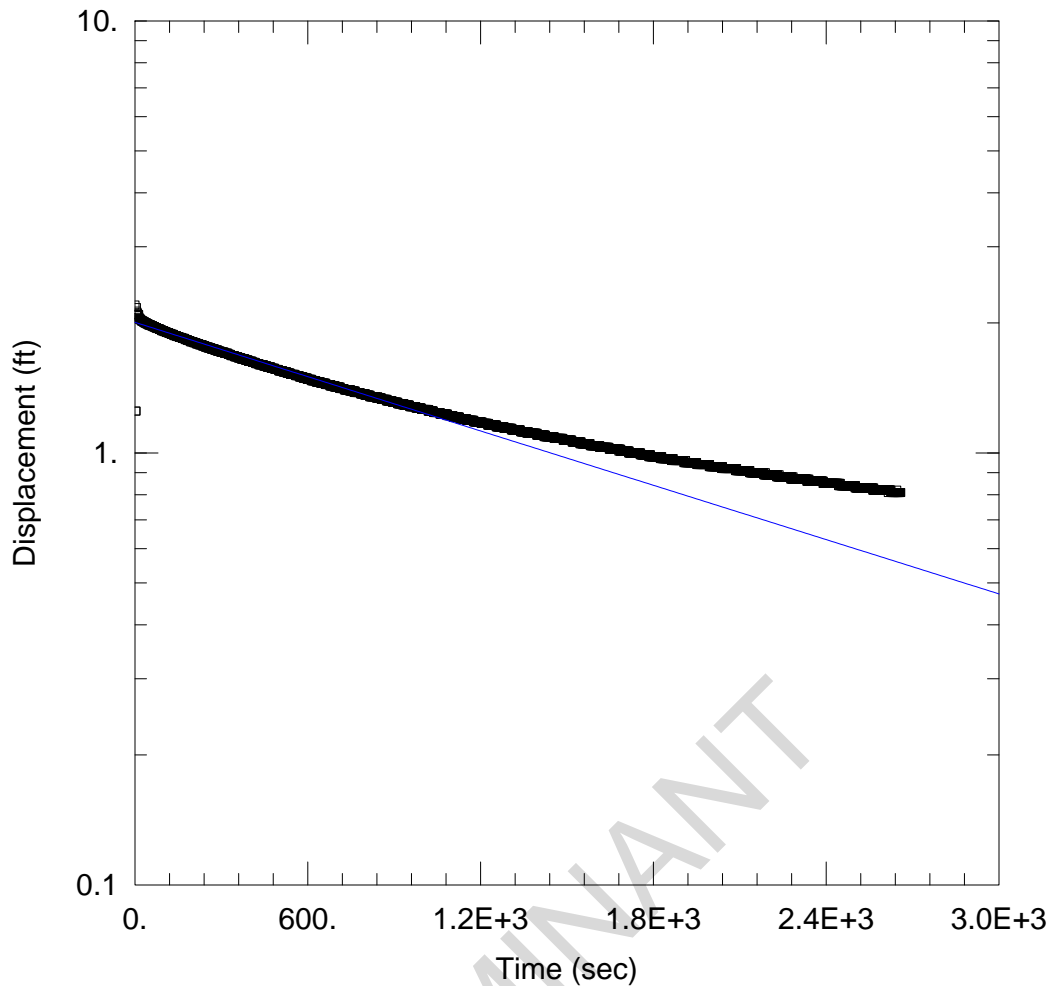
VISUAL ESTIMATION RESULTS

Estimated Parameters

| <u>Parameter</u> | <u>Estimate</u> | |
|------------------|-----------------|--------|
| K | 3.407E-5 | cm/sec |
| y0 | 1.958 | ft |

$T = K \cdot b = 0.008307 \text{ cm}^2/\text{sec}$

LUMINANT



PDP-26 SLUG OUT

Data Set: J:\...\PDP-26 Slug Out.aqt
 Date: 12/16/15

Time: 10:25:50

PROJECT INFORMATION

Company: PBW
 Client: Luminant
 Project: 5164
 Location: MLSES
 Test Well: PDP-26
 Test Date: 10/6/15

AQUIFER DATA

Saturated Thickness: 8. ft

Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (PDP-26)

Initial Displacement: 2.2 ft
 Total Well Penetration Depth: 8. ft
 Casing Radius: 0.083 ft

Static Water Column Height: 20.02 ft
 Screen Length: 8. ft
 Well Radius: 0.27 ft

SOLUTION

Aquifer Model: Unconfined
 K = 1.621E-5 cm/sec

Solution Method: Bouwer-Rice
 y0 = 2.006 ft

Data Set: J:\5164 - Luminant CCR Well Installation and GW Sampling\5164-B_Martin Lake\Slug Tests\PDP5\Aqtes
 Title: PDP-26 Slug Out
 Date: 12/16/15
 Time: 10:26:04

PROJECT INFORMATION

Company: PBW
 Client: Luminant
 Project: 5164
 Location: MLSES
 Test Date: 10/6/15
 Test Well: PDP-26

AQUIFER DATA

Saturated Thickness: 8. ft
 Anisotropy Ratio (Kz/Kr): 1.

SLUG TEST WELL DATA

Test Well: PDP-26

X Location: 0. ft
 Y Location: 0. ft

Initial Displacement: 2.2 ft
 Static Water Column Height: 20.02 ft
 Casing Radius: 0.083 ft
 Well Radius: 0.27 ft
 Well Skin Radius: 0.27 ft
 Screen Length: 8. ft
 Total Well Penetration Depth: 8. ft

No. of Observations: 2657

| Observation Data | | | |
|------------------|-------------------|------------|-------------------|
| Time (sec) | Displacement (ft) | Time (sec) | Displacement (ft) |
| 3. | 1.25 | 1332. | 1.13 |
| 4. | 1.25 | 1333. | 1.13 |
| 5. | 2.17 | 1334. | 1.13 |
| 6. | 2.13 | 1335. | 1.13 |
| 7. | 2.09 | 1336. | 1.13 |
| 8. | 2.1 | 1337. | 1.13 |
| 9. | 2.11 | 1338. | 1.13 |
| 10. | 2.09 | 1339. | 1.12 |
| 11. | 2.09 | 1340. | 1.12 |
| 12. | 2.08 | 1341. | 1.12 |
| 13. | 2.09 | 1342. | 1.12 |
| 14. | 2.06 | 1343. | 1.12 |
| 15. | 2.05 | 1344. | 1.12 |
| 16. | 2.04 | 1345. | 1.12 |
| 17. | 2.04 | 1346. | 1.12 |
| 18. | 2.04 | 1347. | 1.12 |
| 19. | 2.04 | 1348. | 1.12 |
| 20. | 2.03 | 1349. | 1.12 |
| 21. | 2.03 | 1350. | 1.12 |
| 22. | 2.03 | 1351. | 1.12 |
| 23. | 2.02 | 1352. | 1.12 |
| 24. | 2.02 | 1353. | 1.12 |
| 25. | 2.02 | 1354. | 1.12 |
| 26. | 2.02 | 1355. | 1.12 |
| 27. | 2.02 | 1356. | 1.12 |
| 28. | 2.02 | 1357. | 1.12 |
| 29. | 2.01 | 1358. | 1.12 |
| 30. | 2.01 | 1359. | 1.12 |
| 31. | 2.01 | 1360. | 1.12 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 32. | 2.01 | 1361. | 1.11 |
| 33. | 2.01 | 1362. | 1.12 |
| 34. | 2. | 1363. | 1.12 |
| 35. | 2. | 1364. | 1.11 |
| 36. | 2. | 1365. | 1.12 |
| 37. | 2. | 1366. | 1.12 |
| 38. | 2. | 1367. | 1.11 |
| 39. | 2. | 1368. | 1.11 |
| 40. | 2. | 1369. | 1.11 |
| 41. | 1.99 | 1370. | 1.11 |
| 42. | 1.99 | 1371. | 1.11 |
| 43. | 1.99 | 1372. | 1.11 |
| 44. | 1.99 | 1373. | 1.11 |
| 45. | 1.99 | 1374. | 1.11 |
| 46. | 1.99 | 1375. | 1.11 |
| 47. | 1.98 | 1376. | 1.11 |
| 48. | 1.98 | 1377. | 1.11 |
| 49. | 1.98 | 1378. | 1.11 |
| 50. | 1.98 | 1379. | 1.11 |
| 51. | 1.98 | 1380. | 1.11 |
| 52. | 1.98 | 1381. | 1.11 |
| 53. | 1.98 | 1382. | 1.11 |
| 54. | 1.98 | 1383. | 1.11 |
| 55. | 1.97 | 1384. | 1.11 |
| 56. | 1.97 | 1385. | 1.11 |
| 57. | 1.97 | 1386. | 1.11 |
| 58. | 1.97 | 1387. | 1.11 |
| 59. | 1.97 | 1388. | 1.11 |
| 60. | 1.97 | 1389. | 1.11 |
| 61. | 1.97 | 1390. | 1.11 |
| 62. | 1.96 | 1391. | 1.11 |
| 63. | 1.96 | 1392. | 1.11 |
| 64. | 1.96 | 1393. | 1.11 |
| 65. | 1.96 | 1394. | 1.11 |
| 66. | 1.96 | 1395. | 1.1 |
| 67. | 1.96 | 1396. | 1.1 |
| 68. | 1.96 | 1397. | 1.11 |
| 69. | 1.95 | 1398. | 1.1 |
| 70. | 1.95 | 1399. | 1.1 |
| 71. | 1.95 | 1400. | 1.1 |
| 72. | 1.95 | 1401. | 1.1 |
| 73. | 1.95 | 1402. | 1.1 |
| 74. | 1.95 | 1403. | 1.1 |
| 75. | 1.95 | 1404. | 1.1 |
| 76. | 1.94 | 1405. | 1.1 |
| 77. | 1.94 | 1406. | 1.1 |
| 78. | 1.94 | 1407. | 1.1 |
| 79. | 1.94 | 1408. | 1.1 |
| 80. | 1.94 | 1409. | 1.1 |
| 81. | 1.94 | 1410. | 1.1 |
| 82. | 1.94 | 1411. | 1.1 |
| 83. | 1.94 | 1412. | 1.1 |
| 84. | 1.94 | 1413. | 1.1 |
| 85. | 1.93 | 1414. | 1.1 |
| 86. | 1.93 | 1415. | 1.1 |
| 87. | 1.93 | 1416. | 1.1 |
| 88. | 1.93 | 1417. | 1.1 |
| 89. | 1.93 | 1418. | 1.1 |
| 90. | 1.93 | 1419. | 1.1 |
| 91. | 1.93 | 1420. | 1.09 |
| 92. | 1.92 | 1421. | 1.1 |
| 93. | 1.92 | 1422. | 1.1 |
| 94. | 1.92 | 1423. | 1.1 |
| 95. | 1.92 | 1424. | 1.09 |
| 96. | 1.92 | 1425. | 1.1 |
| 97. | 1.92 | 1426. | 1.09 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 98. | 1.92 | 1427. | 1.09 |
| 99. | 1.92 | 1428. | 1.09 |
| 100. | 1.92 | 1429. | 1.09 |
| 101. | 1.91 | 1430. | 1.09 |
| 102. | 1.91 | 1431. | 1.09 |
| 103. | 1.91 | 1432. | 1.09 |
| 104. | 1.91 | 1433. | 1.09 |
| 105. | 1.91 | 1434. | 1.09 |
| 106. | 1.91 | 1435. | 1.09 |
| 107. | 1.91 | 1436. | 1.09 |
| 108. | 1.91 | 1437. | 1.09 |
| 109. | 1.9 | 1438. | 1.09 |
| 110. | 1.9 | 1439. | 1.09 |
| 111. | 1.9 | 1440. | 1.09 |
| 112. | 1.9 | 1441. | 1.09 |
| 113. | 1.9 | 1442. | 1.09 |
| 114. | 1.9 | 1443. | 1.09 |
| 115. | 1.9 | 1444. | 1.09 |
| 116. | 1.9 | 1445. | 1.09 |
| 117. | 1.9 | 1446. | 1.09 |
| 118. | 1.89 | 1447. | 1.09 |
| 119. | 1.89 | 1448. | 1.09 |
| 120. | 1.89 | 1449. | 1.09 |
| 121. | 1.89 | 1450. | 1.09 |
| 122. | 1.89 | 1451. | 1.09 |
| 123. | 1.89 | 1452. | 1.09 |
| 124. | 1.89 | 1453. | 1.09 |
| 125. | 1.89 | 1454. | 1.09 |
| 126. | 1.88 | 1455. | 1.08 |
| 127. | 1.88 | 1456. | 1.09 |
| 128. | 1.88 | 1457. | 1.08 |
| 129. | 1.88 | 1458. | 1.08 |
| 130. | 1.88 | 1459. | 1.08 |
| 131. | 1.88 | 1460. | 1.08 |
| 132. | 1.88 | 1461. | 1.08 |
| 133. | 1.88 | 1462. | 1.08 |
| 134. | 1.88 | 1463. | 1.08 |
| 135. | 1.87 | 1464. | 1.08 |
| 136. | 1.87 | 1465. | 1.08 |
| 137. | 1.87 | 1466. | 1.08 |
| 138. | 1.87 | 1467. | 1.08 |
| 139. | 1.87 | 1468. | 1.08 |
| 140. | 1.87 | 1469. | 1.08 |
| 141. | 1.87 | 1470. | 1.08 |
| 142. | 1.87 | 1471. | 1.08 |
| 143. | 1.87 | 1472. | 1.08 |
| 144. | 1.87 | 1473. | 1.08 |
| 145. | 1.86 | 1474. | 1.08 |
| 146. | 1.86 | 1475. | 1.08 |
| 147. | 1.86 | 1476. | 1.08 |
| 148. | 1.86 | 1477. | 1.08 |
| 149. | 1.86 | 1478. | 1.08 |
| 150. | 1.86 | 1479. | 1.08 |
| 151. | 1.86 | 1480. | 1.08 |
| 152. | 1.86 | 1481. | 1.08 |
| 153. | 1.86 | 1482. | 1.08 |
| 154. | 1.85 | 1483. | 1.08 |
| 155. | 1.85 | 1484. | 1.08 |
| 156. | 1.85 | 1485. | 1.08 |
| 157. | 1.85 | 1486. | 1.08 |
| 158. | 1.85 | 1487. | 1.07 |
| 159. | 1.85 | 1488. | 1.07 |
| 160. | 1.85 | 1489. | 1.07 |
| 161. | 1.85 | 1490. | 1.07 |
| 162. | 1.85 | 1491. | 1.07 |
| 163. | 1.85 | 1492. | 1.07 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 164. | 1.84 | 1493. | 1.07 |
| 165. | 1.84 | 1494. | 1.07 |
| 166. | 1.84 | 1495. | 1.07 |
| 167. | 1.84 | 1496. | 1.07 |
| 168. | 1.84 | 1497. | 1.07 |
| 169. | 1.84 | 1498. | 1.07 |
| 170. | 1.84 | 1499. | 1.07 |
| 171. | 1.84 | 1500. | 1.07 |
| 172. | 1.84 | 1501. | 1.07 |
| 173. | 1.84 | 1502. | 1.07 |
| 174. | 1.83 | 1503. | 1.07 |
| 175. | 1.83 | 1504. | 1.07 |
| 176. | 1.83 | 1505. | 1.07 |
| 177. | 1.83 | 1506. | 1.07 |
| 178. | 1.83 | 1507. | 1.07 |
| 179. | 1.83 | 1508. | 1.07 |
| 180. | 1.83 | 1509. | 1.07 |
| 181. | 1.83 | 1510. | 1.07 |
| 182. | 1.83 | 1511. | 1.07 |
| 183. | 1.82 | 1512. | 1.07 |
| 184. | 1.82 | 1513. | 1.07 |
| 185. | 1.82 | 1514. | 1.07 |
| 186. | 1.82 | 1515. | 1.07 |
| 187. | 1.82 | 1516. | 1.07 |
| 188. | 1.82 | 1517. | 1.07 |
| 189. | 1.82 | 1518. | 1.06 |
| 190. | 1.82 | 1519. | 1.06 |
| 191. | 1.82 | 1520. | 1.06 |
| 192. | 1.81 | 1521. | 1.06 |
| 193. | 1.81 | 1522. | 1.06 |
| 194. | 1.81 | 1523. | 1.06 |
| 195. | 1.81 | 1524. | 1.06 |
| 196. | 1.81 | 1525. | 1.06 |
| 197. | 1.81 | 1526. | 1.06 |
| 198. | 1.81 | 1527. | 1.06 |
| 199. | 1.81 | 1528. | 1.06 |
| 200. | 1.81 | 1529. | 1.06 |
| 201. | 1.81 | 1530. | 1.06 |
| 202. | 1.81 | 1531. | 1.06 |
| 203. | 1.8 | 1532. | 1.06 |
| 204. | 1.8 | 1533. | 1.06 |
| 205. | 1.8 | 1534. | 1.06 |
| 206. | 1.8 | 1535. | 1.06 |
| 207. | 1.8 | 1536. | 1.06 |
| 208. | 1.8 | 1537. | 1.06 |
| 209. | 1.8 | 1538. | 1.06 |
| 210. | 1.8 | 1539. | 1.06 |
| 211. | 1.8 | 1540. | 1.06 |
| 212. | 1.8 | 1541. | 1.06 |
| 213. | 1.79 | 1542. | 1.06 |
| 214. | 1.79 | 1543. | 1.06 |
| 215. | 1.79 | 1544. | 1.06 |
| 216. | 1.79 | 1545. | 1.05 |
| 217. | 1.79 | 1546. | 1.05 |
| 218. | 1.79 | 1547. | 1.06 |
| 219. | 1.79 | 1548. | 1.06 |
| 220. | 1.79 | 1549. | 1.06 |
| 221. | 1.79 | 1550. | 1.05 |
| 222. | 1.79 | 1551. | 1.05 |
| 223. | 1.78 | 1552. | 1.05 |
| 224. | 1.78 | 1553. | 1.05 |
| 225. | 1.78 | 1554. | 1.05 |
| 226. | 1.78 | 1555. | 1.05 |
| 227. | 1.78 | 1556. | 1.05 |
| 228. | 1.78 | 1557. | 1.05 |
| 229. | 1.78 | 1558. | 1.05 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 230. | 1.78 | 1559. | 1.05 |
| 231. | 1.78 | 1560. | 1.05 |
| 232. | 1.78 | 1561. | 1.05 |
| 233. | 1.78 | 1562. | 1.05 |
| 234. | 1.77 | 1563. | 1.05 |
| 235. | 1.77 | 1564. | 1.05 |
| 236. | 1.77 | 1565. | 1.05 |
| 237. | 1.77 | 1566. | 1.05 |
| 238. | 1.77 | 1567. | 1.05 |
| 239. | 1.77 | 1568. | 1.05 |
| 240. | 1.77 | 1569. | 1.05 |
| 241. | 1.77 | 1570. | 1.05 |
| 242. | 1.77 | 1571. | 1.05 |
| 243. | 1.77 | 1572. | 1.05 |
| 244. | 1.76 | 1573. | 1.05 |
| 245. | 1.76 | 1574. | 1.05 |
| 246. | 1.76 | 1575. | 1.05 |
| 247. | 1.76 | 1576. | 1.05 |
| 248. | 1.76 | 1577. | 1.05 |
| 249. | 1.76 | 1578. | 1.05 |
| 250. | 1.76 | 1579. | 1.05 |
| 251. | 1.76 | 1580. | 1.05 |
| 252. | 1.76 | 1581. | 1.04 |
| 253. | 1.75 | 1582. | 1.04 |
| 254. | 1.75 | 1583. | 1.04 |
| 255. | 1.76 | 1584. | 1.04 |
| 256. | 1.75 | 1585. | 1.04 |
| 257. | 1.75 | 1586. | 1.04 |
| 258. | 1.75 | 1587. | 1.04 |
| 259. | 1.75 | 1588. | 1.04 |
| 260. | 1.75 | 1589. | 1.04 |
| 261. | 1.75 | 1590. | 1.04 |
| 262. | 1.75 | 1591. | 1.04 |
| 263. | 1.75 | 1592. | 1.04 |
| 264. | 1.75 | 1593. | 1.04 |
| 265. | 1.74 | 1594. | 1.04 |
| 266. | 1.74 | 1595. | 1.04 |
| 267. | 1.74 | 1596. | 1.04 |
| 268. | 1.74 | 1597. | 1.04 |
| 269. | 1.74 | 1598. | 1.04 |
| 270. | 1.74 | 1599. | 1.04 |
| 271. | 1.74 | 1600. | 1.04 |
| 272. | 1.74 | 1601. | 1.04 |
| 273. | 1.74 | 1602. | 1.04 |
| 274. | 1.74 | 1603. | 1.04 |
| 275. | 1.74 | 1604. | 1.04 |
| 276. | 1.74 | 1605. | 1.04 |
| 277. | 1.73 | 1606. | 1.04 |
| 278. | 1.73 | 1607. | 1.04 |
| 279. | 1.73 | 1608. | 1.04 |
| 280. | 1.73 | 1609. | 1.04 |
| 281. | 1.73 | 1610. | 1.04 |
| 282. | 1.73 | 1611. | 1.04 |
| 283. | 1.73 | 1612. | 1.04 |
| 284. | 1.73 | 1613. | 1.03 |
| 285. | 1.73 | 1614. | 1.04 |
| 286. | 1.72 | 1615. | 1.03 |
| 287. | 1.73 | 1616. | 1.03 |
| 288. | 1.73 | 1617. | 1.03 |
| 289. | 1.72 | 1618. | 1.03 |
| 290. | 1.72 | 1619. | 1.03 |
| 291. | 1.72 | 1620. | 1.03 |
| 292. | 1.72 | 1621. | 1.03 |
| 293. | 1.72 | 1622. | 1.03 |
| 294. | 1.72 | 1623. | 1.03 |
| 295. | 1.72 | 1624. | 1.03 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 296. | 1.72 | 1625. | 1.03 |
| 297. | 1.72 | 1626. | 1.03 |
| 298. | 1.71 | 1627. | 1.03 |
| 299. | 1.71 | 1628. | 1.03 |
| 300. | 1.71 | 1629. | 1.03 |
| 301. | 1.71 | 1630. | 1.03 |
| 302. | 1.71 | 1631. | 1.03 |
| 303. | 1.71 | 1632. | 1.03 |
| 304. | 1.71 | 1633. | 1.03 |
| 305. | 1.71 | 1634. | 1.03 |
| 306. | 1.71 | 1635. | 1.03 |
| 307. | 1.71 | 1636. | 1.03 |
| 308. | 1.71 | 1637. | 1.03 |
| 309. | 1.71 | 1638. | 1.03 |
| 310. | 1.71 | 1639. | 1.03 |
| 311. | 1.7 | 1640. | 1.03 |
| 312. | 1.7 | 1641. | 1.03 |
| 313. | 1.7 | 1642. | 1.03 |
| 314. | 1.7 | 1643. | 1.03 |
| 315. | 1.7 | 1644. | 1.03 |
| 316. | 1.7 | 1645. | 1.03 |
| 317. | 1.7 | 1646. | 1.03 |
| 318. | 1.7 | 1647. | 1.02 |
| 319. | 1.7 | 1648. | 1.02 |
| 320. | 1.7 | 1649. | 1.02 |
| 321. | 1.7 | 1650. | 1.02 |
| 322. | 1.7 | 1651. | 1.02 |
| 323. | 1.7 | 1652. | 1.02 |
| 324. | 1.69 | 1653. | 1.02 |
| 325. | 1.69 | 1654. | 1.02 |
| 326. | 1.69 | 1655. | 1.02 |
| 327. | 1.69 | 1656. | 1.02 |
| 328. | 1.69 | 1657. | 1.02 |
| 329. | 1.69 | 1658. | 1.02 |
| 330. | 1.69 | 1659. | 1.02 |
| 331. | 1.69 | 1660. | 1.02 |
| 332. | 1.69 | 1661. | 1.02 |
| 333. | 1.68 | 1662. | 1.02 |
| 334. | 1.68 | 1663. | 1.02 |
| 335. | 1.68 | 1664. | 1.02 |
| 336. | 1.68 | 1665. | 1.02 |
| 337. | 1.68 | 1666. | 1.02 |
| 338. | 1.68 | 1667. | 1.02 |
| 339. | 1.68 | 1668. | 1.02 |
| 340. | 1.68 | 1669. | 1.02 |
| 341. | 1.68 | 1670. | 1.02 |
| 342. | 1.68 | 1671. | 1.02 |
| 343. | 1.68 | 1672. | 1.02 |
| 344. | 1.68 | 1673. | 1.02 |
| 345. | 1.68 | 1674. | 1.02 |
| 346. | 1.67 | 1675. | 1.02 |
| 347. | 1.67 | 1676. | 1.02 |
| 348. | 1.67 | 1677. | 1.02 |
| 349. | 1.67 | 1678. | 1.02 |
| 350. | 1.67 | 1679. | 1.02 |
| 351. | 1.67 | 1680. | 1.01 |
| 352. | 1.67 | 1681. | 1.02 |
| 353. | 1.67 | 1682. | 1.02 |
| 354. | 1.67 | 1683. | 1.02 |
| 355. | 1.67 | 1684. | 1.01 |
| 356. | 1.67 | 1685. | 1.01 |
| 357. | 1.67 | 1686. | 1.01 |
| 358. | 1.66 | 1687. | 1.02 |
| 359. | 1.66 | 1688. | 1.01 |
| 360. | 1.66 | 1689. | 1.01 |
| 361. | 1.66 | 1690. | 1.01 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 362. | 1.66 | 1691. | 1.01 |
| 363. | 1.66 | 1692. | 1.01 |
| 364. | 1.66 | 1693. | 1.01 |
| 365. | 1.66 | 1694. | 1.01 |
| 366. | 1.66 | 1695. | 1.01 |
| 367. | 1.66 | 1696. | 1.01 |
| 368. | 1.66 | 1697. | 1.01 |
| 369. | 1.65 | 1698. | 1.01 |
| 370. | 1.65 | 1699. | 1.01 |
| 371. | 1.65 | 1700. | 1.01 |
| 372. | 1.65 | 1701. | 1.01 |
| 373. | 1.65 | 1702. | 1.01 |
| 374. | 1.65 | 1703. | 1.01 |
| 375. | 1.65 | 1704. | 1.01 |
| 376. | 1.65 | 1705. | 1.01 |
| 377. | 1.65 | 1706. | 1.01 |
| 378. | 1.65 | 1707. | 1.01 |
| 379. | 1.65 | 1708. | 1.01 |
| 380. | 1.65 | 1709. | 1.01 |
| 381. | 1.65 | 1710. | 1.01 |
| 382. | 1.65 | 1711. | 1.01 |
| 383. | 1.64 | 1712. | 1.01 |
| 384. | 1.64 | 1713. | 1.01 |
| 385. | 1.64 | 1714. | 1. |
| 386. | 1.64 | 1715. | 1.01 |
| 387. | 1.64 | 1716. | 1.01 |
| 388. | 1.64 | 1717. | 1. |
| 389. | 1.64 | 1718. | 1. |
| 390. | 1.64 | 1719. | 1. |
| 391. | 1.64 | 1720. | 1. |
| 392. | 1.64 | 1721. | 1. |
| 393. | 1.64 | 1722. | 1. |
| 394. | 1.63 | 1723. | 1. |
| 395. | 1.63 | 1724. | 1. |
| 396. | 1.63 | 1725. | 1. |
| 397. | 1.63 | 1726. | 1. |
| 398. | 1.63 | 1727. | 1. |
| 399. | 1.63 | 1728. | 1. |
| 400. | 1.63 | 1729. | 1. |
| 401. | 1.63 | 1730. | 1. |
| 402. | 1.63 | 1731. | 1. |
| 403. | 1.63 | 1732. | 1. |
| 404. | 1.63 | 1733. | 1. |
| 405. | 1.63 | 1734. | 1. |
| 406. | 1.63 | 1735. | 1. |
| 407. | 1.63 | 1736. | 1. |
| 408. | 1.62 | 1737. | 1. |
| 409. | 1.62 | 1738. | 1. |
| 410. | 1.62 | 1739. | 1. |
| 411. | 1.62 | 1740. | 1. |
| 412. | 1.62 | 1741. | 1. |
| 413. | 1.62 | 1742. | 1. |
| 414. | 1.62 | 1743. | 1. |
| 415. | 1.62 | 1744. | 1. |
| 416. | 1.62 | 1745. | 1. |
| 417. | 1.62 | 1746. | 1. |
| 418. | 1.62 | 1747. | 1. |
| 419. | 1.61 | 1748. | 1. |
| 420. | 1.61 | 1749. | 1. |
| 421. | 1.61 | 1750. | 1. |
| 422. | 1.61 | 1751. | 1. |
| 423. | 1.61 | 1752. | 1. |
| 424. | 1.61 | 1753. | 1. |
| 425. | 1.61 | 1754. | 0.99 |
| 426. | 1.61 | 1755. | 1. |
| 427. | 1.61 | 1756. | 1. |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 428. | 1.61 | 1757. | 0.99 |
| 429. | 1.61 | 1758. | 0.99 |
| 430. | 1.6 | 1759. | 0.99 |
| 431. | 1.61 | 1760. | 0.99 |
| 432. | 1.6 | 1761. | 0.99 |
| 433. | 1.6 | 1762. | 0.99 |
| 434. | 1.6 | 1763. | 0.99 |
| 435. | 1.6 | 1764. | 0.99 |
| 436. | 1.6 | 1765. | 0.99 |
| 437. | 1.6 | 1766. | 0.99 |
| 438. | 1.6 | 1767. | 0.99 |
| 439. | 1.6 | 1768. | 0.99 |
| 440. | 1.6 | 1769. | 0.99 |
| 441. | 1.6 | 1770. | 0.99 |
| 442. | 1.6 | 1771. | 0.99 |
| 443. | 1.6 | 1772. | 0.99 |
| 444. | 1.6 | 1773. | 0.99 |
| 445. | 1.6 | 1774. | 0.99 |
| 446. | 1.6 | 1775. | 0.99 |
| 447. | 1.59 | 1776. | 0.99 |
| 448. | 1.59 | 1777. | 0.99 |
| 449. | 1.59 | 1778. | 0.99 |
| 450. | 1.59 | 1779. | 0.99 |
| 451. | 1.59 | 1780. | 0.99 |
| 452. | 1.59 | 1781. | 0.99 |
| 453. | 1.59 | 1782. | 0.99 |
| 454. | 1.59 | 1783. | 0.99 |
| 455. | 1.59 | 1784. | 0.98 |
| 456. | 1.59 | 1785. | 0.99 |
| 457. | 1.59 | 1786. | 0.98 |
| 458. | 1.59 | 1787. | 0.99 |
| 459. | 1.58 | 1788. | 0.99 |
| 460. | 1.58 | 1789. | 0.98 |
| 461. | 1.58 | 1790. | 0.99 |
| 462. | 1.58 | 1791. | 0.98 |
| 463. | 1.58 | 1792. | 0.98 |
| 464. | 1.58 | 1793. | 0.98 |
| 465. | 1.58 | 1794. | 0.98 |
| 466. | 1.58 | 1795. | 0.98 |
| 467. | 1.58 | 1796. | 0.98 |
| 468. | 1.58 | 1797. | 0.98 |
| 469. | 1.58 | 1798. | 0.98 |
| 470. | 1.58 | 1799. | 0.98 |
| 471. | 1.58 | 1800. | 0.98 |
| 472. | 1.58 | 1801. | 0.98 |
| 473. | 1.57 | 1802. | 0.98 |
| 474. | 1.57 | 1803. | 0.98 |
| 475. | 1.57 | 1804. | 0.98 |
| 476. | 1.57 | 1805. | 0.98 |
| 477. | 1.57 | 1806. | 0.98 |
| 478. | 1.57 | 1807. | 0.98 |
| 479. | 1.57 | 1808. | 0.98 |
| 480. | 1.57 | 1809. | 0.98 |
| 481. | 1.57 | 1810. | 0.98 |
| 482. | 1.57 | 1811. | 0.98 |
| 483. | 1.57 | 1812. | 0.98 |
| 484. | 1.57 | 1813. | 0.98 |
| 485. | 1.57 | 1814. | 0.98 |
| 486. | 1.56 | 1815. | 0.98 |
| 487. | 1.56 | 1816. | 0.98 |
| 488. | 1.56 | 1817. | 0.98 |
| 489. | 1.56 | 1818. | 0.98 |
| 490. | 1.56 | 1819. | 0.98 |
| 491. | 1.56 | 1820. | 0.98 |
| 492. | 1.56 | 1821. | 0.98 |
| 493. | 1.56 | 1822. | 0.98 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 494. | 1.56 | 1823. | 0.98 |
| 495. | 1.56 | 1824. | 0.97 |
| 496. | 1.56 | 1825. | 0.98 |
| 497. | 1.56 | 1826. | 0.98 |
| 498. | 1.56 | 1827. | 0.97 |
| 499. | 1.55 | 1828. | 0.98 |
| 500. | 1.55 | 1829. | 0.98 |
| 501. | 1.55 | 1830. | 0.97 |
| 502. | 1.55 | 1831. | 0.97 |
| 503. | 1.55 | 1832. | 0.97 |
| 504. | 1.55 | 1833. | 0.97 |
| 505. | 1.55 | 1834. | 0.97 |
| 506. | 1.55 | 1835. | 0.97 |
| 507. | 1.55 | 1836. | 0.97 |
| 508. | 1.55 | 1837. | 0.97 |
| 509. | 1.55 | 1838. | 0.97 |
| 510. | 1.55 | 1839. | 0.97 |
| 511. | 1.55 | 1840. | 0.97 |
| 512. | 1.55 | 1841. | 0.97 |
| 513. | 1.55 | 1842. | 0.97 |
| 514. | 1.54 | 1843. | 0.97 |
| 515. | 1.54 | 1844. | 0.97 |
| 516. | 1.54 | 1845. | 0.97 |
| 517. | 1.54 | 1846. | 0.97 |
| 518. | 1.54 | 1847. | 0.97 |
| 519. | 1.54 | 1848. | 0.97 |
| 520. | 1.54 | 1849. | 0.97 |
| 521. | 1.54 | 1850. | 0.97 |
| 522. | 1.54 | 1851. | 0.97 |
| 523. | 1.54 | 1852. | 0.97 |
| 524. | 1.54 | 1853. | 0.97 |
| 525. | 1.54 | 1854. | 0.97 |
| 526. | 1.54 | 1855. | 0.97 |
| 527. | 1.54 | 1856. | 0.97 |
| 528. | 1.53 | 1857. | 0.97 |
| 529. | 1.53 | 1858. | 0.97 |
| 530. | 1.53 | 1859. | 0.97 |
| 531. | 1.53 | 1860. | 0.97 |
| 532. | 1.53 | 1861. | 0.97 |
| 533. | 1.53 | 1862. | 0.97 |
| 534. | 1.53 | 1863. | 0.96 |
| 535. | 1.53 | 1864. | 0.97 |
| 536. | 1.53 | 1865. | 0.96 |
| 537. | 1.53 | 1866. | 0.97 |
| 538. | 1.53 | 1867. | 0.97 |
| 539. | 1.53 | 1868. | 0.96 |
| 540. | 1.52 | 1869. | 0.97 |
| 541. | 1.52 | 1870. | 0.96 |
| 542. | 1.52 | 1871. | 0.96 |
| 543. | 1.52 | 1872. | 0.96 |
| 544. | 1.52 | 1873. | 0.96 |
| 545. | 1.52 | 1874. | 0.96 |
| 546. | 1.52 | 1875. | 0.96 |
| 547. | 1.52 | 1876. | 0.96 |
| 548. | 1.52 | 1877. | 0.96 |
| 549. | 1.52 | 1878. | 0.96 |
| 550. | 1.52 | 1879. | 0.96 |
| 551. | 1.52 | 1880. | 0.96 |
| 552. | 1.52 | 1881. | 0.96 |
| 553. | 1.52 | 1882. | 0.96 |
| 554. | 1.52 | 1883. | 0.96 |
| 555. | 1.52 | 1884. | 0.96 |
| 556. | 1.52 | 1885. | 0.96 |
| 557. | 1.51 | 1886. | 0.96 |
| 558. | 1.51 | 1887. | 0.96 |
| 559. | 1.51 | 1888. | 0.96 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 560. | 1.51 | 1889. | 0.96 |
| 561. | 1.51 | 1890. | 0.96 |
| 562. | 1.51 | 1891. | 0.96 |
| 563. | 1.51 | 1892. | 0.96 |
| 564. | 1.51 | 1893. | 0.96 |
| 565. | 1.51 | 1894. | 0.96 |
| 566. | 1.51 | 1895. | 0.96 |
| 567. | 1.51 | 1896. | 0.96 |
| 568. | 1.51 | 1897. | 0.96 |
| 569. | 1.51 | 1898. | 0.96 |
| 570. | 1.51 | 1899. | 0.96 |
| 571. | 1.5 | 1900. | 0.96 |
| 572. | 1.5 | 1901. | 0.96 |
| 573. | 1.5 | 1902. | 0.96 |
| 574. | 1.5 | 1903. | 0.96 |
| 575. | 1.5 | 1904. | 0.96 |
| 576. | 1.5 | 1905. | 0.96 |
| 577. | 1.5 | 1906. | 0.95 |
| 578. | 1.5 | 1907. | 0.96 |
| 579. | 1.5 | 1908. | 0.95 |
| 580. | 1.5 | 1909. | 0.95 |
| 581. | 1.5 | 1910. | 0.95 |
| 582. | 1.5 | 1911. | 0.95 |
| 583. | 1.5 | 1912. | 0.96 |
| 584. | 1.49 | 1913. | 0.95 |
| 585. | 1.49 | 1914. | 0.95 |
| 586. | 1.49 | 1915. | 0.95 |
| 587. | 1.49 | 1916. | 0.95 |
| 588. | 1.49 | 1917. | 0.95 |
| 589. | 1.49 | 1918. | 0.95 |
| 590. | 1.49 | 1919. | 0.95 |
| 591. | 1.49 | 1920. | 0.95 |
| 592. | 1.49 | 1921. | 0.95 |
| 593. | 1.49 | 1922. | 0.95 |
| 594. | 1.49 | 1923. | 0.95 |
| 595. | 1.49 | 1924. | 0.95 |
| 596. | 1.49 | 1925. | 0.95 |
| 597. | 1.49 | 1926. | 0.95 |
| 598. | 1.48 | 1927. | 0.95 |
| 599. | 1.49 | 1928. | 0.95 |
| 600. | 1.48 | 1929. | 0.95 |
| 601. | 1.48 | 1930. | 0.95 |
| 602. | 1.48 | 1931. | 0.95 |
| 603. | 1.48 | 1932. | 0.95 |
| 604. | 1.48 | 1933. | 0.95 |
| 605. | 1.48 | 1934. | 0.95 |
| 606. | 1.48 | 1935. | 0.95 |
| 607. | 1.48 | 1936. | 0.95 |
| 608. | 1.48 | 1937. | 0.95 |
| 609. | 1.48 | 1938. | 0.95 |
| 610. | 1.48 | 1939. | 0.95 |
| 611. | 1.48 | 1940. | 0.95 |
| 612. | 1.47 | 1941. | 0.95 |
| 613. | 1.48 | 1942. | 0.95 |
| 614. | 1.48 | 1943. | 0.95 |
| 615. | 1.47 | 1944. | 0.95 |
| 616. | 1.47 | 1945. | 0.95 |
| 617. | 1.47 | 1946. | 0.95 |
| 618. | 1.47 | 1947. | 0.95 |
| 619. | 1.47 | 1948. | 0.95 |
| 620. | 1.47 | 1949. | 0.95 |
| 621. | 1.47 | 1950. | 0.95 |
| 622. | 1.47 | 1951. | 0.94 |
| 623. | 1.47 | 1952. | 0.94 |
| 624. | 1.47 | 1953. | 0.94 |
| 625. | 1.47 | 1954. | 0.94 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 626. | 1.47 | 1955. | 0.94 |
| 627. | 1.47 | 1956. | 0.94 |
| 628. | 1.47 | 1957. | 0.94 |
| 629. | 1.46 | 1958. | 0.94 |
| 630. | 1.46 | 1959. | 0.94 |
| 631. | 1.46 | 1960. | 0.94 |
| 632. | 1.46 | 1961. | 0.94 |
| 633. | 1.46 | 1962. | 0.94 |
| 634. | 1.46 | 1963. | 0.94 |
| 635. | 1.46 | 1964. | 0.94 |
| 636. | 1.46 | 1965. | 0.94 |
| 637. | 1.46 | 1966. | 0.94 |
| 638. | 1.46 | 1967. | 0.94 |
| 639. | 1.46 | 1968. | 0.94 |
| 640. | 1.46 | 1969. | 0.94 |
| 641. | 1.46 | 1970. | 0.94 |
| 642. | 1.46 | 1971. | 0.94 |
| 643. | 1.46 | 1972. | 0.94 |
| 644. | 1.46 | 1973. | 0.94 |
| 645. | 1.45 | 1974. | 0.94 |
| 646. | 1.45 | 1975. | 0.94 |
| 647. | 1.45 | 1976. | 0.94 |
| 648. | 1.45 | 1977. | 0.94 |
| 649. | 1.45 | 1978. | 0.94 |
| 650. | 1.45 | 1979. | 0.94 |
| 651. | 1.45 | 1980. | 0.94 |
| 652. | 1.45 | 1981. | 0.94 |
| 653. | 1.45 | 1982. | 0.94 |
| 654. | 1.45 | 1983. | 0.94 |
| 655. | 1.45 | 1984. | 0.94 |
| 656. | 1.45 | 1985. | 0.94 |
| 657. | 1.45 | 1986. | 0.94 |
| 658. | 1.45 | 1987. | 0.94 |
| 659. | 1.45 | 1988. | 0.94 |
| 660. | 1.45 | 1989. | 0.94 |
| 661. | 1.44 | 1990. | 0.94 |
| 662. | 1.44 | 1991. | 0.94 |
| 663. | 1.45 | 1992. | 0.94 |
| 664. | 1.44 | 1993. | 0.94 |
| 665. | 1.44 | 1994. | 0.93 |
| 666. | 1.44 | 1995. | 0.94 |
| 667. | 1.44 | 1996. | 0.93 |
| 668. | 1.44 | 1997. | 0.93 |
| 669. | 1.44 | 1998. | 0.93 |
| 670. | 1.44 | 1999. | 0.93 |
| 671. | 1.44 | 2000. | 0.93 |
| 672. | 1.44 | 2001. | 0.93 |
| 673. | 1.44 | 2002. | 0.93 |
| 674. | 1.44 | 2003. | 0.93 |
| 675. | 1.44 | 2004. | 0.93 |
| 676. | 1.44 | 2005. | 0.93 |
| 677. | 1.43 | 2006. | 0.93 |
| 678. | 1.43 | 2007. | 0.93 |
| 679. | 1.43 | 2008. | 0.93 |
| 680. | 1.44 | 2009. | 0.93 |
| 681. | 1.43 | 2010. | 0.93 |
| 682. | 1.43 | 2011. | 0.93 |
| 683. | 1.43 | 2012. | 0.93 |
| 684. | 1.43 | 2013. | 0.93 |
| 685. | 1.43 | 2014. | 0.93 |
| 686. | 1.43 | 2015. | 0.93 |
| 687. | 1.43 | 2016. | 0.93 |
| 688. | 1.43 | 2017. | 0.93 |
| 689. | 1.43 | 2018. | 0.93 |
| 690. | 1.43 | 2019. | 0.93 |
| 691. | 1.43 | 2020. | 0.93 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 692. | 1.42 | 2021. | 0.93 |
| 693. | 1.43 | 2022. | 0.93 |
| 694. | 1.43 | 2023. | 0.93 |
| 695. | 1.43 | 2024. | 0.93 |
| 696. | 1.42 | 2025. | 0.93 |
| 697. | 1.42 | 2026. | 0.93 |
| 698. | 1.42 | 2027. | 0.93 |
| 699. | 1.42 | 2028. | 0.93 |
| 700. | 1.42 | 2029. | 0.93 |
| 701. | 1.42 | 2030. | 0.93 |
| 702. | 1.42 | 2031. | 0.93 |
| 703. | 1.42 | 2032. | 0.93 |
| 704. | 1.42 | 2033. | 0.93 |
| 705. | 1.42 | 2034. | 0.93 |
| 706. | 1.42 | 2035. | 0.93 |
| 707. | 1.42 | 2036. | 0.93 |
| 708. | 1.42 | 2037. | 0.92 |
| 709. | 1.42 | 2038. | 0.93 |
| 710. | 1.42 | 2039. | 0.92 |
| 711. | 1.41 | 2040. | 0.93 |
| 712. | 1.41 | 2041. | 0.92 |
| 713. | 1.42 | 2042. | 0.92 |
| 714. | 1.41 | 2043. | 0.92 |
| 715. | 1.41 | 2044. | 0.92 |
| 716. | 1.41 | 2045. | 0.92 |
| 717. | 1.41 | 2046. | 0.92 |
| 718. | 1.41 | 2047. | 0.92 |
| 719. | 1.41 | 2048. | 0.92 |
| 720. | 1.41 | 2049. | 0.92 |
| 721. | 1.41 | 2050. | 0.92 |
| 722. | 1.41 | 2051. | 0.92 |
| 723. | 1.41 | 2052. | 0.92 |
| 724. | 1.41 | 2053. | 0.92 |
| 725. | 1.41 | 2054. | 0.92 |
| 726. | 1.41 | 2055. | 0.92 |
| 727. | 1.4 | 2056. | 0.92 |
| 728. | 1.4 | 2057. | 0.92 |
| 729. | 1.4 | 2058. | 0.92 |
| 730. | 1.4 | 2059. | 0.92 |
| 731. | 1.4 | 2060. | 0.92 |
| 732. | 1.4 | 2061. | 0.92 |
| 733. | 1.4 | 2062. | 0.92 |
| 734. | 1.4 | 2063. | 0.92 |
| 735. | 1.4 | 2064. | 0.92 |
| 736. | 1.4 | 2065. | 0.92 |
| 737. | 1.4 | 2066. | 0.92 |
| 738. | 1.4 | 2067. | 0.92 |
| 739. | 1.4 | 2068. | 0.92 |
| 740. | 1.4 | 2069. | 0.92 |
| 741. | 1.4 | 2070. | 0.92 |
| 742. | 1.4 | 2071. | 0.92 |
| 743. | 1.4 | 2072. | 0.92 |
| 744. | 1.4 | 2073. | 0.92 |
| 745. | 1.4 | 2074. | 0.92 |
| 746. | 1.39 | 2075. | 0.92 |
| 747. | 1.39 | 2076. | 0.92 |
| 748. | 1.4 | 2077. | 0.92 |
| 749. | 1.4 | 2078. | 0.92 |
| 750. | 1.39 | 2079. | 0.92 |
| 751. | 1.39 | 2080. | 0.92 |
| 752. | 1.39 | 2081. | 0.92 |
| 753. | 1.39 | 2082. | 0.92 |
| 754. | 1.39 | 2083. | 0.92 |
| 755. | 1.39 | 2084. | 0.92 |
| 756. | 1.39 | 2085. | 0.91 |
| 757. | 1.39 | 2086. | 0.92 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 758. | 1.39 | 2087. | 0.91 |
| 759. | 1.39 | 2088. | 0.91 |
| 760. | 1.39 | 2089. | 0.92 |
| 761. | 1.38 | 2090. | 0.91 |
| 762. | 1.39 | 2091. | 0.91 |
| 763. | 1.39 | 2092. | 0.91 |
| 764. | 1.38 | 2093. | 0.91 |
| 765. | 1.39 | 2094. | 0.91 |
| 766. | 1.38 | 2095. | 0.91 |
| 767. | 1.38 | 2096. | 0.91 |
| 768. | 1.38 | 2097. | 0.91 |
| 769. | 1.38 | 2098. | 0.91 |
| 770. | 1.38 | 2099. | 0.91 |
| 771. | 1.38 | 2100. | 0.91 |
| 772. | 1.38 | 2101. | 0.91 |
| 773. | 1.38 | 2102. | 0.91 |
| 774. | 1.38 | 2103. | 0.91 |
| 775. | 1.38 | 2104. | 0.91 |
| 776. | 1.38 | 2105. | 0.91 |
| 777. | 1.38 | 2106. | 0.91 |
| 778. | 1.38 | 2107. | 0.91 |
| 779. | 1.38 | 2108. | 0.91 |
| 780. | 1.38 | 2109. | 0.91 |
| 781. | 1.38 | 2110. | 0.91 |
| 782. | 1.38 | 2111. | 0.91 |
| 783. | 1.37 | 2112. | 0.91 |
| 784. | 1.37 | 2113. | 0.91 |
| 785. | 1.37 | 2114. | 0.91 |
| 786. | 1.37 | 2115. | 0.91 |
| 787. | 1.37 | 2116. | 0.91 |
| 788. | 1.37 | 2117. | 0.91 |
| 789. | 1.37 | 2118. | 0.91 |
| 790. | 1.37 | 2119. | 0.91 |
| 791. | 1.37 | 2120. | 0.91 |
| 792. | 1.37 | 2121. | 0.91 |
| 793. | 1.37 | 2122. | 0.91 |
| 794. | 1.37 | 2123. | 0.91 |
| 795. | 1.37 | 2124. | 0.91 |
| 796. | 1.37 | 2125. | 0.91 |
| 797. | 1.37 | 2126. | 0.91 |
| 798. | 1.36 | 2127. | 0.91 |
| 799. | 1.37 | 2128. | 0.91 |
| 800. | 1.37 | 2129. | 0.91 |
| 801. | 1.36 | 2130. | 0.91 |
| 802. | 1.36 | 2131. | 0.91 |
| 803. | 1.36 | 2132. | 0.91 |
| 804. | 1.36 | 2133. | 0.91 |
| 805. | 1.36 | 2134. | 0.9 |
| 806. | 1.36 | 2135. | 0.91 |
| 807. | 1.36 | 2136. | 0.9 |
| 808. | 1.36 | 2137. | 0.9 |
| 809. | 1.36 | 2138. | 0.9 |
| 810. | 1.36 | 2139. | 0.9 |
| 811. | 1.36 | 2140. | 0.9 |
| 812. | 1.36 | 2141. | 0.9 |
| 813. | 1.36 | 2142. | 0.9 |
| 814. | 1.36 | 2143. | 0.9 |
| 815. | 1.35 | 2144. | 0.9 |
| 816. | 1.35 | 2145. | 0.9 |
| 817. | 1.36 | 2146. | 0.9 |
| 818. | 1.35 | 2147. | 0.9 |
| 819. | 1.35 | 2148. | 0.9 |
| 820. | 1.35 | 2149. | 0.9 |
| 821. | 1.35 | 2150. | 0.9 |
| 822. | 1.35 | 2151. | 0.9 |
| 823. | 1.35 | 2152. | 0.9 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 824. | 1.35 | 2153. | 0.9 |
| 825. | 1.35 | 2154. | 0.9 |
| 826. | 1.35 | 2155. | 0.9 |
| 827. | 1.35 | 2156. | 0.9 |
| 828. | 1.35 | 2157. | 0.9 |
| 829. | 1.35 | 2158. | 0.9 |
| 830. | 1.35 | 2159. | 0.9 |
| 831. | 1.35 | 2160. | 0.9 |
| 832. | 1.35 | 2161. | 0.9 |
| 833. | 1.35 | 2162. | 0.9 |
| 834. | 1.35 | 2163. | 0.9 |
| 835. | 1.35 | 2164. | 0.9 |
| 836. | 1.35 | 2165. | 0.9 |
| 837. | 1.35 | 2166. | 0.9 |
| 838. | 1.34 | 2167. | 0.9 |
| 839. | 1.34 | 2168. | 0.9 |
| 840. | 1.34 | 2169. | 0.9 |
| 841. | 1.34 | 2170. | 0.9 |
| 842. | 1.34 | 2171. | 0.9 |
| 843. | 1.35 | 2172. | 0.9 |
| 844. | 1.34 | 2173. | 0.9 |
| 845. | 1.34 | 2174. | 0.9 |
| 846. | 1.34 | 2175. | 0.9 |
| 847. | 1.34 | 2176. | 0.9 |
| 848. | 1.34 | 2177. | 0.9 |
| 849. | 1.34 | 2178. | 0.9 |
| 850. | 1.34 | 2179. | 0.9 |
| 851. | 1.34 | 2180. | 0.9 |
| 852. | 1.34 | 2181. | 0.9 |
| 853. | 1.34 | 2182. | 0.9 |
| 854. | 1.34 | 2183. | 0.89 |
| 855. | 1.33 | 2184. | 0.9 |
| 856. | 1.34 | 2185. | 0.89 |
| 857. | 1.33 | 2186. | 0.89 |
| 858. | 1.33 | 2187. | 0.89 |
| 859. | 1.33 | 2188. | 0.89 |
| 860. | 1.33 | 2189. | 0.9 |
| 861. | 1.33 | 2190. | 0.89 |
| 862. | 1.33 | 2191. | 0.89 |
| 863. | 1.33 | 2192. | 0.89 |
| 864. | 1.33 | 2193. | 0.89 |
| 865. | 1.33 | 2194. | 0.89 |
| 866. | 1.33 | 2195. | 0.89 |
| 867. | 1.33 | 2196. | 0.89 |
| 868. | 1.33 | 2197. | 0.89 |
| 869. | 1.33 | 2198. | 0.89 |
| 870. | 1.33 | 2199. | 0.89 |
| 871. | 1.33 | 2200. | 0.89 |
| 872. | 1.33 | 2201. | 0.89 |
| 873. | 1.32 | 2202. | 0.89 |
| 874. | 1.33 | 2203. | 0.89 |
| 875. | 1.32 | 2204. | 0.89 |
| 876. | 1.33 | 2205. | 0.89 |
| 877. | 1.32 | 2206. | 0.89 |
| 878. | 1.32 | 2207. | 0.89 |
| 879. | 1.32 | 2208. | 0.89 |
| 880. | 1.32 | 2209. | 0.89 |
| 881. | 1.32 | 2210. | 0.89 |
| 882. | 1.32 | 2211. | 0.89 |
| 883. | 1.32 | 2212. | 0.89 |
| 884. | 1.32 | 2213. | 0.89 |
| 885. | 1.32 | 2214. | 0.89 |
| 886. | 1.32 | 2215. | 0.89 |
| 887. | 1.32 | 2216. | 0.89 |
| 888. | 1.32 | 2217. | 0.89 |
| 889. | 1.32 | 2218. | 0.89 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 890. | 1.32 | 2219. | 0.89 |
| 891. | 1.32 | 2220. | 0.89 |
| 892. | 1.32 | 2221. | 0.89 |
| 893. | 1.32 | 2222. | 0.89 |
| 894. | 1.31 | 2223. | 0.89 |
| 895. | 1.31 | 2224. | 0.89 |
| 896. | 1.31 | 2225. | 0.89 |
| 897. | 1.31 | 2226. | 0.89 |
| 898. | 1.31 | 2227. | 0.89 |
| 899. | 1.31 | 2228. | 0.88 |
| 900. | 1.31 | 2229. | 0.89 |
| 901. | 1.31 | 2230. | 0.89 |
| 902. | 1.31 | 2231. | 0.88 |
| 903. | 1.31 | 2232. | 0.89 |
| 904. | 1.31 | 2233. | 0.88 |
| 905. | 1.31 | 2234. | 0.88 |
| 906. | 1.31 | 2235. | 0.88 |
| 907. | 1.31 | 2236. | 0.88 |
| 908. | 1.31 | 2237. | 0.89 |
| 909. | 1.31 | 2238. | 0.88 |
| 910. | 1.31 | 2239. | 0.88 |
| 911. | 1.31 | 2240. | 0.88 |
| 912. | 1.3 | 2241. | 0.88 |
| 913. | 1.31 | 2242. | 0.88 |
| 914. | 1.3 | 2243. | 0.88 |
| 915. | 1.3 | 2244. | 0.88 |
| 916. | 1.3 | 2245. | 0.88 |
| 917. | 1.3 | 2246. | 0.88 |
| 918. | 1.3 | 2247. | 0.88 |
| 919. | 1.3 | 2248. | 0.88 |
| 920. | 1.3 | 2249. | 0.88 |
| 921. | 1.3 | 2250. | 0.88 |
| 922. | 1.3 | 2251. | 0.88 |
| 923. | 1.3 | 2252. | 0.88 |
| 924. | 1.3 | 2253. | 0.88 |
| 925. | 1.3 | 2254. | 0.88 |
| 926. | 1.3 | 2255. | 0.88 |
| 927. | 1.3 | 2256. | 0.88 |
| 928. | 1.3 | 2257. | 0.88 |
| 929. | 1.3 | 2258. | 0.88 |
| 930. | 1.29 | 2259. | 0.88 |
| 931. | 1.3 | 2260. | 0.88 |
| 932. | 1.3 | 2261. | 0.88 |
| 933. | 1.3 | 2262. | 0.88 |
| 934. | 1.3 | 2263. | 0.88 |
| 935. | 1.29 | 2264. | 0.88 |
| 936. | 1.29 | 2265. | 0.88 |
| 937. | 1.29 | 2266. | 0.88 |
| 938. | 1.29 | 2267. | 0.88 |
| 939. | 1.29 | 2268. | 0.88 |
| 940. | 1.29 | 2269. | 0.88 |
| 941. | 1.29 | 2270. | 0.88 |
| 942. | 1.29 | 2271. | 0.88 |
| 943. | 1.29 | 2272. | 0.88 |
| 944. | 1.29 | 2273. | 0.88 |
| 945. | 1.29 | 2274. | 0.88 |
| 946. | 1.29 | 2275. | 0.88 |
| 947. | 1.29 | 2276. | 0.88 |
| 948. | 1.29 | 2277. | 0.87 |
| 949. | 1.29 | 2278. | 0.88 |
| 950. | 1.29 | 2279. | 0.87 |
| 951. | 1.29 | 2280. | 0.88 |
| 952. | 1.29 | 2281. | 0.88 |
| 953. | 1.29 | 2282. | 0.87 |
| 954. | 1.28 | 2283. | 0.87 |
| 955. | 1.28 | 2284. | 0.87 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 956. | 1.28 | 2285. | 0.88 |
| 957. | 1.28 | 2286. | 0.87 |
| 958. | 1.28 | 2287. | 0.87 |
| 959. | 1.28 | 2288. | 0.87 |
| 960. | 1.28 | 2289. | 0.87 |
| 961. | 1.28 | 2290. | 0.87 |
| 962. | 1.28 | 2291. | 0.87 |
| 963. | 1.28 | 2292. | 0.87 |
| 964. | 1.28 | 2293. | 0.87 |
| 965. | 1.28 | 2294. | 0.87 |
| 966. | 1.28 | 2295. | 0.87 |
| 967. | 1.28 | 2296. | 0.87 |
| 968. | 1.28 | 2297. | 0.87 |
| 969. | 1.28 | 2298. | 0.87 |
| 970. | 1.28 | 2299. | 0.87 |
| 971. | 1.28 | 2300. | 0.87 |
| 972. | 1.28 | 2301. | 0.87 |
| 973. | 1.28 | 2302. | 0.87 |
| 974. | 1.28 | 2303. | 0.87 |
| 975. | 1.28 | 2304. | 0.87 |
| 976. | 1.27 | 2305. | 0.87 |
| 977. | 1.27 | 2306. | 0.87 |
| 978. | 1.27 | 2307. | 0.87 |
| 979. | 1.27 | 2308. | 0.87 |
| 980. | 1.27 | 2309. | 0.87 |
| 981. | 1.27 | 2310. | 0.87 |
| 982. | 1.27 | 2311. | 0.87 |
| 983. | 1.27 | 2312. | 0.87 |
| 984. | 1.27 | 2313. | 0.87 |
| 985. | 1.27 | 2314. | 0.87 |
| 986. | 1.27 | 2315. | 0.87 |
| 987. | 1.27 | 2316. | 0.87 |
| 988. | 1.27 | 2317. | 0.87 |
| 989. | 1.27 | 2318. | 0.87 |
| 990. | 1.27 | 2319. | 0.87 |
| 991. | 1.27 | 2320. | 0.87 |
| 992. | 1.27 | 2321. | 0.87 |
| 993. | 1.27 | 2322. | 0.87 |
| 994. | 1.27 | 2323. | 0.87 |
| 995. | 1.26 | 2324. | 0.87 |
| 996. | 1.26 | 2325. | 0.87 |
| 997. | 1.26 | 2326. | 0.87 |
| 998. | 1.26 | 2327. | 0.87 |
| 999. | 1.26 | 2328. | 0.87 |
| 1000. | 1.26 | 2329. | 0.87 |
| 1001. | 1.26 | 2330. | 0.87 |
| 1002. | 1.26 | 2331. | 0.87 |
| 1003. | 1.26 | 2332. | 0.87 |
| 1004. | 1.26 | 2333. | 0.86 |
| 1005. | 1.26 | 2334. | 0.86 |
| 1006. | 1.26 | 2335. | 0.86 |
| 1007. | 1.26 | 2336. | 0.87 |
| 1008. | 1.26 | 2337. | 0.86 |
| 1009. | 1.26 | 2338. | 0.86 |
| 1010. | 1.26 | 2339. | 0.86 |
| 1011. | 1.26 | 2340. | 0.87 |
| 1012. | 1.26 | 2341. | 0.86 |
| 1013. | 1.26 | 2342. | 0.86 |
| 1014. | 1.26 | 2343. | 0.86 |
| 1015. | 1.26 | 2344. | 0.86 |
| 1016. | 1.26 | 2345. | 0.86 |
| 1017. | 1.26 | 2346. | 0.86 |
| 1018. | 1.25 | 2347. | 0.86 |
| 1019. | 1.25 | 2348. | 0.86 |
| 1020. | 1.26 | 2349. | 0.86 |
| 1021. | 1.25 | 2350. | 0.86 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 1022. | 1.25 | 2351. | 0.86 |
| 1023. | 1.25 | 2352. | 0.86 |
| 1024. | 1.25 | 2353. | 0.86 |
| 1025. | 1.25 | 2354. | 0.86 |
| 1026. | 1.25 | 2355. | 0.86 |
| 1027. | 1.25 | 2356. | 0.86 |
| 1028. | 1.25 | 2357. | 0.86 |
| 1029. | 1.25 | 2358. | 0.86 |
| 1030. | 1.25 | 2359. | 0.86 |
| 1031. | 1.25 | 2360. | 0.86 |
| 1032. | 1.25 | 2361. | 0.86 |
| 1033. | 1.25 | 2362. | 0.86 |
| 1034. | 1.25 | 2363. | 0.86 |
| 1035. | 1.25 | 2364. | 0.86 |
| 1036. | 1.25 | 2365. | 0.86 |
| 1037. | 1.24 | 2366. | 0.86 |
| 1038. | 1.24 | 2367. | 0.86 |
| 1039. | 1.24 | 2368. | 0.86 |
| 1040. | 1.24 | 2369. | 0.86 |
| 1041. | 1.24 | 2370. | 0.86 |
| 1042. | 1.24 | 2371. | 0.86 |
| 1043. | 1.24 | 2372. | 0.86 |
| 1044. | 1.24 | 2373. | 0.86 |
| 1045. | 1.24 | 2374. | 0.86 |
| 1046. | 1.24 | 2375. | 0.86 |
| 1047. | 1.24 | 2376. | 0.86 |
| 1048. | 1.24 | 2377. | 0.86 |
| 1049. | 1.24 | 2378. | 0.86 |
| 1050. | 1.24 | 2379. | 0.86 |
| 1051. | 1.24 | 2380. | 0.86 |
| 1052. | 1.24 | 2381. | 0.86 |
| 1053. | 1.24 | 2382. | 0.86 |
| 1054. | 1.24 | 2383. | 0.86 |
| 1055. | 1.24 | 2384. | 0.86 |
| 1056. | 1.24 | 2385. | 0.86 |
| 1057. | 1.24 | 2386. | 0.86 |
| 1058. | 1.24 | 2387. | 0.86 |
| 1059. | 1.23 | 2388. | 0.86 |
| 1060. | 1.24 | 2389. | 0.85 |
| 1061. | 1.23 | 2390. | 0.86 |
| 1062. | 1.23 | 2391. | 0.85 |
| 1063. | 1.23 | 2392. | 0.85 |
| 1064. | 1.23 | 2393. | 0.85 |
| 1065. | 1.23 | 2394. | 0.85 |
| 1066. | 1.23 | 2395. | 0.85 |
| 1067. | 1.23 | 2396. | 0.85 |
| 1068. | 1.23 | 2397. | 0.85 |
| 1069. | 1.23 | 2398. | 0.85 |
| 1070. | 1.23 | 2399. | 0.85 |
| 1071. | 1.23 | 2400. | 0.85 |
| 1072. | 1.23 | 2401. | 0.85 |
| 1073. | 1.23 | 2402. | 0.85 |
| 1074. | 1.23 | 2403. | 0.85 |
| 1075. | 1.23 | 2404. | 0.85 |
| 1076. | 1.23 | 2405. | 0.85 |
| 1077. | 1.23 | 2406. | 0.85 |
| 1078. | 1.23 | 2407. | 0.85 |
| 1079. | 1.23 | 2408. | 0.85 |
| 1080. | 1.23 | 2409. | 0.85 |
| 1081. | 1.23 | 2410. | 0.85 |
| 1082. | 1.23 | 2411. | 0.85 |
| 1083. | 1.22 | 2412. | 0.85 |
| 1084. | 1.23 | 2413. | 0.85 |
| 1085. | 1.23 | 2414. | 0.85 |
| 1086. | 1.22 | 2415. | 0.85 |
| 1087. | 1.22 | 2416. | 0.85 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 1088. | 1.22 | 2417. | 0.85 |
| 1089. | 1.22 | 2418. | 0.85 |
| 1090. | 1.22 | 2419. | 0.85 |
| 1091. | 1.22 | 2420. | 0.85 |
| 1092. | 1.22 | 2421. | 0.85 |
| 1093. | 1.22 | 2422. | 0.85 |
| 1094. | 1.22 | 2423. | 0.85 |
| 1095. | 1.22 | 2424. | 0.85 |
| 1096. | 1.22 | 2425. | 0.85 |
| 1097. | 1.22 | 2426. | 0.85 |
| 1098. | 1.22 | 2427. | 0.85 |
| 1099. | 1.22 | 2428. | 0.85 |
| 1100. | 1.22 | 2429. | 0.85 |
| 1101. | 1.22 | 2430. | 0.85 |
| 1102. | 1.22 | 2431. | 0.85 |
| 1103. | 1.22 | 2432. | 0.85 |
| 1104. | 1.22 | 2433. | 0.85 |
| 1105. | 1.21 | 2434. | 0.85 |
| 1106. | 1.21 | 2435. | 0.85 |
| 1107. | 1.21 | 2436. | 0.85 |
| 1108. | 1.21 | 2437. | 0.85 |
| 1109. | 1.21 | 2438. | 0.85 |
| 1110. | 1.21 | 2439. | 0.85 |
| 1111. | 1.21 | 2440. | 0.85 |
| 1112. | 1.21 | 2441. | 0.85 |
| 1113. | 1.21 | 2442. | 0.85 |
| 1114. | 1.21 | 2443. | 0.84 |
| 1115. | 1.21 | 2444. | 0.85 |
| 1116. | 1.21 | 2445. | 0.84 |
| 1117. | 1.21 | 2446. | 0.85 |
| 1118. | 1.21 | 2447. | 0.84 |
| 1119. | 1.21 | 2448. | 0.85 |
| 1120. | 1.21 | 2449. | 0.85 |
| 1121. | 1.21 | 2450. | 0.84 |
| 1122. | 1.21 | 2451. | 0.84 |
| 1123. | 1.21 | 2452. | 0.84 |
| 1124. | 1.21 | 2453. | 0.84 |
| 1125. | 1.21 | 2454. | 0.84 |
| 1126. | 1.21 | 2455. | 0.84 |
| 1127. | 1.21 | 2456. | 0.84 |
| 1128. | 1.2 | 2457. | 0.84 |
| 1129. | 1.2 | 2458. | 0.84 |
| 1130. | 1.2 | 2459. | 0.84 |
| 1131. | 1.2 | 2460. | 0.84 |
| 1132. | 1.2 | 2461. | 0.84 |
| 1133. | 1.2 | 2462. | 0.84 |
| 1134. | 1.2 | 2463. | 0.84 |
| 1135. | 1.2 | 2464. | 0.84 |
| 1136. | 1.2 | 2465. | 0.84 |
| 1137. | 1.2 | 2466. | 0.84 |
| 1138. | 1.2 | 2467. | 0.84 |
| 1139. | 1.2 | 2468. | 0.84 |
| 1140. | 1.2 | 2469. | 0.84 |
| 1141. | 1.2 | 2470. | 0.84 |
| 1142. | 1.2 | 2471. | 0.84 |
| 1143. | 1.2 | 2472. | 0.84 |
| 1144. | 1.2 | 2473. | 0.84 |
| 1145. | 1.2 | 2474. | 0.84 |
| 1146. | 1.2 | 2475. | 0.84 |
| 1147. | 1.2 | 2476. | 0.84 |
| 1148. | 1.2 | 2477. | 0.84 |
| 1149. | 1.2 | 2478. | 0.84 |
| 1150. | 1.2 | 2479. | 0.84 |
| 1151. | 1.19 | 2480. | 0.84 |
| 1152. | 1.2 | 2481. | 0.84 |
| 1153. | 1.19 | 2482. | 0.84 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 1154. | 1.19 | 2483. | 0.84 |
| 1155. | 1.19 | 2484. | 0.84 |
| 1156. | 1.19 | 2485. | 0.84 |
| 1157. | 1.19 | 2486. | 0.84 |
| 1158. | 1.19 | 2487. | 0.84 |
| 1159. | 1.19 | 2488. | 0.84 |
| 1160. | 1.19 | 2489. | 0.84 |
| 1161. | 1.19 | 2490. | 0.84 |
| 1162. | 1.19 | 2491. | 0.84 |
| 1163. | 1.19 | 2492. | 0.84 |
| 1164. | 1.19 | 2493. | 0.84 |
| 1165. | 1.19 | 2494. | 0.84 |
| 1166. | 1.19 | 2495. | 0.84 |
| 1167. | 1.19 | 2496. | 0.84 |
| 1168. | 1.19 | 2497. | 0.84 |
| 1169. | 1.19 | 2498. | 0.84 |
| 1170. | 1.19 | 2499. | 0.84 |
| 1171. | 1.19 | 2500. | 0.83 |
| 1172. | 1.19 | 2501. | 0.84 |
| 1173. | 1.19 | 2502. | 0.84 |
| 1174. | 1.19 | 2503. | 0.83 |
| 1175. | 1.18 | 2504. | 0.83 |
| 1176. | 1.19 | 2505. | 0.83 |
| 1177. | 1.19 | 2506. | 0.83 |
| 1178. | 1.18 | 2507. | 0.83 |
| 1179. | 1.18 | 2508. | 0.83 |
| 1180. | 1.18 | 2509. | 0.83 |
| 1181. | 1.18 | 2510. | 0.83 |
| 1182. | 1.18 | 2511. | 0.83 |
| 1183. | 1.18 | 2512. | 0.83 |
| 1184. | 1.18 | 2513. | 0.83 |
| 1185. | 1.18 | 2514. | 0.83 |
| 1186. | 1.18 | 2515. | 0.83 |
| 1187. | 1.18 | 2516. | 0.83 |
| 1188. | 1.18 | 2517. | 0.83 |
| 1189. | 1.18 | 2518. | 0.83 |
| 1190. | 1.18 | 2519. | 0.83 |
| 1191. | 1.18 | 2520. | 0.83 |
| 1192. | 1.18 | 2521. | 0.83 |
| 1193. | 1.18 | 2522. | 0.83 |
| 1194. | 1.18 | 2523. | 0.83 |
| 1195. | 1.18 | 2524. | 0.83 |
| 1196. | 1.18 | 2525. | 0.83 |
| 1197. | 1.18 | 2526. | 0.83 |
| 1198. | 1.18 | 2527. | 0.83 |
| 1199. | 1.18 | 2528. | 0.83 |
| 1200. | 1.18 | 2529. | 0.83 |
| 1201. | 1.18 | 2530. | 0.83 |
| 1202. | 1.17 | 2531. | 0.83 |
| 1203. | 1.17 | 2532. | 0.83 |
| 1204. | 1.17 | 2533. | 0.83 |
| 1205. | 1.18 | 2534. | 0.83 |
| 1206. | 1.17 | 2535. | 0.83 |
| 1207. | 1.17 | 2536. | 0.83 |
| 1208. | 1.17 | 2537. | 0.83 |
| 1209. | 1.17 | 2538. | 0.83 |
| 1210. | 1.17 | 2539. | 0.83 |
| 1211. | 1.17 | 2540. | 0.83 |
| 1212. | 1.17 | 2541. | 0.83 |
| 1213. | 1.17 | 2542. | 0.83 |
| 1214. | 1.17 | 2543. | 0.83 |
| 1215. | 1.17 | 2544. | 0.83 |
| 1216. | 1.17 | 2545. | 0.83 |
| 1217. | 1.17 | 2546. | 0.83 |
| 1218. | 1.17 | 2547. | 0.83 |
| 1219. | 1.17 | 2548. | 0.83 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 1220. | 1.17 | 2549. | 0.83 |
| 1221. | 1.17 | 2550. | 0.83 |
| 1222. | 1.17 | 2551. | 0.83 |
| 1223. | 1.17 | 2552. | 0.83 |
| 1224. | 1.17 | 2553. | 0.83 |
| 1225. | 1.16 | 2554. | 0.83 |
| 1226. | 1.16 | 2555. | 0.83 |
| 1227. | 1.16 | 2556. | 0.83 |
| 1228. | 1.17 | 2557. | 0.83 |
| 1229. | 1.16 | 2558. | 0.83 |
| 1230. | 1.16 | 2559. | 0.83 |
| 1231. | 1.16 | 2560. | 0.83 |
| 1232. | 1.16 | 2561. | 0.83 |
| 1233. | 1.16 | 2562. | 0.82 |
| 1234. | 1.16 | 2563. | 0.82 |
| 1235. | 1.16 | 2564. | 0.82 |
| 1236. | 1.16 | 2565. | 0.83 |
| 1237. | 1.16 | 2566. | 0.82 |
| 1238. | 1.16 | 2567. | 0.82 |
| 1239. | 1.16 | 2568. | 0.82 |
| 1240. | 1.16 | 2569. | 0.82 |
| 1241. | 1.16 | 2570. | 0.82 |
| 1242. | 1.16 | 2571. | 0.82 |
| 1243. | 1.16 | 2572. | 0.82 |
| 1244. | 1.16 | 2573. | 0.82 |
| 1245. | 1.16 | 2574. | 0.82 |
| 1246. | 1.16 | 2575. | 0.82 |
| 1247. | 1.16 | 2576. | 0.82 |
| 1248. | 1.16 | 2577. | 0.82 |
| 1249. | 1.16 | 2578. | 0.82 |
| 1250. | 1.16 | 2579. | 0.82 |
| 1251. | 1.16 | 2580. | 0.82 |
| 1252. | 1.16 | 2581. | 0.82 |
| 1253. | 1.16 | 2582. | 0.82 |
| 1254. | 1.15 | 2583. | 0.82 |
| 1255. | 1.15 | 2584. | 0.82 |
| 1256. | 1.16 | 2585. | 0.82 |
| 1257. | 1.15 | 2586. | 0.82 |
| 1258. | 1.15 | 2587. | 0.82 |
| 1259. | 1.15 | 2588. | 0.82 |
| 1260. | 1.15 | 2589. | 0.82 |
| 1261. | 1.15 | 2590. | 0.82 |
| 1262. | 1.15 | 2591. | 0.82 |
| 1263. | 1.15 | 2592. | 0.82 |
| 1264. | 1.15 | 2593. | 0.82 |
| 1265. | 1.15 | 2594. | 0.82 |
| 1266. | 1.15 | 2595. | 0.82 |
| 1267. | 1.15 | 2596. | 0.82 |
| 1268. | 1.15 | 2597. | 0.82 |
| 1269. | 1.15 | 2598. | 0.82 |
| 1270. | 1.15 | 2599. | 0.82 |
| 1271. | 1.15 | 2600. | 0.82 |
| 1272. | 1.15 | 2601. | 0.82 |
| 1273. | 1.15 | 2602. | 0.82 |
| 1274. | 1.15 | 2603. | 0.82 |
| 1275. | 1.15 | 2604. | 0.82 |
| 1276. | 1.15 | 2605. | 0.82 |
| 1277. | 1.15 | 2606. | 0.82 |
| 1278. | 1.15 | 2607. | 0.82 |
| 1279. | 1.15 | 2608. | 0.82 |
| 1280. | 1.15 | 2609. | 0.82 |
| 1281. | 1.14 | 2610. | 0.82 |
| 1282. | 1.15 | 2611. | 0.82 |
| 1283. | 1.14 | 2612. | 0.82 |
| 1284. | 1.14 | 2613. | 0.82 |
| 1285. | 1.14 | 2614. | 0.82 |

| <u>Time (sec)</u> | <u>Displacement (ft)</u> | <u>Time (sec)</u> | <u>Displacement (ft)</u> |
|-------------------|--------------------------|-------------------|--------------------------|
| 1286. | 1.14 | 2615. | 0.82 |
| 1287. | 1.14 | 2616. | 0.81 |
| 1288. | 1.14 | 2617. | 0.82 |
| 1289. | 1.14 | 2618. | 0.82 |
| 1290. | 1.14 | 2619. | 0.82 |
| 1291. | 1.14 | 2620. | 0.82 |
| 1292. | 1.14 | 2621. | 0.82 |
| 1293. | 1.14 | 2622. | 0.82 |
| 1294. | 1.14 | 2623. | 0.82 |
| 1295. | 1.14 | 2624. | 0.81 |
| 1296. | 1.14 | 2625. | 0.82 |
| 1297. | 1.14 | 2626. | 0.81 |
| 1298. | 1.14 | 2627. | 0.81 |
| 1299. | 1.14 | 2628. | 0.81 |
| 1300. | 1.14 | 2629. | 0.81 |
| 1301. | 1.14 | 2630. | 0.81 |
| 1302. | 1.14 | 2631. | 0.81 |
| 1303. | 1.14 | 2632. | 0.81 |
| 1304. | 1.14 | 2633. | 0.81 |
| 1305. | 1.14 | 2634. | 0.81 |
| 1306. | 1.14 | 2635. | 0.81 |
| 1307. | 1.13 | 2636. | 0.81 |
| 1308. | 1.14 | 2637. | 0.81 |
| 1309. | 1.14 | 2638. | 0.81 |
| 1310. | 1.13 | 2639. | 0.81 |
| 1311. | 1.13 | 2640. | 0.81 |
| 1312. | 1.13 | 2641. | 0.81 |
| 1313. | 1.13 | 2642. | 0.81 |
| 1314. | 1.13 | 2643. | 0.81 |
| 1315. | 1.13 | 2644. | 0.81 |
| 1316. | 1.13 | 2645. | 0.82 |
| 1317. | 1.13 | 2646. | 0.81 |
| 1318. | 1.13 | 2647. | 0.81 |
| 1319. | 1.13 | 2648. | 0.81 |
| 1320. | 1.13 | 2649. | 0.81 |
| 1321. | 1.13 | 2650. | 0.81 |
| 1322. | 1.13 | 2651. | 0.81 |
| 1323. | 1.13 | 2652. | 0.81 |
| 1324. | 1.13 | 2653. | 0.81 |
| 1325. | 1.13 | 2654. | 0.81 |
| 1326. | 1.13 | 2655. | 0.81 |
| 1327. | 1.13 | 2656. | 0.81 |
| 1328. | 1.13 | 2657. | 0.81 |
| 1329. | 1.13 | 2658. | 0.81 |
| 1330. | 1.13 | 2659. | 0.81 |
| 1331. | 1.13 | | |

SOLUTION

Slug Test
 Aquifer Model: Unconfined
 Solution Method: Bouwer-Rice
 In(Re/rw): 2.56

VISUAL ESTIMATION RESULTSEstimated Parameters

| <u>Parameter</u> | <u>Estimate</u> | |
|------------------|-----------------|--------|
| K | 1.621E-5 | cm/sec |
| y0 | 2.006 | ft |

T = K*b = 0.003953 cm²/sec